

UNITED STATES NATURAL RESOURCES (USNR) TEST PLOT –

ANNUAL REPORT NO. 1

LITTLE ROCK AND TYRONE MINES

REPORT

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1.0 INTRODUCTION

The Little Rock Mine is permitted as an existing mine under Mining Act Permit No. GR007RE and Discharge Permit 1236 (DP-1236). The best available materials for reclamation at the Little Rock mine is overburden composed of Precambrian Granite. In early 2014, Freeport Mc-Moran Inc. (Tyrone) proposed to build test plots on a portion of the United States National Resource (USNR) reclamation area to evaluate the use of Precambrian Granite from the Little Rock pit. The test plot was tentatively approved by the New Mexico Mining and Minerals Division (MMD) and the New Mexico Environment Department (NMED) prior to construction with the understanding that formal approval was pending further consideration. The test plots were constructed starting in 2014 and seeded in the Spring of 2015.

In November 2014, Tyrone prepared a work plan for the USNR test plots to facilitate technical discussion with the MMD and NMED. The Agencies requested that Tyrone modify the work plan to include enhanced erosion and vegetation monitoring and consider the application of amendments. The USNR test plot work plan was conditionally approved and is intended to meet the requirements of Condition 8.P.1 (b) of Revision 14-1 to Permit GR007RE and Condition 33 of DP-1236. The intent of this submittal is to document the construction of the test plots and provide results of the erosion and vegetation monitoring.

1.1 Background

The Little Rock Test Plots were originally constructed on the 7A Stockpile at the Tyrone Mine using Precambrian Granite overburden from the Copper Mountain Pit. When the Little Rock Test Plot work plan was originally developed (2001 with major revisions in 2004) it was impractical to access the overburden from the Little Rock pit because mining had not started and the haul road to Tyrone was not constructed. Copper Mountain materials were used because of their similarity to the overburden from the Little Rock pit and the availability of materials and a test location (7A stockpile). Once mining at Little Rock commenced, it was possible to construct test plots using overburden from the Little Rock pit. The USNR reclamation area provided an opportunity to test the overburden material from the Little Rock pit and further refine and demonstrate material handling techniques and reclamation specifications.

1.2 Objectives

The primary goal for the USNR test plot program is to evaluate revegetation success for the Little Rock Precambrian granite. Tyrone hypothesized that multiple year delays in seeding the Precambrian Granite on the 7A test plots, combined with drought conditions, contributed to unacceptable vegetation establishment (Golder, 2014). Thus, the major performance criterion to be assessed at the USNR test plots is vegetation performance. These test plots will further inform Tyrone about the implications of surface armoring on seedling establishment over time. Because the vegetation establishment was delayed quantitative erosion measurement were not made on the 7A test plots. The establishment of quantitative



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erosion transects in the USNR cover materials will aid in quantifying erosion on the Precambrian Granite cover materials.



2.0 USNR TEST PLOT CHARACTERISTICS

Reclamation of the USNR Leach Stockpile area involved removal of the residual leached ore materials primarily from drainage areas, minor regrading of the site to tie into bedrock drainages, and installation of a nominal 3-foot thick cover of Precambrian Granite from the Little Rock Mine. The construction and material handling methods are described in Section 2.1. The layout and design of the test plot treatments are discussed in Section 2.2. The revegetation techniques are described in Section 2.3.

2.1 Construction and Materials Handling

Test plot construction included site grading, cover placement, and revegetation. Test plots were constructed using available mine equipment. Cover for the test plots was sourced from the Little Rock Open Pit Phase 4 mining area. As a normal course of operations, Tyrone follows the Material Characterization and Handling Plan (dated October 25, 2011) for its cover material segregation. This plan was implemented in segregating material for USNR reclamation and the test plots. In addition to the procedures outlined in the characterization and handling plan, Tyrone reclamation quality control personnel visually monitored the source material (in the Little Rock pit) and rejected materials that were too coarse for use as cover. The materials were hauled from the pit with large haul trucks (CAT 793) and staged near the test plots, prior to hauling with smaller trucks (CAT 730 Ejector) to the test plots; smaller truck were used to place cover materials as the roads were too narrow for larger haul trucks. Consistent with Tyrone's materials management practices, the materials on the temporary stockpile where managed to reduce the overall volume of rock fragments. Cover material was end-dumped on the test plots using ≈30 ton trucks and graded down slope with a dozer.

2.2 Test Plot Layout and Design

The two acre test plot included four treatments which were approximately a half acre each. A control and three treatments were proposed for the USNR test plots. The major treatments involve changes in the seed mix and the timing of mulching. The treatments are described below:

- Control (conventional seed mix and mulching)
- Mulch prior to seeding with conventional seed mix
- Conventional mulch with alternative seed mix
- Mulch prior to seeding with alternative seed mix

Figure 1 illustrates the layout and configuration of the USNR test plots. Typical cross-sections are shown in Figure 2. The finished slope gradients on the test plot ranged from about 3:1 to 4:1. Based on the final surveys, the slope lengths ranged from about 150 to 180 feet. The cover thickness exceeded three feet on the test plot (Section 3.2).





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2.3 Revegetation

The plots were revegetated in a manner consistent with requirements of Appendix C of Permit GR007RE, with some minor variations related to the seed mix and the timing of the mulching, which are described below. The revegetation operations were performed by the Freeport-McMoRan seeding crew on June 4 and 5, 2015. Operationally, the revegetation procedures included: 1) scarification and seedbed preparation, 2) seeding, and 3) mulching and crimping.

2.3.1 Scarification and Seeding

Scarification was performed on the contour at a depth of 8-12 inches. The seed was drilled and broadcast simultaneously using a modified rangeland drill with depth control bands, packer wheels, agitators and augers, and picker wheels. The light and fluffy seeds were allowed to fall freely behind the drill and were covered using chain drags pulled behind the drill. Compact seeds were drilled to promote proper seed placement.

2.3.2 Seed Mix

Two seed mixes were applied on USNR test plots. The conventional seed mix was modified slightly from the primary seed mix in Appendix C of the MMD permit modification 06-3 to accommodate the availability of seed and included 4 warm season grass, 5 cool season grass, 3 forb, and 4 shrub species (Table 1). An alternative seed mix deviated from the typical seed mix in Appendix C of Permit GR007RE to include a number of experimental species native to the Desert Southwest region. The alternative seed mix was comprised of 10 warm season grass, 6 cool season grass, 10 forb, and 6 shrub species (Table 2). For reference the number of seeds per square foot were similar for both seed mixes, but the experimental mix contained some species with larger seeds.

2.3.3 Mulching

Conventionally, Tyrone has applied mulch after seed placement. At the USNR, the timing of seeding and mulching varied among the test plot treatments. Mulch was applied prior to seeding on half the area and after seeding on the other half. Mulch was applied at a rate of approximately 2-tons/ac. The mulch was then crimped 3 to 4 inches into the cover using a disc harrow with straight coulter discs spaced approximately 6 to 8 inches apart. The crimping operation was performed on the contour.





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Table 1. Conventional S	Seed Mix used at the	USNR Test Plots
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Species	Common Name	lbs/ac
Warm Season Grass		
Bothriochloa barbinodis	Cane bluestem	0.3
Bouteloua curtipendula	Sideoats gramma	1.25
Bouteloua gracilis	Blue grama	0.25
Leptochloa dubia	Green sprangletop	0.40
Cool Season Grass		
Achnatherum hymenoides	Indian ricegrass	1.50
Agropyron dasystachyum	Streambank wheatgrass	1.00
Elymus elymoides	Bottlebrush squirreltail	1.25
Koeleria macrantha	Prairie Junegrass	0.10
Sporobolus cryptandrus	Sand dropseed	0.05
Shrubs		
Atriplex canescens	Fourwing saltbush	0.75
Chilopsis Linearis	Desert willow	0.75
Ericameria nauseosa	Rubber rabbit brush	0.30
Krascheninikovia lanata	Winterfat	0.50
Forbs		
Dalea candida	White prairie clover	0.4
Linum lewisii	Blue flax	0.12
Ratibida columnaris	Prairie coneflower	0.2
	PLS (Ibs/acre)	9.12

Note: lbs/ac = pounds per acre, PLS = pure live seed





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Table 2. Alternative Seed Mix used at the USNR Test Plots

Species	Common Name	lbs/ac
Warm Season Grass		
Aristida purpurea var. longiseta	Fendler threeawn	0.25
Bothriochloa barbinodis	Cane bluestem	0.10
Bouteloua curtipendula	Sideoats grama	1.00
Bouteloua rothrockii	Rothrock's grama	0.05
Eragrostis intermedia	Plains lovegrass	0.05
Heteropogon contortus	Tanglehead	0.25
Muhlenbergia montana	Mountain muhly	0.03
Schizachyrium scoparium	Little bluestem	0.90
Sporobolus airoides	Alkali sacaton	0.05
Sporobolus giganteus	Giant dropseed	0.05
Cool Season Grass		
Elymus elymoides	Bottlebrush squirreltail	1.00
Elymus glaucus	Blue wildrye	0.40
Hesperostipa neomexicana	New Mexico feathergrass	3.00
Poa secunda	Sandberg bluegrass	0.05
Sporobolus cryptandrus	Sand dropseed	0.02
Thinopyrum intermedium	Intermediate wheatgrass	1.00
Shrubs		
Acacia constricta	Whitethorn acacia	1.00
Acacia greggii	Catclaw acacia	2.00
Atriplex canescens	Fourwing saltbush	1.50
Encelia virginensis	Virgin River brittlebush	0.25
Ericameria nauseosa	Rubber rabbitbrush	0.20
Robinia neomexicana	New Mexico locust	2.50
Forbs		
Achillea millefolium var. occidentalis	Western yarrow	0.01
Artemisia ludoviciana	White sagebrush	0.05
Baileya multiradiata	Desert marigold	0.05
Erigeron speciosus	Aspen fleabane	0.05
Isocoma tenuisecta	Burroweed	0.05
Lotus rigidus	Deervetch	0.10
Oenothera pallida	Pale evening primrose	0.10
Penstemon palmeri	Palmer's penstemon	0.20
Senna covesii	Coues' cassia	0.25
Sphaeralcea coccinea	Scarlet globemallow	0.10
	PLS (lbs/acre)	16.61

Note: lbs/ac = pounds per acre, PLS = pure live seed



3.0 COVER CHARACTERISTICS

The configuration and physical and chemical characteristics of the cover materials were evaluated after placement on the test plots. The field and laboratory methods are discussed in Section 3.1. The results of the field observations are described in Section 3.2. Section 3.3 contains a summary of the chemical characteristics of the covers. The results of the physical and hydraulic testing are summarized in Sections 3.4 and 3.5. Section 3.6 provides information on the estimated water holding capacity for the cover materials and presents a generalized relationship for predicting water holding capacity based on material properties.

3.1 Methods

The field, laboratory, and computational methods associated with the cover material characterization are described in the following sections.

3.1.1 Field Methods

Five test pits were excavated and described on the test plots. The sample locations are shown on Figure 1. Five samples of the cover materials were also collected for physical and chemical analysis of the fine earth fraction (particles < 2mm in diameter). In addition, three samples were collected for soil hydraulic testing. The samples collected for fine-earth analysis were about 5 to 10 kg with the larger rock fragments (> 75 mm) removed. The samples collected for particle size analyses were placed directly in gallon-size plastic bags, while the samples for soil-hydraulic analyses were placed in 5-gallon airtight plastic buckets. The samples were shipped to the associated analytical laboratories at ambient temperature.

3.1.2 Laboratory

The soil hydraulic samples were analyzed at the Daniel B. Stephens & Associates (DBS&A) Laboratory in Albuquerque, NM. The chemical and particle size analyses were conducted at Energy Laboratories in Billings, MT. The bulk soil samples collected for fine-earth analysis were air-dried and passed through a 2 mm sieve at the laboratory. The analytical methods are listed in Table 3.

Because the cover materials contained rock fragments, the soil-hydraulic analyses were conducted on the fine-earth fraction. Column tests were performed on < 2mm subsamples packed to a specified target density based on established soil textural relationships (Soil Survey Division Staff, 1993). The target density for the laboratory samples was 1.4 g/cm³. Paired suction and water content measurements were made using hanging-column, pressure plate, water activity meter, and relative humidity box methods. The soil samples were subjected to at least 5 suction points ranging from near saturation (≈ 0 cm) to about 850,000 cm. The saturated hydraulic conductivity (K_{sat}) of the fine earth fraction samples was determined by the constant-head method. Laboratory reports are in Appendix A.





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Table 3. Soil Chemical, Physical and Hydraulic Test Methods

Test	Method
Saturated Paste pH	SLS 1954, Method 2 and 21a
Electrical Conductivity	SLS 1954, Method 3a and 4b
Particle Size Distribution	ASA 1982, Method 15-5
Saturation percentage	SLS 1954, Method 27a
N as Nitrate	ASA 1982, Method 33-8.1
Phosphorous (Olsen)	ASA 1982, Method 24-5.4
Dry Bulk Density:	ASTM D4531; ASTM D6836
Organic Matter	ASA 1982 Method 29-3.5.2
Moisture Content:	ASTM D2216; ASTM D6836
Calculated Porosity:	ASTM D2435; Klute, A. 1986. Porosity. Chp.18-2.1, pp. 444- 445, in A. Klute (ed.), Methods of Soil Analysis, American Society of Agronomy, Madison, WI
Saturated Hydraulic Conductivity: Constant Head: (Rigid Wall)	ASTM D 2434 (modified apparatus)
Hanging Column	ASTM D6836; Klute, A. 1986. Porosity. Chp.26, in A. Klute (ed.), Methods of Soil Analysis, American Society of Agronomy, Madison, WI
Pressure Plate	ASTM D6836; ASTM D2325
Water Potential (Dewpoint Potentiometer)	ASTM D6836; Rawlins, S.L. and G.S. Campbell, 1986. Water Potential: Thermocouple Psychrometry. Chp.24, pp. 597-619, in A. Klute (ed.), Methods of Soil Analysis, Part 1. American Society of Agronomy, Madison, WI.
Relative Humidity (Box)	Karathanasis & Hajek. 1982. Quantitative Evaluation of Water Absorption on Soil Clays. SSSA Journal 46:1324-1325; Campbell, G. and Gee. 1986. Water Potential: Miscellaneous Methods. Ch. 25, pp. 631-632, in A. Klute (ed.), Methods of Soil Analysis, American Society of Agronomy, Madison, WI
Moisture Retention Characteristics & Calculated Unsaturated Hydraulic Conductivity:	ASTM D6836; van Genuchten, M.T. 1980. A closed-form equation for predicting the hydraulic conductivity of unsaturated soils. SSSAJ 44:892-898; van Genuchten, M.T., F.J. Leij, and S.R. Yates. 1991. The RETC code for quantifying the hydraulic functions of unsaturated soils. Robert S. Kerr Environmental Research Laboratory, Office of Research and Development, U.S. Environmental Protection Agency, Ada, Oklahoma. EPA/600/2091/065. December 1991
Specific Gravity (Fine)	ASTM D854

Note:

SLS = Salinity Laboratory Staff

ASA = American Society of Agronomy

3.1.3 Soil Water Characteristic Curves

Soil water characteristic curves (SWCC) were developed using the RETC code (van Genuchten et al., 1991). The saturated water content (θ_s), residual water content (θ_r) and van Genuchten α and N parameters





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and relative hydraulic conductivity were estimated using the RETC code (van Genuchten et al., 1991). The SWCC's were developed for the fine-earth fraction and for the whole soils after correction of the fine-earth fraction data for rock fragments. The laboratory data were subsequently corrected to account for rock fragments representative of the whole soil. In particular, the volumetric water content of the fine-earth fraction at various matric suction values was proportionally reduced in accordance with the volume of rock fragments contained in the whole soil.

3.1.4 Water Holding Capacity Estimation

The water holding capacity was determined by subtracting the water held at the traditionally defined field capacity from water held at wilting point (USDA 2014). Field capacity was estimated as the water held at 100 cm (10 kPa) of suction and wilting point was estimated as the water held at 15,000 cm (1500 kPa) of suction (USDA, 2014). Because the cover materials are consistently sandy loams and generally contain between 40 and 60% rock fragments, they were considered coarse textured and field capacity was determined at 100 cm suction. The water content at field capacity and wilting point were determined numerically (rather than graphically) from the soil water characteristic curve functions developed for each sample.

3.2 Thickness and Structural Observations

Cover thickness and structure were assessed in 5 test pits distributed across the test plot area. The covers in the test pits all exceeded the 36 inch minimum requirement with range from 38 to 45 inches thick. Structurally, the covers were dominantly matrix supported with occasional and localized zones of clast supported. The cover materials were pushed in lifts and feathered down the slope to reduce clast supported zones and promotes gravity separation of the larger rock fragments, which were removed from the base of the slope.

3.3 Chemical Properties

The soil testing results indicate that there are no inherent chemical limitations for the growth of native plants. The cover materials are slightly alkaline (pH 7.6 to 7.7) and non-saline (EC < 2 dS/m). The organic matter, phosphorous, and nitrate nitrogen concentrations are considered adequate for the target plant species. The test results are summarized in the Table 4.



	Paste pH	Paste Extract EC	Organic Carbon	Phosphorus	Nitrate-N
Sample ID	s.u.	dS/m	%	t/ac	c-ft
UTPQA-1	7.7	0.5	< 0.1	12	8
UTPQA-2	7.7	0.4	< 0.1	8	8
UTPQA-3	7.6	0.5	< 0.1	8	8
LTPQA-4	7.7	0.5	< 0.1	8	8
LTPQA-5	7.7	0.6	< 0.1	12	8

Table 4. Chemical Characteristics of the USNR Cover Materials

3.4 Particle Size Distribution

The range in particle size distribution for the fine-earth fractions was relatively narrow with all the samples classified as sandy loams (Table 5). The rock fragment content ranged from 40 to 60 percent by volume and sizes ranged from gravel to stones. The saturation percentage data was relatively consistent increasing with clay content, suggesting that the samples are mineralogically similar.

Sample	USDA Texture	Particle Size Distribution (wt %)			Rock Fragments ²	Saturation Percentage
ID	Class ¹	Sand	Silt	Clay	(vol %)	%
UTPQA-1	SL	73	20	7	60	25.4
UTPQA-2	SL	73	19	8	55	25.3
UTPQA-3	SL	71	21	8	40	24.2
LTPQA-4	SL	71	19	10	50	26.2
LTPQA-5	SL	67	23	10	55	26.5

Table 5. Particle Size Distribution for the USNR Samples

Notes: 1) Texture = USDA texture class according to Soil Survey Division Staff (1993); SL = sandy loam 2) Rock fragments based on field volumetric estimates from test pits

3.5 Soil Hydraulic Properties

The saturated water content of the < 2 mm soil fraction was consistent among the samples, ranging between 0.48 and 0.51 cm³/cm³ (Table 6). The minor variations in saturated water content and other properties are not unexpected given the textural consistency of the materials (Section 4.1). The other soil hydrologic parameters (θ_r and van Genuchten α and N) compare well with standardized relationships among soil particle size and hydraulic properties of similarly textured soils (Rawls et al., 1982; Carsel and Parrish, 1988). The K_{sat} of the < 2 mm samples ranged from 8.9 x 10⁻² to 2.6 x 10⁻² cm/s (Table 6), which is the high end of the range expected for sandy loams when compared to typical published values (Klute and Dirksen, 1986). The post-consolidation bulk densities of the laboratory samples only increased slightly compared to the laboratory target densities indicating that the samples were near equilibrium levels at the target densities.





	Coturated	van Genuchten Coefficients				
Sample ID	Saturated Hydraulic Conductivity	θr	θs	α	N	Bulk Density
	(cm/s)	(cm³/cm³)		1/cm	Dimensionless	(g/cm³)
UTPQA-2	8.9E-02	0.00	0.48	0.103	1.29	1.44
UTPQA-3	7.0E-02	0.00	0.50	0.097	1.31	1.53
LTPQA-4	3.2E-02	0.00	0.50	0.092	1.29	1.52
T7ALRLC	2.6E-02	0.05	0.51	0.078	1.39	1.51

Table 6. Soil Hydraulic Properties of USNR Cover Materials Fine-Earth Fraction

Notes: 1) θr = residual water content; θs = saturated water content

cm/s = centimeters per second; mm = millimeters; cm³ = cubic centimeters; g/cm³ = grams per cubic centimeter

	Coturated					
Sample ID	Saturated Hydraulic Conductivity	θr	θs	α	N	Rock Fragments
	(cm/s)	(cm³/cm³)		1/cm	Dimensionless	(vol %)
UTPQA-2	1.6E-02	0.00	0.22	0.103	1.29	55
UTPQA-3	2.0E-02	0.00	0.30	0.098	1.31	40
LTPQA-4	1.0E-02	0.00	0.25	0.093	1.30	55
T7ALRLC	7.2E-03	0.00	0.28	0.115	1.27	45

Notes: 1) θ_r = residual water content; θ_s = saturated water content

2) cm/s = centimeters per second; mm = millimeters; cm³ = cubic centimeters; g/cm³ = grams per cubic centimeter

The SWCC's for each sample are provided in Appendix B. The SWCC graphs display the curves for the fine-earth fraction and for the whole soil assuming the rock fragment content for each test pit based on the field descriptions (Table 7).

3.6 Water Holding Capacity

The estimated water holding capacity of the fine-earth fraction ranged from about 2.1 to 2.4 in/ft (Table 8). The water holding capacity on a whole soil basis (corrected for the field rock fragment contents) ranged from about 1.0 to 1.4 in/ft reflecting the reduction of water holding capacity associated with the rock fragments. The average water holding capacity of the fine-earth fraction was 2.23 in/ft based on the 4 samples tested.





Sample ID	Water Holdi (in	• • •	Rock Fragment Content ²	
	Fine Earth Whole Soil		(vol %)	
UTPQA-2	2.21	1.00	55	
UTPQA-3	2.30	1.38	40	
LTPQA-4	2.35	1.17	50	
T7ALRLC	2.07	1.28	45	

Table 8. Estimated Water Holding Capacity of USNR Cover Samples

Notes: 1) Whole soil based on RETC adjusted for field rock fragments

2) Total rock fragments based on field estimates for profile

Because the water holding capacity of the cover is directly related to the quantity of rock fragments, a generalized relationship was developed using the average water holding capacity of the fine earth fraction corrected for various rock fragment concentrations (Figure 3). The line is described by the following equation;

Field WHC = (FE WHC) x (1- VRF)

Where the FE WHC is the fine-earth water holding capacity, which is assumed to be 2.23 in/ft (average of materials tested), and VRF is the volumetric rock fragment content. This relationship will allow determination of the water holding capacity of the cover using soil textural (i.e., rock fragment) data, which is collected as part of the cover quality control process. For example, if the cover material in a reclamation area had an average rock fragment content of 45% (0.45) the field water holding capacity would be estimated to be 1.4 in/ft (i.e., 2.23 x 1-0.45).

This analysis indicates that the Little Rock cover materials will achieve the Copper Rule requirements (≈ 2.6 inches) with the 3-foot thick cover. The cover material on the test plots had an average rock fragment of about 48%. Thus, the cover materials on the test plots have a water holding capacity that exceeds the 20.6.7.F (2) requirements.



4.0 EROSION MONITORING

Erosion is the detachment and movement of soil by wind or water. Soil erosion rates vary temporally in response to a number of controlling factors. The major factors affecting erosion include the amount, duration, and intensity of rainfall, soil physical characteristics, nature of the soil surface, vegetation, litter, and rock cover, and the gradient, shape, and length of slope. Soil erosion at mine sites is typically predicted using models that incorporate these factors (Toy and Foster 1998). Because erosion is episodic, short-term measurements are typically poorly correlated to the long-term prediction provided by models (Weltz et al. 1998). For instance, erosion rates are expected to be highest during the vegetation establishment period and may not reflect long-term rates. Similarly, variations in weather events can strongly affect the erosion process. Because of the large size of the plots, sediment traps were considered impractical as a means to measure erosion. Soil erosion was measured using a portable erosion meter (McCool et al 1981; Kincaid and Williams 1966). The erosion measurements were made using the erosion meter described in Golder (2009).

The erosion transects were installed and baseline monitoring was conducted in June 2016. A subsequent monitoring episode was conducted in December 2016 to assess changes in surface topography. Figure 4 shows the location of the erosion monitoring stations. Cross-section plots of the relative changes in the ground surface from the baseline measurements in 2016 are included in Appendix C (Figures C-1 to C-2). Photographs of the monitoring locations compared to the baseline conditions are included in Appendix D.

4.1 Changes in Surface Elevation and Erosion

Changes in soil surface elevations were evaluated assuming each erosion meter station represented a separate sample. For each station, the average change in surface elevation from the initial measurement was calculated using points that intersected soil, rock fragments, and litter. Positive changes in surface elevation indicate degradation and negative changes indicate aggradation. The four individual stations on each transect were averaged to determine the change in elevation for each transect. The two transects were averaged to estimate the change in surface elevation for the test plot as a whole considering that the vegetation was not substantively different among the mulching treatments.

The relative changes in ground surface elevation were minimal considering that the test plots is still in the vegetation establishment phase. The relative change in ground surface from baseline was 1.7 mm on the south transect (1:2.98 gradient) and 0.9 mm on the north transect (1:3.2 gradient). The average for the test plot was 1.3 mm. This represents an estimated erosion rate of about 8.5 tons/ac for the first measurement period, which is within the measurement error of this method (Golder, 2009).

The erosion transects were constructed and baseline conditions were measured about 1 year after seeding and mulching. The amount of surface aggradation or degradation that occurred during the period between mulching and the baseline measurement (i.e., summer of 2015) is impossible to quantify. Thus, the erosion





estimates provided in this section do not represent the entire period of reclamation. Because the straw mulch was largely intact through the summer of 2015 and persisted locally with diminishing effectiveness into 2016, we believe that the actual erosion is likely to be somewhat, but probably not substantially higher.

Examination of the station cross-sections suggests that rill erosion is more prevalent than sheet erosion on the slopes. The zone of apparent riling tends to occur near the mid-point of the slope, which is consistent with erosion processes on natural hillslopes.

Station #	USNR-South	Average		
1 (near crest)	1.5	0.5	1.0	
2	0.2	2.6	1.4	
3	5.0	1.6	3.3	
4 (near toe)	0.0	-1.0	-0.5	
Transect Average	1.7	1.7 0.9		
Test Plot Average			1.3	

Table 9. Average Change in Ground Surface Elevation of the USNR Erosion Transects

Notes:

Changes in elevation are from baseline in millimeters (mm)

Negative values indicate surface aggradation

Positive values indicate surface degradation



5.0 **VEGETATION MONITORING**

Vegetation attributes on the test plots were evaluated qualitatively in 2016 with emphasis on plant establishment. Because weather conditions have an important impact on plant establishment, the precipitation records from the Little Rock meteorological station are provide in this section. Table 10 lists the monthly and annual precipitation for 2015, and 2016. Compared to the long-term regional records (Ft Bayard with about 16 inches), annual precipitation was somewhat, but not drastically, below average for 2015 and slightly above normal for 2016. The daily distribution of precipitation is shown in Figure 5. Overall, the prevailing precipitation is considered favorable, but not exceptionally wet.

	2014	2015	2016
January	0.00	2.22	1.03
February	0.00	0.44	0.31
March	1.12	0.82	0.00
April	0.33	0.31	0.54
Мау	0.03	0.52	0.15
June	0.15	1.14	0.61
July	0.83	2.40	2.43
August	4.80	2.57	5.53
September	3.04	1.14	3.34
October	1.63	0.25	0.27
November	1.28	1.15	0.26
December	1.12	1.44	2.54
Annual	14.33	14.40	17.01

Table 10. Monthly and Annual Precipitation at the Little Rock Met Station

The status of the vegetation in 2016 is depicted in Figures 6 through 9 for the mulching and seeding variations. In general, the vegetation on all treatments is performing adequately for this stage of reclamation with average plant density exceeding 1 plant/square foot. There were no discernable differences in canopy cover on the plots that were seeded either before or after mulching. Species composition varied among the experimental and conventional seed mix treatments, although the early stage of reclamation made definitive identification of some species difficult. The future vegetation studies required by the work plan and Permit will be necessary to better define species response of the conventional and experimental seed mix treatments. Nonetheless, species with a notable response on the experimental seed mix plots included whitethorn and catclaw acacia, white sagebrush, Palmer's penstemon and deer vetch. Coues' senna, which was observed on the experimental seed mix treatment in the fall of 2015, was not present in 2016.





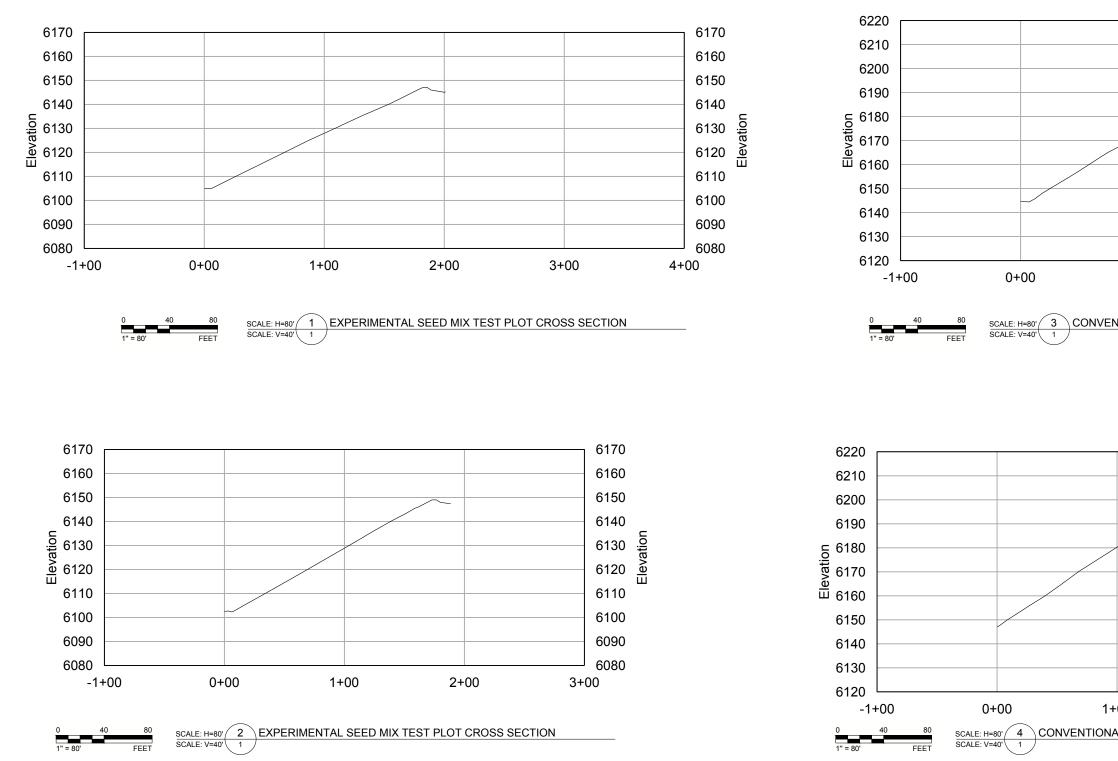
6.0 **REFERENCES**

- American Society of Agronomy. 1986. Methods of Soil Analysis Part 1: Physical and Mineralogical Methods. American Society of Agronomy, Madison, WI.
- Carsel, R. F. and R. S. Parrish. 1988. Developing joint probability distributions of soil water retention characteristics. Water Resour. Res. 24: 755-769.
- Golder 2009. No. 1 Stockpile Test Plots Annual Report- Report No. 3. Prepared for Freeport-McMoRan Tyrone Inc. February 27, 2009.
- Golder. 2014. Little Rock Mine and Tyrone Mine Leach Cap Test Plots Status Report 2013 Reseeding. Technical Memorandum. October, 2014
- Kincaid, D.R., and G. Williams. 1966. Rainfall Effect on Soil Surface Characteristics Following Range Improvement Treatments. J. Range Manage. 19: 346-351.
- Klute, A., and C. Dirksen. 1986. Hydraulic conductivity and diffusivity: Laboratory methods. In: A. Klute (ed). Methods of Soil Analysis. Part 1-Physical and Mineralogical Methods, 2nd Edition. Soil Sci. Soc. Am., Madison, WI. Agron. 9:687-732.
- McCool, D.K., M.G. Dossett, and S.J. Yecha. 1981. A Portable Rill Meter for Field Measurement of Soil Loss. Erosion and Sediment Transport Measurement, Proc of the Florence Symp., IAHS Publ. no. 133 pp. 479-484.
- Rawls, W.J., D.L. Brakensiek, and K.E. Saxton. 1982. Estimating soil water properties. Transactions ASAE 25:1316-1320, 1325.
- Salinity Laboratory Staff. 1954. Diagnosis and improvement of saline and alkali soils. Agricultural Handbook No. 60. USDA-Agricultural Research Service. US Government Printing Office, Washington, D.C.
- Soil Survey Division Staff, 1993. Soil survey manual. Handbook No. 18, 2nd ed. USDA-Soil Conservation Service. US Government Printing Office, Washington, D.C.
- Toy, T.J., and G. R. Foster. 1998. Guidelines for the use of the Revised Universal Soil Loss Equation (RUSLE v. 1.06) on mined lands, construction sites, and reclaimed lands. J.R. Galetovic (ed.) Office of Surface Mining, Denver, CO.
- USDA Natural Resource Conservation Service (NRCS). 2014. National Soil Survey Handbook. Title 430-VI. Section 618.6.D.3 Available online. Accessed 3/28/2014.
- van Genuchten, M.Th., F.J. Leij, and S.R. Yates. 1991. The RETC code for quantifying the hydraulic functions of unsaturated soils. Robert S. Kerr Environmental Research Laboratory, Office of Research and Development, U.S. Environmental Protection Agency. Ada, Oklahoma. EPA/600/2091/065. December 1991.
- Weltz, M.A., M.R. Kidwell, and H.D. Fox. 1998. Influence of Abiotic and Biotic Factors in Measuring and Modeling Soil Erosion on Rangelands: State of knowledge. J. Range Manage. 51:482-495.Sanchez and Wood 1987



FIGURES





CLIENT FREEPORT McMoRan TYRONE INC.

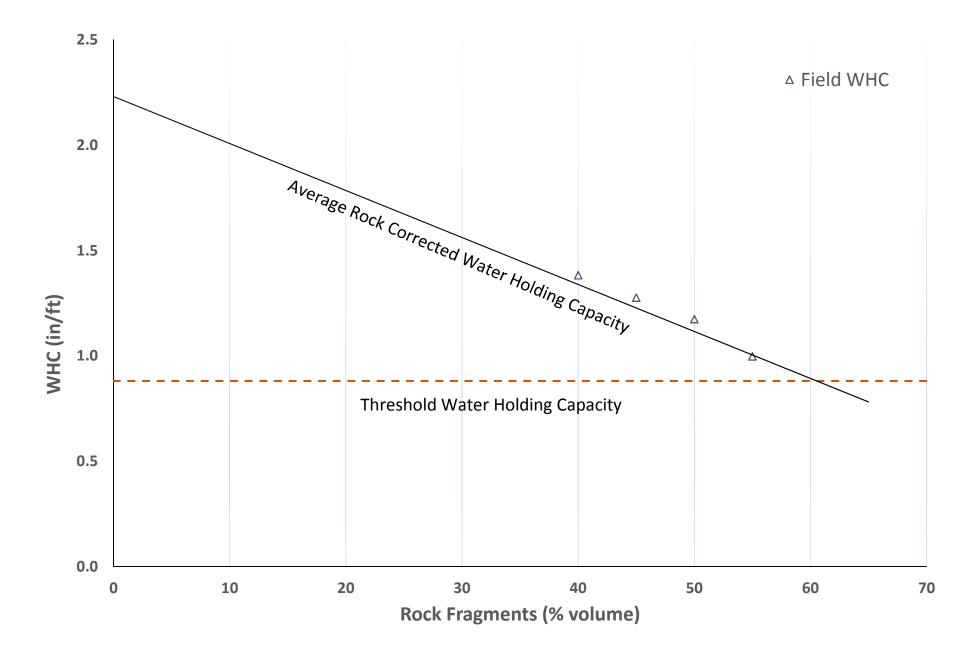
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CONSULTANT

GRANT COUNTY, NEW MEXICO

	YYYY-MM-DD	2017-02-22
È.	DESIGNED	LM
Golder	PREPARED	CM
Associates	REVIEWED	LM
	APPROVED	LM

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SEED MIX	TEST PLOT CROSS SECT	6130 6120 3+00	
	TEST PLOT CROSS SECT	6130 6120 3+00	
PROJEC USNR	TEST PLOT CROSS SECT	6130 6120 3+00	FIGURE





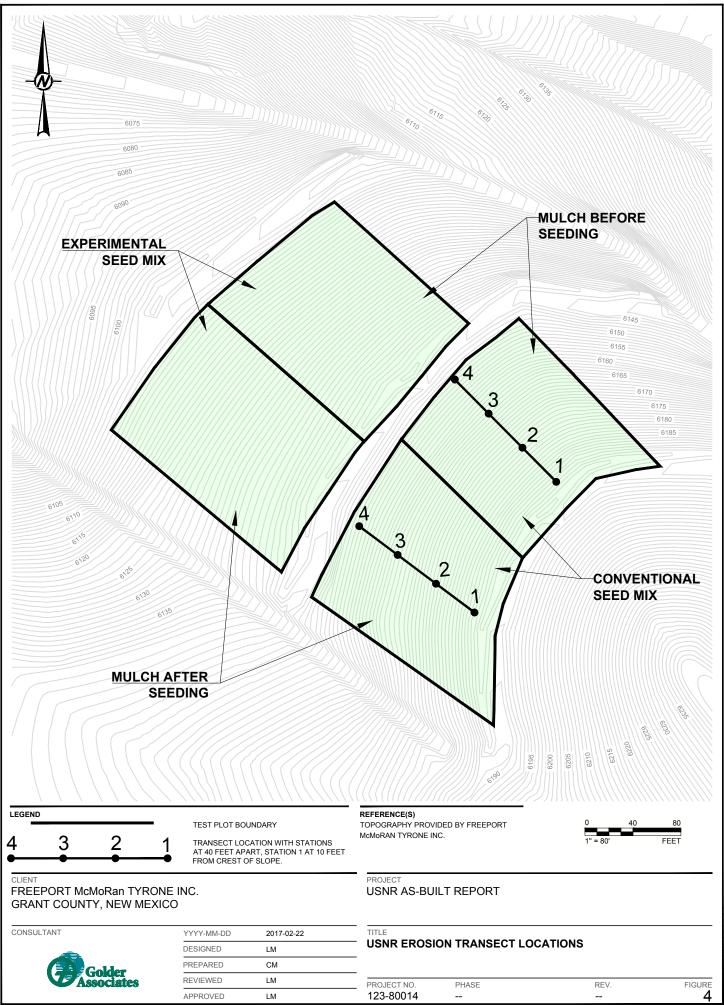


Figure 5: Daily Precipitation at the Little Rock Met Station

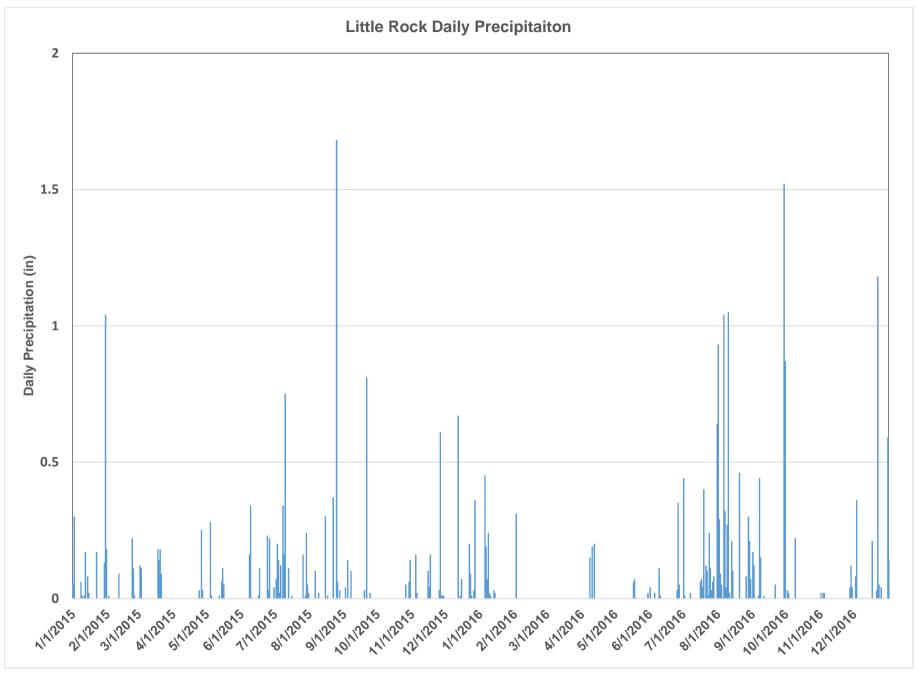








Figure 6. Status of vegetation on the seeding after mulching conventional treatment. (October 2016)



Figure 7. Status of vegetation on the seeding before mulching treatment. (Conventional mix. October 2016)





Figure 8. Status of vegetation on the seeding before mulching treatment. (Experimental mix. June 2016)



Figure 9. Status of vegetation on the seeding after mulching treatment. (Experimental mix. June 2016)



APPENDIX A LABORATORY REPORTS

ENERGY LABORATORIES



ANALYTICAL SUMMARY REPORT

March 11, 2016

Golder Associates Inc 5200 Pasadena NE Ste C Albuquerque, NM 87113

Work Order: B16030333

Project Name: USNR Test Plots

Energy Laboratories Inc Billings MT received the following 5 samples for Golder Associates Inc on 3/3/2016 for analysis.

Lab ID	Client Sample ID	Collect Date	Receive Date	Matrix	Test
B16030333-001	USNR UTPQA-1	05/28/15 0:00	03/03/16	Soil	Coarse Fragments Conductivity, Saturated Paste Extract Nitrate as N, KCL Extract Organic Carbon/Matter Walkley- Black pH, Saturated Paste Phosphorus-Olsen Saturated Paste Extraction Particle Size Analysis Saturation Percentage Texture
B16030333-002	USNR UTPQA-2	05/28/15 0:00	03/03/16	Soil	Same As Above
B16030333-003	USNR UTPQA-3	05/28/15 0:00	03/03/16	Soil	Same As Above
B16030333-004	USNR LTPQA-4	05/28/15 0:00	03/03/16	Soil	Same As Above
B16030333-005	USNR LTPQA-5	05/28/15 0:00	03/03/16	Soil	Same As Above

The analyses presented in this report were performed by Energy Laboratories, Inc., 1120 S 27th St., Billings, MT 59101, unless otherwise noted. Any exceptions or problems with the analyses are noted in the Laboratory Analytical Report, the QA/QC Summary Report, or the Case Narrative.

The results as reported relate only to the item(s) submitted for testing.

If you have any questions regarding these test results, please call.

Report Approved By:



Billings, MT 800.735.4489 • Casper, WY 888.235.0515 College Station, TX 888.690.2218 • Gillette, WY 866.686.7175 • Helena, MT 877.472.0711

LABORATORY ANALYTICAL REPORT

Prepared by Billings, MT Branch

Client:Golder Associates IncProject:USNR Test PlotsWorkorder:B16030333

Report Date: 03/11/16 **Date Received:** 03/03/16

	Analysis	Coarse Frags	Sand	Silt	Clay	Texture	pН	COND	Saturation	Organic Carbon	Phos, Olsen	Nitrate as N
	Units	%	%	%	%		s_u_	mmhos/cm	%	%	mg/kg	mg/kg
Sample ID	Client Sample ID	Results	Results	Results	Results	Results	Results	Results	Results	Results	Results	Results
B16030333-001	USNR UTPQA-1	62	73	20	7	SL	7.7	0.5	25.4	< 0.1	3	2
B16030333-002	USNR UTPQA-2	55	73	19	8	SL	7.7	0.4	25.3	< 0.1	2	2
B16030333-003	USNR UTPQA-3	53	71	21	8	SL	76.0	0.5	24.2	< 0.1	2	2
B16030333-004	USNR LTPQA-4	55	71	19	10	SL	7.7	0.5	26.2	< 0.1	2	2
B16030333-005	USNR LTPQA-5	61	67	23	10	SL	7.7	0.6	26.5	< 0.1	3	2



Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Analyte		Result	Units	RL	%REC L	Low Limit	High Limit	RPD	RPDLimit	Qual
Method:	ASA15-5								Batch	: R257811
Lab ID:	B16030336-001A DUP	Sample Duplic	ate			Run: MISC	-SOIL_160311A		03/1 <i>°</i>	1/16 10:18
Sand		74	%	1.0				1.4	30	
Silt		19	%	1.0				5.1	30	
Clay		7.0	%	1.0				0.0	30	
Lab ID:	LCS-1603111018	Laboratory Co	ntrol Sample			Run: MISC	-SOIL_160311A		03/1 ⁻	1/16 10:18
Sand		44	%	1.0	107	70	130			
Silt		37	%	1.0	106	70	130			
Clay		19	%	1.0	79	70	130			



Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Analyte		Result	Units	RL	%REC	Low Limit	High Limit	RPD	RPDLimit	Qual
Method:	ASA24-5						Batch	n: OM_3·	-11-2016_07	-54-09AM
Lab ID:	LCS	Laboratory Co	ntrol Sample Run: FIA205-B_160311A			03/11/16 07:55				
Phosphorus	, Olsen	7.4	mg/kg	1.0	111	70	130			
Lab ID:	B16030333-001ADUP	Sample Dupli	cate			Run: FIA20)5-B_160311A		03/11	/16 08:04
Phosphorus	, Olsen	2.4	mg/kg	1.0				8.4	30	
Lab ID:	B16030333-001AMS	Sample Matrix	k Spike			Run: FIA20)5-B_160311A		03/11	/16 08:05
Phosphorus	, Olsen	13	mg/kg	1.0	101	70	130			



Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Analyte	Result Units	RL %REC Low Limit High Limit R	PD RPDLimit Qual
Method: ASA29-3			Batch: R257811
Lab ID: B16030333-001A DUP	Sample Duplicate	Run: MISC-SOIL_160311A	03/11/16 10:12
Organic Carbon	0.0700 %	0.10	30
Lab ID: LCS-1603111012	Laboratory Control Sample	Run: MISC-SOIL_160311A	03/11/16 10:12
Organic Carbon	1.26 %	0.10 79 70 130	



Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Analyte	Result Units	RL %REC Low Limit High Limit RPD RPDLimit Qual
Method: ASA33-8		Batch: OM_3-10-2016_11-41-30AM
Lab ID: LCS Nitrate as N, KCL Extract	Laboratory Control Sample 8.10 mg/kg	Run: FIA205-B_160310A 03/10/16 11:42 1.0 109 70 130
Lab ID:B16030336-005ADUPNitrate as N, KCL Extract	Sample Duplicate 2.68 mg/kg	Run: FIA205-B_160310A03/10/16 11:561.09.430
Lab ID: B16030336-005AMS Nitrate as N, KCL Extract	Sample Matrix Spike 4.91 mg/kg	Run: FIA205-B_160310A03/10/16 11:561.011850150



Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Analyte	Result Units	RL	%REC Low Limi	t High Limit	RPD	RPDLimit	Qual
Method: ASAM10-3						Batch:	R257811
Lab ID: B16030333-005A DUP Conductivity, sat. paste	Sample Duplicate 0.540 mmhos/cm	0.10	Run: MIS	C-SOIL_160311A	1.8	03/11 30	/16 10:10
Lab ID: LCS-1603111010 Conductivity, sat. paste	Laboratory Control Sample 11.9 mmhos/cm	0.10	Run: MIS 88 70	C-SOIL_160311A 130		03/11	/16 10:10



QA/QC Summary Report

Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Report Date: 03/11/16 **Work Order:** B16030333

Analyte	Result Units	RL %REC Low Limit High Limit RPD RPDLimit Qual
Method: ASAM10-3.2		Batch: R25781
Lab ID: B16030333-005A DUP pH, sat. paste	Sample Duplicate 7.60 s.u.	Run: MISC-SOIL_160311A 03/11/16 10:1 0.10 1.3 10
Lab ID: LCS-1603111010 pH, sat. paste	Laboratory Control Sample 7.00 s.u.	Run: MISC-SOIL_160311A 03/11/16 10:1 0.10 99 90 110



QA/QC Summary Report

Prepared by Billings, MT Branch

Client: Golder Associates Inc

Project: USNR Test Plots

Report Date: 03/11/16 **Work Order:** B16030333

Analyte		Result	Units	RL	%REC	Low Limit	High Limit	RPD	RPDLimit	Qual
Method:	USDA27a								Batch:	R257811
Lab ID: Saturation	B16030333-005A DUP	Sample Duplica 28.2	ite %	0.10		Run: MISC	-SOIL_160311A	6.2	03/11 20	/16 10:10
Lab ID: Saturation	LCS-1603111010	Laboratory Con 36.9	trol Sample %	0.10	97	Run: MISC 50	-SOIL_160311A 150		03/11	/16 10:10



Work Order Receipt Checklist

Golder Associates Inc

B16030333

Login completed by:	Cindy Rohrer	Date Received: 3/3/2016					
Reviewed by:	BL2000\jmueller		Re	ceived by: car			
Reviewed Date:	3/4/2016		Car	rier name: FedEx Ground			
Shipping container/cooler in	good condition?	Yes 🗹	No 🗌	Not Present			
Custody seals intact on all s	Yes	No 🗌	Not Present √				
Custody seals intact on all s	Yes	No 🗌	Not Present 🗹				
Chain of custody present?	Yes 🗹	No 🗌					
Chain of custody signed who	Yes 🗹	No 🗌					
Chain of custody agrees with	Yes 🗹	No 🗌					
Samples in proper container	/bottle?	Yes 🗹	No 🗌				
Sample containers intact?		Yes 🗹	No 🗌				
Sufficient sample volume for	r indicated test?	Yes 🗹	No 🗌				
All samples received within I (Exclude analyses that are c such as pH, DO, Res CI, Su	considered field parameters	Yes 🗹	No 🗌				
Temp Blank received in all s	hipping container(s)/cooler(s)?	Yes	No 🗌	Not Applicable 🗹			
Container/Temp Blank temp	erature:	11.0°C No Ice					
Water - VOA vials have zero	headspace?	Yes	No 🗌	Not Applicable			
Water - pH acceptable upon	receipt?	Yes	No 🗌	Not Applicable			

Standard Reporting Procedures:

Lab measurement of analytes considered field parameters that require analysis within 15 minutes of sampling such as pH, Dissolved Oxygen and Residual Chlorine, are qualified as being analyzed outside of recommended holding time.

Solid/soil samples are reported on a wet weight basis (as received) unless specifically indicated. If moisture corrected, data units are typically noted as –dry. For agricultural and mining soil parameters/characteristics, all samples are dried and ground prior to sample analysis.

Contact and Corrective Action Comments:

None

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RGY	frust our People. 1
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Chain of Custody & Analytical Request Record

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<u>ww.energylab.com</u>

Bill To: 123-80014 8 Rian30303-000 002 82 Fa MUST be contacted prior to standard unless marked as RUSH sample submittal for charges and scheduling -All turnaround times are See Instructions Page bhul ELILAB (D) Leveny Use Off Energy Laboratories ď Receipt Number (cash/check only) RUSH Page 1 A K Signature 1 Signature Comments TAT See Attached 9:30 PaterTime 3.3-1-10 Amount > Cravel Content >2mm > > > > のないの Date/Time 69 > Nitrate as N, KCL Extract > > Analysis Requested Report Information [if different than Account Information] EDD/EDT (contact laboratory)
 Other > > uəsiO-surordsord > > Walkley/Niack Payment Type Received by Laboratory (print) Check - nodreO oinegrO > ` Saturation Percentage > `` Cash Received by (print) yelo, tilis ,bnea Particle Size Analysis: > $\mathbf{>}$ > ` 8 Conductivity, sat. pasate ` ` > \$€ 5 ≻ > > > > PH, Saturated Paste Special Report/Formats (See Codes Above) Matrix Company/Name Mailing Address Matrix Codes City, State, Zip B - Bioassay V - Vegetation DW - ^{Drinking} Water W- Water S - Sails/ Solids 0 - Other A - Air S တ ဟ S S Contact Phone Number of Containers Signature A Email d ng Doug_Romig@Golder.com;Drichelle_Pierce@Golder.co Email ° C Lime Lime 2/24/ 16 15:14 Date/Time □ Unpracessed ore (NOT ground or refined)* Collection Sampler Phone (505) 821-3043 EPA/State Compliance Receive Report CHard Copy Bottle Order Date 5/28/15 5/28/15 5/28/15 5/28/15 5/28/15 √ Intact Date Ξ Project Name, PWSID, Permit, etc. USNR Test Plots Albuquerque, NM 87113-2208 Seals C E MINING CLIENTS, please indicate sample type. "If ore has been processed or refined, call before sending. Mailing Address 5200 Pasadena NE, Ste. C Account Information (Billing information) Z Custed Sample Identification OEmail ≻ (Name, Location, Interval, etc.) Company/Name Golder Associates Kylc Kic HC (505) 821-3043 Quote Sample Origin State New Mexico Doug Romig Cooler ID(s) Receive Invoice Ellard Copy rouished by Sampler Name Doug Romig Byproduct 11 (e)2 material Project Information **USNR UTPQA-1 USNR UTPQA-2 USNR UTPQA-3 USNR LTPQA-4 USNR LTPQA-5** Record MUST be signed City, State, Zip Fell, C ^ourchase Order Shipped By Custody Contact Phone Email ₽ ĉ ŝ σ,

In certain circumstances, samples submitted to Energy Laboratories, Inc. may be subcontracted to other certified laboratories in order to complete the analysis requested. This serves as notice of this possibility. All subcontracted data will be clearly notated on your analytical report.

DANIEL B. STEPHENS & ASSOCIATES, INC.

Laboratory Report for Golder Associates, Inc.

USNR, 1303098

April 13, 2016



Daniel B. Stephens & Associates, Inc.

4400 Alameda Blvd. NE, Suite C • Albuquerque, New Mexico 87113

April 13, 2016



Lewis Munk Golder Associates, Inc. 5200 Pasadena NE, Suite C Albuquerque, NM 87113 (505) 821-3043

Re: DBS&A Laboratory Report for the Golder Associates, Inc., USNR 1303098 Project

Dear Mr. Munk:

Enclosed is the report for the Golder Associates, Inc. USNR 1303098 project samples. Please review this report and provide any comments as samples will be held for a maximum of 30 days. After 30 days samples will be returned or disposed of in an appropriate manner.

All testing results were evaluated subjectively for consistency and reasonableness, and the results appear to be reasonably representative of the material tested. However, DBS&A does not assume any responsibility for interpretations or analyses based on the data enclosed, nor can we guarantee that these data are fully representative of the undisturbed materials at the field site. We recommend that careful evaluation of these laboratory results be made for your particular application.

The testing utilized to generate the enclosed report employs methods that are standard for the industry. The results do not constitute a professional opinion by DBS&A, nor can the results affect any professional or expert opinions rendered with respect thereto by DBS&A. You have acknowledged that all the testing undertaken by us, and the report provided, constitutes mere test results using standardized methods, and cannot be used to disqualify DBS&A from rendering any professional or expert opinion, having waived any claim of conflict of interest by DBS&A.

We are pleased to provide this service to Golder Associates, Inc. and look forward to future laboratory testing on other projects. If you have any questions about the enclosed data, please do not hesitate to call.

Sincerely,

DANIEL B. STEPHENS & ASSOCIATES, INC. SOIL TESTING & RESEARCH LABORATORY

John

Joleen Hines Laboratory Supervising Manager

Enclosure

Daniel B. Stephens & Associates, Inc. Soil Testing & Research Laboratory 4400 Alameda Blvd. NE, Suite C Albuquerque, NM 87113

Summaries



Summary of Tests Performed

				S	aturate	ed																
	In	Initial Soil		н	lydraul	ic				Moi	sture				F	Particl	е	Spe	cific	Air		
Laboratory	Pr	opert	ies ¹	Co	nductiv	/ity ²			(Charac	teristi	cs ³				Size ⁴		Gra	vity ⁵	Perm-	Atterberg	Proctor
Sample Number	G	VM	VD	СН	FH	FW	HC	PP	FP	DPP	RH	EP	WHC	K _{unsat}	DS	WS	Н	F	С	eability	Limits	Compaction
T7ALRLC-Comp (<2mm, 1.4g/cc)	Х	х		х			х			Х	х			Х								
UTPQA-2 (<2mm, 1.4g/cc)	Х	х		х			х			х	х			х								
UTPQA-3 (<2mm, 1.4g/cc)	Х	х		х			х			х	х			х								
LTPQA-4 (<2mm, 1.4g/cc)	Х	х		х			х			Х	Х			Х								

¹ G = Gravimetric Moisture Content, VM = Volume Measurement Method, VD = Volume Displacement Method

² CH = Constant Head Rigid Wall, FH = Falling Head Rigid Wall, FW = Falling Head Rising Tail Flexible Wall

³ HC = Hanging Column, PP = Pressure Plate, FP = Filter Paper, DPP = Dew Point Potentiometer, RH = Relative Humidity Box,

EP = Effective Porosity, WHC = Water Holding Capacity, Kunsat = Calculated Unsaturated Hydraulic Conductivity

⁴ DS = Dry Sieve, WS = Wet Sieve, H = Hydrometer

⁵ F = Fine (<4.75mm), C = Coarse (>4.75mm)



Notes

Sample Receipt:

Four samples, each in a full 5-gallon bucket sealed with a lid, were hand delivered on February 29, 2016. All samples were received in good order.

Sample Preparation and Testing Notes:

Particles larger than 2mm were removed from each sample by splitting the material over a #10 sieve after gently breaking up larger clods by hand. Sample T7ALRLC-Comp was processes at the as received moisture content, and the remaining three samples were processed after a short air drying period in order to facilitate the splitting process. The <2mm fraction from each sample was then remolded into a testing ring to target a dry bulk density of 1.40 g/cm³, each at the respective as processed moisture content. Each remolded sub-sample ID was annotated with the actual remold density achieved (in g/cm³), and with "<2mm" to indicate that the <2mm fraction was used for testing. The remolded <2mm sub-samples were subjected to initial properties analysis, saturated hydraulic conductivity testing, and the hanging column and pressure chamber portions of the moisture retention testing. Additional <2mm material was obtained for the dewpoint potentiometer and relative humidity chamber portions of the moisture retention testing.

Volumetric water contents were adjusted for changes in volume, where applicable. Due to the irregularities formed on the sample surfaces during settling, volume measurements obtained after the initial reading should be considered estimates.

Oversize correction calculations are presented since the >2mm fraction removed was greater than 5% of the bulk sample mass. The percentages of coarse (>2mm) and fine (<2mm) fractions used in the calculations are based on the initial splitting process. The percentage of <2mm material would be greater if the material had been soaked and washed during the splitting process.

Porosity calculations are based on the use of an assumed specific gravity value of 2.65.

Summary of Sample Preparation/Volume Changes

	Target Remold Parameters ¹		Actual Remold Data			Volume Change Post Saturation ²				Volume Change Post Drying Curve ³				
	Dry Bulk Density	Dry Bulk Density	Moist. Cont.	Dry Bulk Density	Dry Bulk Density	% of Target Density	Dry Bulk Density	Dry Bulk Density	% Volume Change	% of Initial Density	Dry Bulk Density	Dry Bulk Density	% Volume Change	% of Initial Density
Sample Number	(g/cm ³)	(pcf)	(%, g/g)	(g/cm ³)	(pcf)	(%)	(g/cm ³)	(pcf)	(%)	(%)	(g/cm ³)	(pcf)	(%)	(%)
T7ALRLC-Comp (<2mm, 1.4g/cc)	1.40	87.4	2.6	1.40	87.44	100.1%	1.40	87.44		100.0%	1.44	90.07	-2.9%	103.0%
UTPQA-2 (<2mm, 1.4g/cc)	1.40	87.4	9.0	1.40	87.59	100.2%	1.40	87.59		100.0%	1.46	90.91	-3.7%	103.8%
UTPQA-3 (<2mm, 1.4g/cc)	1.40	87.4	8.2	1.40	87.68	100.3%	1.40	87.68		100.0%	1.45	90.50	-3.1%	103.2%
LTPQA-4 (<2mm, 1.4g/cc)	1.40	87.4	7.4	1.40	87.62	100.2%	1.40	87.62		100.0%	1.48	92.36	-5.1%	105.4%

¹Target Remold Parameters: Provided by the client: Remold <2mm fraction to target 1.40 g/cm³.

²Volume Change Post Saturation: Volume change measurements were obtained after saturated hydraulic conductivity testing.

³Volume Change Post Drying Curve: Volume change measurements were obtained throughout hanging column and pressure plate testing. The 'Volume Change Post Drying Curve' values represent the final sample dimensions after the last pressure plate point.

Notes:

"+" indicates sample swelling, "-" indicates sample settling, and "---" indicates no volume change occurred.



	As Re	eceived	Rem	olded	Dry Bulk	Wet Bulk	Calculated
Sample Number	Gravimetric (%, g/g)	Volumetric (%, cm ³ /cm ³)	Gravimetric (%, g/g)	Volumetric (%, cm ³ /cm ³)	Density (g/cm ³)	Density (g/cm ³)	Porosity (%)
T7ALRLC-Comp (<2mm, 1.4g/cc)	NA	NA	2.6	3.6	1.40	1.44	47.1
UTPQA-2 (<2mm, 1.4g/cc)	NA	NA	9.0	12.6	1.40	1.53	47.1
UTPQA-3 (<2mm, 1.4g/cc)	NA	NA	8.2	11.6	1.40	1.52	47.0
LTPQA-4 (<2mm, 1.4g/cc)	NA	NA	7.4	10.3	1.40	1.51	47.0

Summary of Initial Moisture Content, Dry Bulk Density Wet Bulk Density and Calculated Porosity

NA = Not analyzed



Summary of Saturated Hydraulic Conductivity Tests

		K _{sat}	Oversize Corrected K _{sat}	Method of Analysis			
_	Sample Number	(cm/sec)	(cm/sec)	Constant Head	Falling Head		
	T7ALRLC-Comp (<2mm, 1.4g/cc)	2.6E-02	7.2E-03	Х			
	UTPQA-2 (<2mm, 1.4g/cc)	8.9E-02	1.6E-02	Х			
	UTPQA-3 (<2mm, 1.4g/cc)	7.0E-02	2.0E-02	Х			
	LTPQA-4 (<2mm, 1.4g/cc)	3.2E-02	1.0E-02	Х			

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NR = Not requested

NA = Not applicable

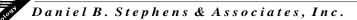


	Pressure Head	Moisture Content
Sample Number	(-cm water)	(%, cm ³ /cm ³)
T7ALRLC-Comp (<2mm, 1.4g/cc)	0	48.9
	4	48.5 ^{‡‡}
	11	48.0 ^{‡‡}
	28	31.8 #
	157	21.5 #
	816	14.2 #
	2550	12.0 ##
	36815	7.2 **
	214872	5.1 #
	845560	4.3 ^{‡‡}
UTPQA-2 (<2mm, 1.4g/cc)	0	46.2
011 QA-2 (*211111, 1.+9/00)	4	46.2
	9	43.4 #
	32	32.3 #
	168	18.0 #
	1836	10.3 #
	12034	7.4 **
	43647	5.9 ^{‡‡}
	191314	4.2 ^{‡‡}
	845560	3.3 #
LITDOA = (-2)mm = 1 A a a a a	0	48.7
UTPQA-3 (<2mm, 1.4g/cc)	0 4	40.7 47.1 [#]
	4 11	45.9 #
	23	45.9 [#]
	161	18.4 #
	612	12.6 #
	3977	9.5 #
	57211	5.7 [#]
	219155	4.5 [#]
	845560	3.4 ^{‡‡}

Summary of Moisture Characteristics of the Initial Drainage Curve

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^{‡‡} Volume adjustments are applicable at this matric potential (see data sheet for this sample).



Summary of Moisture Characteristics of the Initial Drainage Curve (Continued)

	Pressure Head	Moisture Content
Sample Number	(-cm water)	(%, cm ³ /cm ³)
LTPQA-4 (<2mm, 1.4g/cc)	0	47.8
	4	47.6 **
	12	46.6 #
	26	33.5 ^{‡‡}
	157	19.8 #
	918	12.3 #
	10504	8.3 #
	69142	5.8 ^{‡‡}
	722120	3.6 #
	845560	3.6 #

^{‡‡} Volume adjustments are applicable at this matric potential (see data sheet for this sample).



Summary of Calculated Unsaturated Hydraulic Properties

						Oversize	Corrected
	Sample Number	ପ (cm⁻¹)	N (dimensionless)	θ _r (% vol)	θ s (% vol)	θ _r (% vol)	θ _s (% vol)
T7AI	LRLC-Comp (<2mm, 1.4g/cc)	0.0784	1.3933	4.76	50.56	1.97	21.34
L	JTPQA-2 (<2mm, 1.4g/cc)	0.0641	1.4448	4.12	47.26	1.18	13.93
L	JTPQA-3 (<2mm, 1.4g/cc)	0.0650	1.4700	4.39	49.37	1.83	20.91
L	.TPQA-4 (<2mm, 1.4g/cc)	0.0610	1.4543	4.31	49.19	1.99	23.37

^{--- =} Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NR = Not requested

NA = Not applicable

Initial Properties



	As Re	eceived	Rem	olded	Dry Bulk	Wet Bulk	Calculated	
Sample Number	Gravimetric (%, g/g)	Volumetric (%, cm ³ /cm ³)	Gravimetric (%, g/g)	Volumetric (%, cm ³ /cm ³)	Density (g/cm ³)	Density (g/cm ³)	Porosity (%)	
T7ALRLC-Comp (<2mm, 1.4g/cc)	NA	NA	2.6	3.6	1.40	1.44	47.1	
UTPQA-2 (<2mm, 1.4g/cc)	NA	NA	9.0	12.6	1.40	1.53	47.1	
UTPQA-3 (<2mm, 1.4g/cc)	NA	NA	8.2	11.6	1.40	1.52	47.0	
LTPQA-4 (<2mm, 1.4g/cc)	NA	NA	7.4	10.3	1.40	1.51	47.0	

Summary of Initial Moisture Content, Dry Bulk Density Wet Bulk Density and Calculated Porosity

NA = Not analyzed



Data for Initial Moisture Content, Bulk Density, Porosity, and Percent Saturation

Job Number: Sample Number: Date Sampled:	Golder Associates, Inc. NM16.0055.00 T7ALRLC-Comp (<2mm, 1.4g/cc) 5/18/2013 USNR, 1303098		
	As Received	Remolded	
Test Date:	NA	10-Mar-16	
Field weight* of sample (g): Tare weight, ring (g): Tare weight, pan/plate (g): Tare weight, other (g): Dry weight of sample (g): Sample volume (cm ³): Assumed particle density (g/cm ³):		453.11 133.37 0.00 0.00 311.66 222.50 2.65	
Gravimetric Moisture Content (% g/g):		2.6	
Volumetric Moisture Content (% vol):		3.6	
Dry bulk density (g/cm ³):		1.40	
Wet bulk density (g/cm ³):		1.44	
Calculated Porosity (% vol):		47.1	
Percent Saturation:		7.7	
Laboratory analysis by: Data entered by: Checked by:		D. O'Dowd D. O'Dowd J. Hines	

Comments:

* Weight including tares

NA = Not analyzed



Data for Initial Moisture Content, Bulk Density, Porosity, and Percent Saturation

Job Number: Sample Number: Date Sampled:	Golder Associates, Inc. NM16.0055.00 UTPQA-2 (<2mm, 1.4g/cc) 5/28/2015 USNR, 1303098		
	As Received	Remolded	
Test Date:	NA	10-Mar-16	
Field weight* of sample (g): Tare weight, ring (g): Tare weight, pan/plate (g): Tare weight, other (g): Dry weight of sample (g): Sample volume (cm ³): Assumed particle density (g/cm ³):		468.48 125.40 0.00 0.00 314.72 224.31 2.65	
Gravimetric Moisture Content (% g/g):		9.0	
Volumetric Moisture Content (% vol):		12.6	
Dry bulk density (g/cm ³):		1.40	
Wet bulk density (g/cm ³):		1.53	
Calculated Porosity (% vol):		47.1	
Percent Saturation:		26.9	
Laboratory analysis by: Data entered by: Checked by:	I	D. O'Dowd D. O'Dowd J. Hines	

Comments:

* Weight including tares

NA = Not analyzed



Data for Initial Moisture Content, Bulk Density, Porosity, and Percent Saturation

Job Number: Sample Number: Date Sampled:	Golder Associates, Inc. NM16.0055.00 UTPQA-3 (<2mm, 1.4g/cc) 5/28/2015 USNR, 1303098		
	As Received R	emolded	
Test Date:	NA 1	0-Mar-16	
Field weight* of sample (g): Tare weight, ring (g): Tare weight, pan/plate (g): Tare weight, other (g): Dry weight of sample (g): Sample volume (cm ³): Assumed particle density (g/cm ³):		468.35 126.74 0.00 0.00 315.62 224.72 2.65	
Gravimetric Moisture Content (% g/g):		8.2	
Volumetric Moisture Content (% vol):		11.6	
Dry bulk density (g/cm ³):		1.40	
Wet bulk density (g/cm ³):		1.52	
Calculated Porosity (% vol):		47.0	
Percent Saturation:		24.6	
Laboratory analysis by: Data entered by: Checked by:	-	'Dowd 'Dowd nes	

Comments:

* Weight including tares

NA = Not analyzed



Data for Initial Moisture Content, Bulk Density, Porosity, and Percent Saturation

Job Number: Sample Number: Date Sampled:	Golder Associates, Inc. NM16.0055.00 LTPQA-4 (<2mm, 1.4g/cc) 5/28/2015 USNR, 1303098		
	As Received Re	molded	
Test Date:	NA 10-	Mar-16	
Field weight* of sample (g): Tare weight, ring (g): Tare weight, pan/plate (g): Tare weight, other (g): Dry weight of sample (g): Sample volume (cm ³): Assumed particle density (g/cm ³):	12 (((3	67.21 27.87 0.00 0.00 16.08 25.21 2.65	
Gravimetric Moisture Content (% g/g):		7.4	
Volumetric Moisture Content (% vol):		10.3	
Dry bulk density (g/cm ³):		1.40	
Wet bulk density (g/cm ³):		1.51	
Calculated Porosity (% vol):		47.0	
Percent Saturation:		22.0	
Laboratory analysis by: Data entered by: Checked by:	D. O'E D. O'E J. Hine	lowd	

Comments:

* Weight including tares

NA = Not analyzed

Saturated Hydraulic Conductivity



Summary of Saturated Hydraulic Conductivity Tests

		K _{sat}	Oversize Corrected K _{sat}	Method of	Analysis
-	Sample Number	(cm/sec)	(cm/sec)	Constant Head	Falling Head
	T7ALRLC-Comp (<2mm, 1.4g/cc)	2.6E-02	7.2E-03	Х	
	UTPQA-2 (<2mm, 1.4g/cc)	8.9E-02	1.6E-02	Х	
	UTPQA-3 (<2mm, 1.4g/cc)	7.0E-02	2.0E-02	Х	
	LTPQA-4 (<2mm, 1.4g/cc)	3.2E-02	1.0E-02	Х	

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NR = Not requested

NA = Not applicable



Saturated Hydraulic Conductivity Constant Head Method

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: T7ALRLC-Comp (<2mm, 1.4g/cc) Date Sampled: 5/18/2013 Project: USNR, 1303098 Type of water used: TAP Collection vessel tare (g): 10.99

Sample length (cm): 7.59

Sample diameter (cm): 6.11

Sample x-sectional area (cm²): 29.31

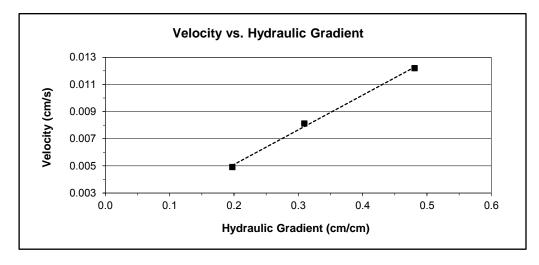
Date	Time	Temp (°C)	Head (cm)	Q + Tare (g)	Q (cm ³)	Elapsed time (sec)	Ksat (cm/sec)	Ksat @ 20°C (cm/sec)
Test # 1: 11-Mar-16 11-Mar-16	9:09:30 9:10:00	19.5	3.65	21.71	10.7	30	2.5E-02	2.6E-02
Test # 2: 11-Mar-16 11-Mar-16	9:31:00 9:31:30	19.5	2.35	18.12	7.1	30	2.6E-02	2.7E-02
Test # 3: 11-Mar-16 11-Mar-16	9:41:00 9:41:30	19.5	1.5	15.30	4.3	30	2.5E-02	2.5E-02

Average Ksat (cm/sec): 2.6E-02

Oversize Corrected Ksat (cm/sec): 7.2E-03

Comments:

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass





Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	T7ALRLC-Comp (<2mm, 1.4g/cc)
Date Sampled:	5/18/2013
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10 Calculated Porosity of Fines (% vol): 47.1

	Coarse Fraction*	Fines Fraction	<u>Composite</u>
Subsample Mass (g): Bulk Density (g/cm ³): Volume of Solids (cm ³): Volume of Voids (cm ³):	8137.70 2.65 3070.83 0.00	3142.11 1.40 1185.70 1057.51	11279.81 2.12 4256.53 1057.51
<i>Total Volume</i> (cm ³):	3070.83	2243.21	5314.04
Volumetric Fraction (%): Mass Fraction (%):	57.79 72.14	42.21 27.86	100.00 100.00
Ksat (cm/sec):	NM	2.6E-02	7.2E-03

* = Porosity and moisture content of coarse fraction assumed to be zero.

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NM = Not measured



Saturated Hydraulic Conductivity Constant Head Method

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: UTPQA-2 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098 Type of water used: TAP Collection vessel tare (g): 10.97

Sample length (cm): 7.60

Sample diameter (cm): 6.13

Sample x-sectional area (cm²): 29.50

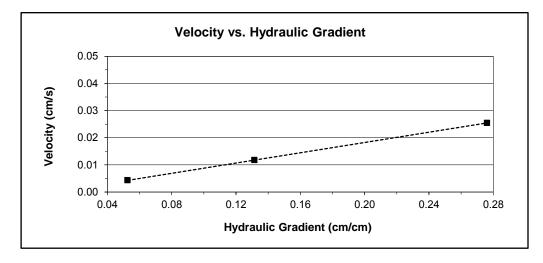
Date	Time	Temp (°C)	Head (cm)	Q + Tare (g)	Q (cm ³)	Elapsed time (sec)	Ksat (cm/sec)	Ksat @ 20°C (cm/sec)
Test # 1: 11-Mar-16 11-Mar-16	9:21:00 9:21:30	19.5	2.1	33.48	22.5	30	9.2E-02	9.3E-02
Test # 2: 11-Mar-16 11-Mar-16	9:32:00 9:32:30	19.5	1	21.34	10.4	30	8.9E-02	9.0E-02
Test # 3: 11-Mar-16 11-Mar-16	9:42:00 9:42:30	19.5	0.4	14.78	3.8	30	8.2E-02	8.3E-02

Average Ksat (cm/sec): 8.9E-02

Oversize Corrected Ksat (cm/sec): 1.6E-02

Comments:

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass





Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	UTPQA-2 (<2mm, 1.4g/cc)
Date Sampled:	5/28/2015
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10 Calculated Porosity of Fines (% vol): 47.1

	Coarse Fraction*	Fines Fraction	<u>Composite</u>
Subsample Mass (g): Bulk Density (g/cm ³): Volume of Solids (cm ³): Volume of Voids (cm ³):	4912.19 2.65 1853.66	1087.57 1.40 410.40	5999.76 2.28 2264.06
Total Volume (cm ³): Volumetric Fraction (%):	0.00 1853.66 70.51	364.75 775.15 29.49	364.75 2628.81 100.00
Mass Fraction (%): Ksat (cm/sec):	81.87 NM	18.13 8.9E-02	100.00 1.6E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NM = Not measured



Saturated Hydraulic Conductivity Constant Head Method

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: UTPQA-3 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098 Type of water used: TAP

Collection vessel tare (g): 11.00

Sample length (cm): 7.61

Sample diameter (cm): 6.13

Sample x-sectional area (cm²): 29.52

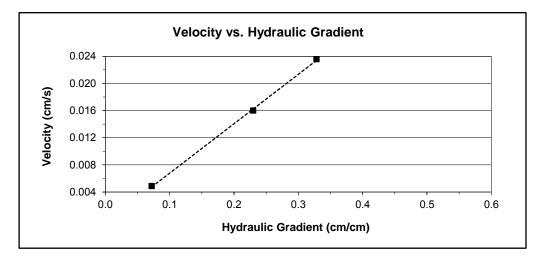
Date	Time	Temp (°C)	Head (cm)	Q + Tare (g)	Q (cm ³)	Elapsed time (sec)	Ksat (cm/sec)	Ksat @ 20°C (cm/sec)
Test # 1: 11-Mar-16 11-Mar-16	9:22:00 9:22:30	19.5	2.5	31.87	20.9	30	7.2E-02	7.3E-02
Test # 2: 11-Mar-16 11-Mar-16	9:33:00 9:33:30	19.5	1.75	25.15	14.2	30	6.9E-02	7.1E-02
Test # 3: 11-Mar-16 11-Mar-16	9:43:00 9:43:30	19.5	0.55	15.30	4.3	30	6.7E-02	6.8E-02

Average Ksat (cm/sec): 7.0E-02

Oversize Corrected Ksat (cm/sec): 2.0E-02

Comments:

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass





Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	UTPQA-3 (<2mm, 1.4g/cc)
Date Sampled:	5/28/2015
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10 Calculated Porosity of Fines (% vol): 47.0

	Coarse Fraction*	Fines Fraction	<u>Composite</u>
Subsample Mass (g): Bulk Density (g/cm ³): Volume of Solids (cm ³): Volume of Voids (cm ³):	4561.39 2.65 1721.28 0.00	1776.38 1.40 670.33 594.47	6337.77 2.12 2391.61 594.47
Total Volume (cm ³):	1721.28	1264.80	2986.08
Volumetric Fraction (%): Mass Fraction (%):	57.64 71.97	42.36 28.03	100.00 100.00
Ksat (cm/sec):	NM	7.0E-02	2.0E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NM = Not measured



Saturated Hydraulic Conductivity Constant Head Method

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: LTPQA-4 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098 Type of water used: TAP

Collection vessel tare (g): 11.04

Sample length (cm): 7.62

Sample diameter (cm): 6.14

Sample x-sectional area (cm²): 29.57

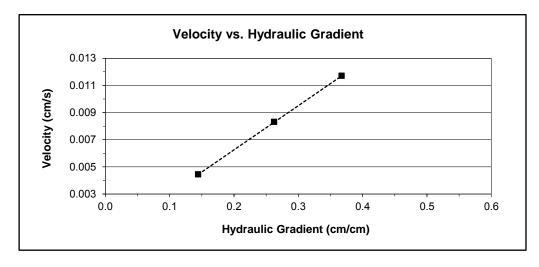
Date	Time	Temp (°C)	Head (cm)	Q + Tare (g)	Q (cm ³)	Elapsed time (sec)	Ksat (cm/sec)	Ksat @ 20°C (cm/sec)
Test # 1: 11-Mar-16 11-Mar-16	9:23:00 9:23:30	19.5	2.8	21.42	10.4	30	3.2E-02	3.2E-02
Test # 2: 11-Mar-16 11-Mar-16	9:34:00 9:34:30	19.5	2	18.41	7.4	30	3.2E-02	3.2E-02
Test # 3: 11-Mar-16 11-Mar-16	9:44:00 9:44:30	19.5	1.1	14.98	3.9	30	3.1E-02	3.1E-02

Average Ksat (cm/sec): 3.2E-02

Oversize Corrected Ksat (cm/sec): 1.0E-02

Comments:

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass





Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	LTPQA-4 (<2mm, 1.4g/cc)
Date Sampled:	5/28/2015
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10 Calculated Porosity of Fines (% vol): 47.0

	Coarse Fraction*	Fines Fraction	<u>Composite</u>
Subsample Mass (g): Bulk Density (g/cm ³): Volume of Solids (cm ³): Volume of Voids (cm ³):	5018.47 2.65 1893.76 0.00	2406.12 1.40 907.97 806.41	7424.59 2.06 2801.73 806.41
Total Volume (cm ³):	1893.76	1714.38	3608.15
Volumetric Fraction (%): Mass Fraction (%):	52.49 67.59	47.51 32.41	100.00 100.00
Ksat (cm/sec):	NM	3.2E-02	1.0E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

--- = Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NM = Not measured

Moisture Retention Characteristics

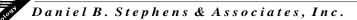


	Pressure Head	Moisture Content
Sample Number	(-cm water)	(%, cm ³ /cm ³)
T7ALRLC-Comp (<2mm, 1.4g/cc)	0	48.9
	4	48.5 ^{‡‡}
	11	48.0 ^{‡‡}
	28	31.8 #
	157	21.5 #
	816	14.2 #
	2550	12.0 ^{‡‡}
	36815	7.2 #
	214872	5.1 ^{‡‡}
	845560	4.3 ^{##}
UTPQA-2 (<2mm, 1.4g/cc)	0	46.2
011 QA-2 (1211111, 1.+9/00)	4	46.2
	9	43.4 #
	32	32.3 [#]
	168	18.0 #
	1836	10.3 #
	12034	7.4 #
	43647	5.9 ^{‡‡}
	191314	4.2 ^{‡‡}
	845560	3.3 #
LITDOA = (-2)mm = 1 da(-2)	0	48.7
UTPQA-3 (<2mm, 1.4g/cc)	0 4	48.7 47.1 [#]
	4 11	47.1 **
	23	35.0 [#]
	161	18.4 #
	612	12.6 #
	3977	9.5 #
	57211	5.7 [#]
	219155	4.5 ^{‡‡}
	845560	3.4 #

Summary of Moisture Characteristics of the Initial Drainage Curve

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^{‡‡} Volume adjustments are applicable at this matric potential (see data sheet for this sample).



Summary of Moisture Characteristics of the Initial Drainage Curve (Continued)

	Pressure Head	Moisture Content
Sample Number	(-cm water)	(%, cm ³ /cm ³)
LTPQA-4 (<2mm, 1.4g/cc)	0	47.8
	4	47.6 **
	12	46.6 #
	26	33.5 ^{‡‡}
	157	19.8 #
	918	12.3 #
	10504	8.3 #
	69142	5.8 ^{‡‡}
	722120	3.6 #
	845560	3.6 #

^{‡‡} Volume adjustments are applicable at this matric potential (see data sheet for this sample).



Summary of Calculated Unsaturated Hydraulic Properties

						Oversize Corrected	
	Sample Number	ପ (cm⁻¹)	N (dimensionless)	θ _r (% vol)	θ _s (% vol)	θ _r (% vol)	θ _s (% vol)
	T7ALRLC-Comp (<2mm, 1.4g/cc)	0.0784	1.3933	4.76	50.56	1.97	21.34
	UTPQA-2 (<2mm, 1.4g/cc)	0.0641	1.4448	4.12	47.26	1.18	13.93
	UTPQA-3 (<2mm, 1.4g/cc)	0.0650	1.4700	4.39	49.37	1.83	20.91
	LTPQA-4 (<2mm, 1.4g/cc)	0.0610	1.4543	4.31	49.19	1.99	23.37

^{--- =} Oversize correction is unnecessary since coarse fraction < 5% of composite mass

NR = Not requested

NA = Not applicable



Moisture Retention Data

Hanging Column / Pressure Plate

(Soil-Water Characteristic Curve)

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: T7ALRLC-Comp (<2mm, 1.4g/cc) Date Sampled: 5/18/2013 Project: USNR, 1303098

Dry wt. of sample (g):	311.66
Tare wt., ring (g):	133.37
Tare wt., screen & clamp (g):	
<i>Initial sample volume</i> (cm ³):	
Initial dry bulk density (g/cm ³):	1.40
Assumed particle density (g/cm ³):	2.65
Initial calculated total porosity (%):	47.14

	Date	Time	Weight*	Matric Potential (-cm water)	Moisture Content [†] (% vol)	
		-	(g)		· /	_
Hanging column:	11-Mar-16	12:05	581.35	0	48.93	
	18-Mar-16	10:05	578.60	4.0	48.50	‡ ‡
	25-Mar-16	12:10	576.20	11.0	48.02	‡ ‡
	1-Apr-16	16:00	541.10	28.0	31.77	‡ ‡
	8-Apr-16	9:30	519.00	157.0	21.54	‡ ‡

Volume Adjusted Data¹

					Adjusted
	Matric	Adjusted	% Volume	Adjusted	Calculated
	Potential	Volume	Change ²	Density	Porosity
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)
Hanging column:	0.0				
	4.0	218.84	-1.65%	1.42	46.26
	11.0	216.02	-2.91%	1.44	45.56
	28.0	216.02	-2.91%	1.44	45.56
	157.0	216.02	-2.91%	1.44	45.56

Comments:

- ¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent each of the volume change measurements obtained after saturated hydraulic conductivity testing and throughout hanging column/pressure plate testing. "---" indicates no volume changes occurred.
- ² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

[†] Assumed density of water is 1.0 g/cm³

⁺⁺ Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

Technician Notes:



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box (Soil-Water Characteristic Curve)

Sample Number: T7ALRLC-Comp (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of dew point potentiometer sample (g): 170.62 Tare weight, jar (g): 115.79

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	
Dew point potentiometer:	29-Mar-16	10:50	176.03	816	14.24	±‡
	24-Mar-16	9:10	175.19	2550	12.02	‡ ‡
	21-Mar-16	10:20	173.37	36815	7.24	‡ ‡
	17-Mar-16	8:15	172.56	214872	5.10	

	Volume Adjusted Data ¹					
	Water Potential	Adjusted Volume	% Volume Change ²	Adjusted Density	Adjusted Calc. Porosity	
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)	
Dew point potentiometer:	816	216.02	-2.91%	1.44	45.56	
	2550	216.02	-2.91%	1.44	45.56	
	36815	216.02	-2.91%	1.44	45.56	
	214872	216.02	-2.91%	1.44	45.56	

Comments:

¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

^{##} Volume adjustments are applicable at this matric potential (see comment #1).



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: T7ALRLC-Comp (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of relative humidity box sample (g): 79.16 Tare weight (g): 38.82

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	_
Relative humidity box:	15-Mar-16	10:40	80.37	845560	4.33	‡ ‡
			Volume Adjust	ted Data ¹		
	Water	Adjusted	% Volume	Adjusted	Adjusted	
	Potential	Volume	Change ²	Density	Calc. Porosity	
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)	
Relative humidity box:	845560	216.02	-2.91%	1.44	45.56	_

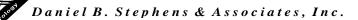
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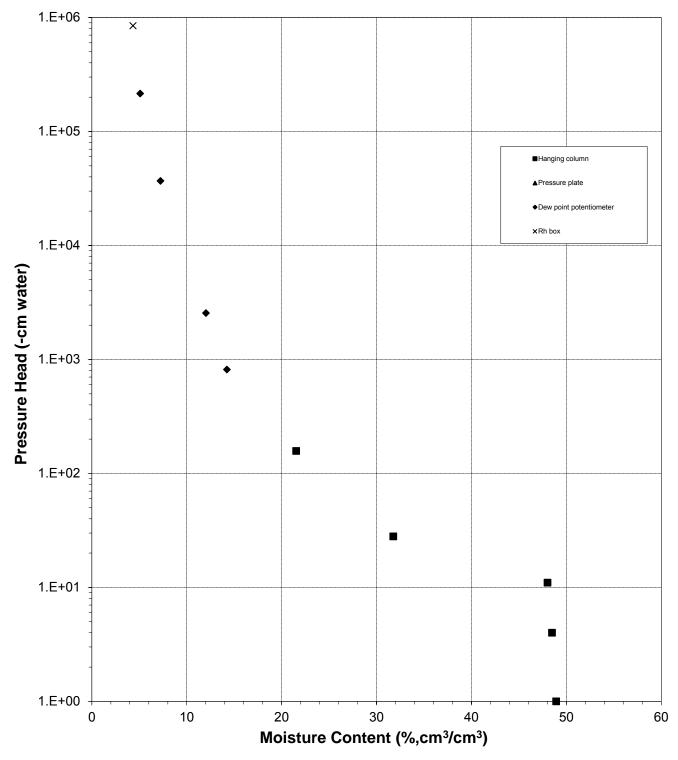
¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

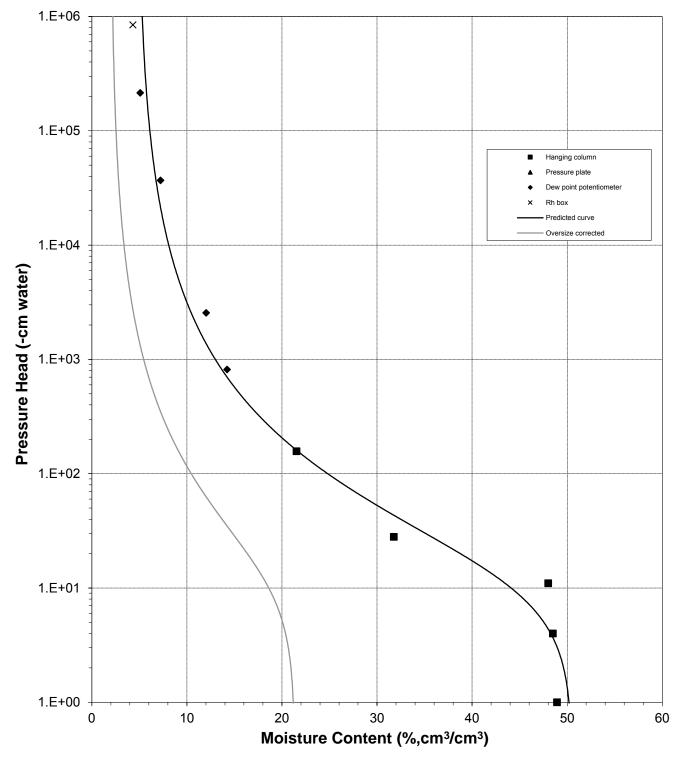
* Weight including tares

^{‡‡} Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

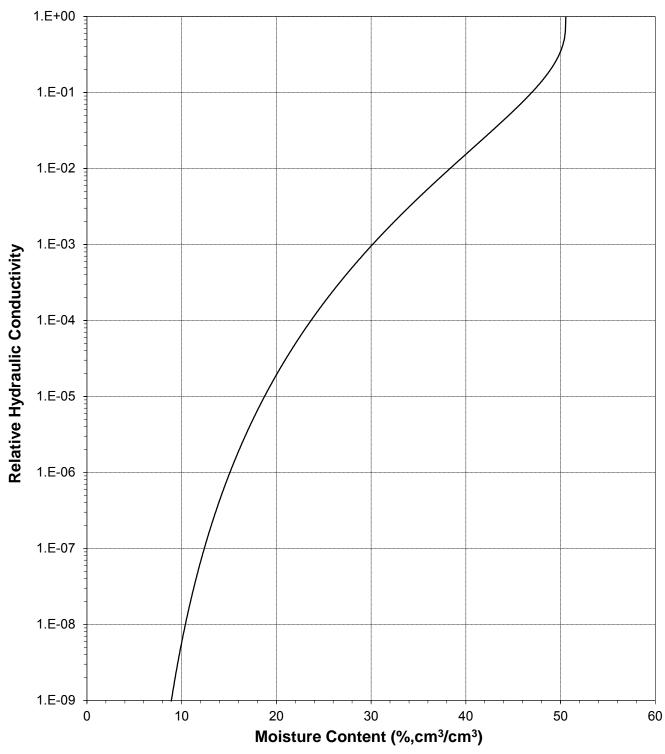




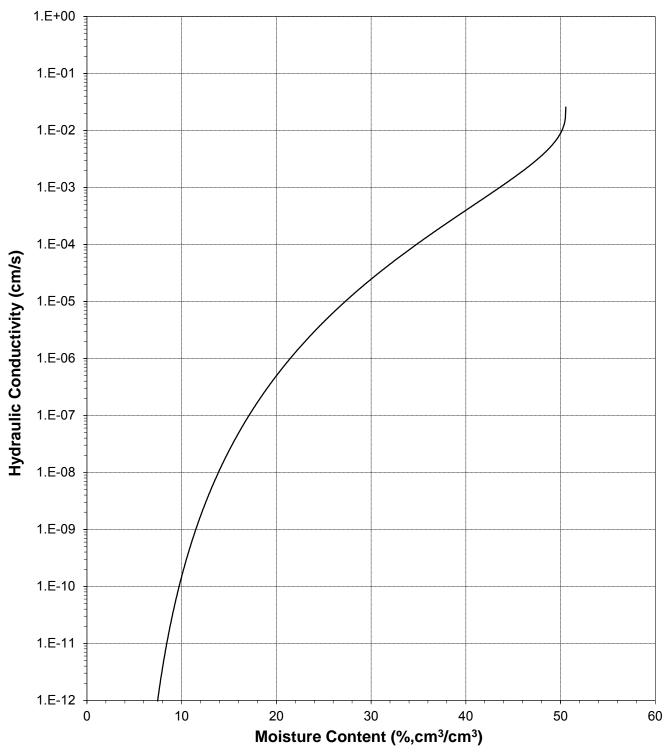
Water Retention Data Points



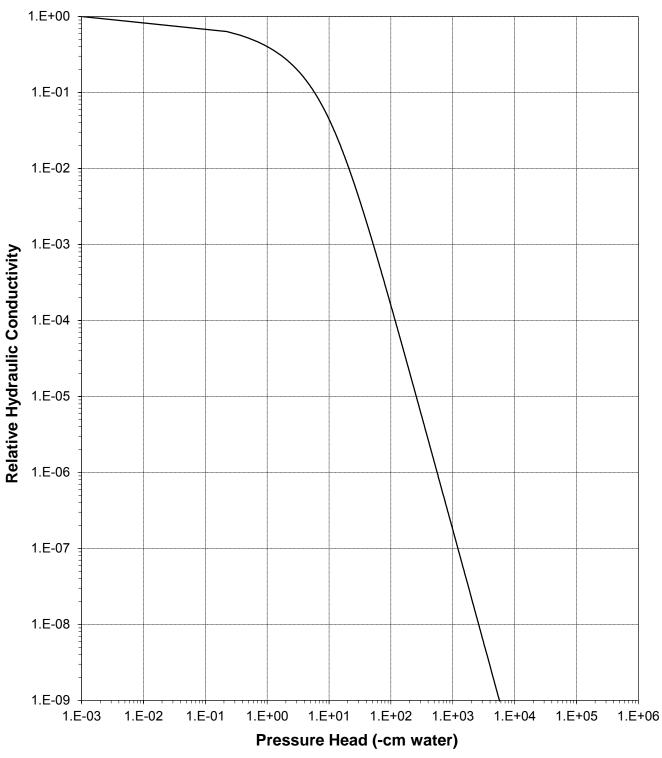
Predicted Water Retention Curve and Data Points



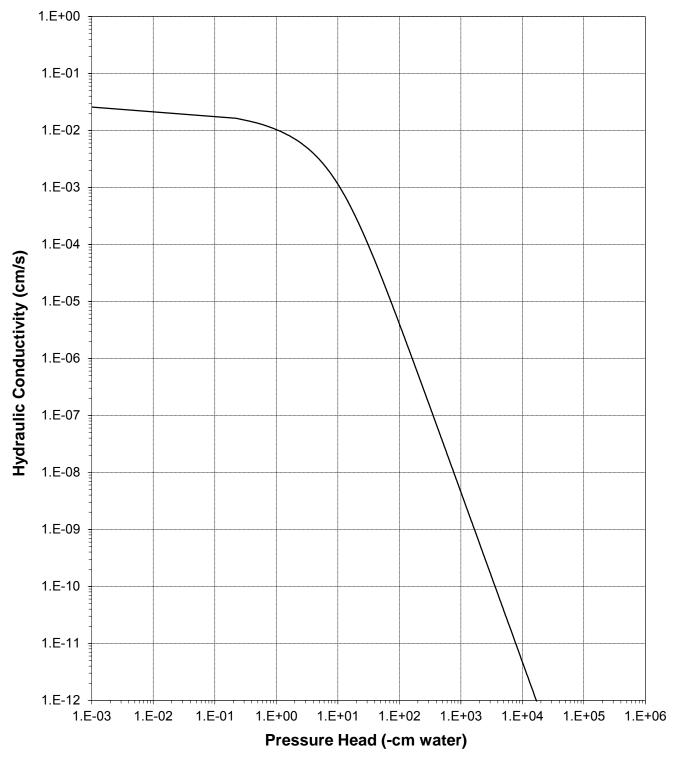
Plot of Relative Hydraulic Conductivity vs Moisture Content



Plot of Hydraulic Conductivity vs Moisture Content



Plot of Relative Hydraulic Conductivity vs Pressure Head



Plot of Hydraulic Conductivity vs Pressure Head



Oversize Correction Data Sheet

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: T7ALRLC-Comp (<2mm, 1.4g/cc) Date Sampled: 5/18/2013 Project: USNR, 1303098

Split (3/4", 3/8", #4): #10

	Coarse Fraction*	Fines Fraction**	<u>Composite</u>
Subsample Mass (g):	8137.70	3142.11	11279.81
Mass Fraction (%):	72.14	27.86	100.00
Initial Sample θ_i			
Bulk Density (g/cm ³):	2.65	1.40	2.12
Calculated Porosity (% vol):	0.00	47.14	19.90
Volume of Solids (cm ³):	3070.83	1185.70	4256.53
<i>Volume of Voids</i> (cm ³):	0.00	1057.51	1057.51
<i>Total Volume</i> (cm ³):	3070.83	2243.21	5314.04
Volumetric Fraction (%):	57.79	42.21	100.00
Initial Moisture Content (% vol):	0.00	3.63	1.53
Saturated Sample θ_s			
Bulk Density (g/cm ³):	2.65	1.40	2.12
Calculated Porosity (% vol):	0.00	47.14	19.90
Volume of Solids (cm ³):	3070.83	1185.70	4256.53
<i>Volume of Voids</i> (cm ³):	0.00	1057.51	1057.51
<i>Total Volume</i> (cm ³):	3070.83	2243.21	5314.04
Volumetric Fraction (%):	57.79	42.21	100.00
Saturated Moisture Content (% vol):	0.00	50.56	21.34
Residual Sample θ_r			
Bulk Density (g/cm ³):	2.65	1.44	2.15
Calculated Porosity (% vol):	0.00	45.56	18.90
Volume of Solids (cm ³):	3070.83	1185.70	4256.53
<i>Volume of Voids</i> (cm ³):	0.00	992.20	992.20
<i>Total Volume</i> (cm ³):	3070.83	2177.90	5248.73
Volumetric Fraction (%):	58.51	41.49	100.00
Residual Moisture Content (% vol):	0.00	4.76	1.97
Ksat (cm/sec):	NM	2.6E-02	7.2E-03

* = Porosity and moisture content of coarse fraction assumed to be zero.

** = Volume adjusted, if applicable. See notes on Moisture Retention Data pages.

NM = Not measured



Moisture Retention Data

Hanging Column / Pressure Plate

(Soil-Water Characteristic Curve)

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: UTPQA-2 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098

Dry wt. of sample (g):	314.72
Tare wt., ring (g):	125.40
Tare wt., screen & clamp (g):	
<i>Initial sample volume</i> (cm ³):	
Initial dry bulk density (g/cm³):	1.40
Assumed particle density (g/cm ³):	2.65
Initial calculated total porosity (%):	47.06

			Weight*	Matric Potential	Moisture Content [†]	
	Date	Time	(g)	(-cm water)	(% vol)	
Hanging column:	11-Mar-16	12:12	571.74	0	46.24	
	18-Mar-16	10:10	571.70	4.0	46.23	
	25-Mar-16	12:12	563.10	8.5	43.42	‡ ‡
	1-Apr-16	16:05	538.30	31.5	32.34	‡ ‡
	8-Apr-16	9:33	506.90	168.0	18.00	‡ ‡

|--|

	Matric Potential (-cm water)	Adjusted Volume (cm ³)	% Volume Change ² (%)	Adjusted Density (g/cm ³)	Adjusted Calculated Porosity (%)
Hanging column:	0.0				
	4.0				
	8.5	219.00	-2.37%	1.44	45.77
	31.5	217.38	-3.09%	1.45	45.37
	168.0	216.11	-3.66%	1.46	45.05

Comments:

- ¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent each of the volume change measurements obtained after saturated hydraulic conductivity testing and throughout hanging column/pressure plate testing. "---" indicates no volume changes occurred.
- ² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

[†] Assumed density of water is 1.0 g/cm³

⁺⁺ Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

Technician Notes:



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: UTPQA-2 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of dew point potentiometer sample (g): 162.72 Tare weight, jar (g): 113.19

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	
Dew point potentiometer:	24-Mar-16	9:17	166.22	1836	10.29	+ ‡
	22-Mar-16	12:40	165.24	12034	7.41	‡ ‡
	21-Mar-16	10:30	164.72	43647	5.88	‡ ‡
	17-Mar-16	8:21	164.16	191314	4.23	

			Volume Adjusted	d Data ¹	
	Water Potential	Adjusted Volume	% Volume Change ²	Adjusted Density	Adjusted Calc. Porosity
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)
Dew point potentiometer:	1836	216.11	-3.66%	1.46	45.05
	12034	216.11	-3.66%	1.46	45.05
	43647	216.11	-3.66%	1.46	45.05
	191314	216.11	-3.66%	1.46	45.05

Comments:

¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

^{##} Volume adjustments are applicable at this matric potential (see comment #1).



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: UTPQA-2 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of relative humidity box sample (g): 82.06

Tare weight (g): 47.61

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	
Relative humidity box:	15-Mar-16	10:40	82.83	845560	3.27	‡‡
			Volume Adjust	ted Data ¹		
	Water	Adjusted	% Volume	Adjusted	Adjusted	
	Potential	Volume	Change ²	Density	Calc. Porosity	
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)	
Relative humidity box:	845560	216.11	-3.66%	1.46	45.05	_

Comments:

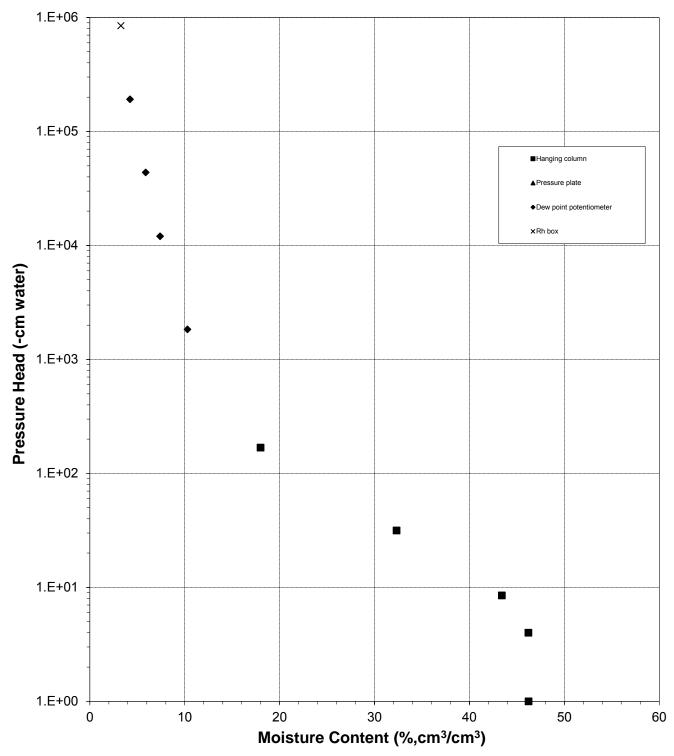
¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

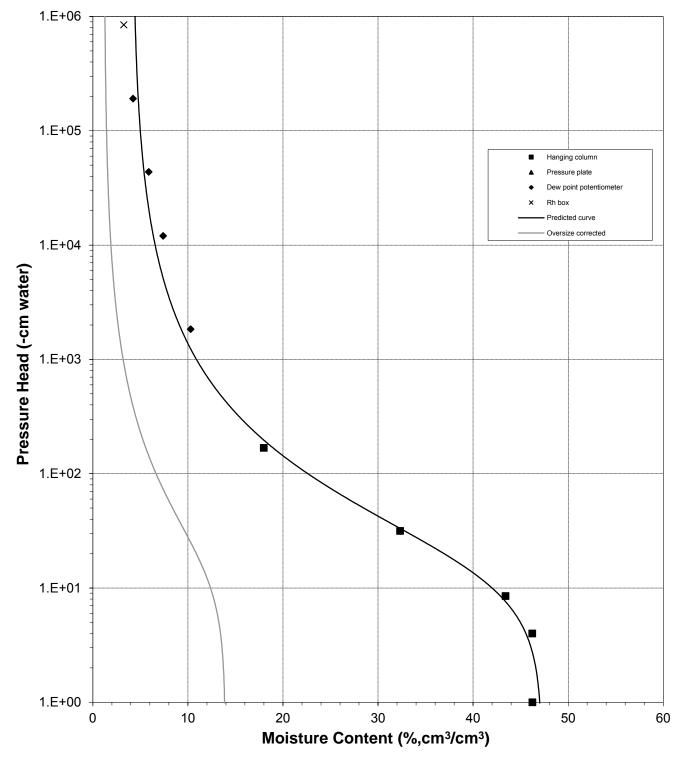
* Weight including tares

^{‡‡} Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

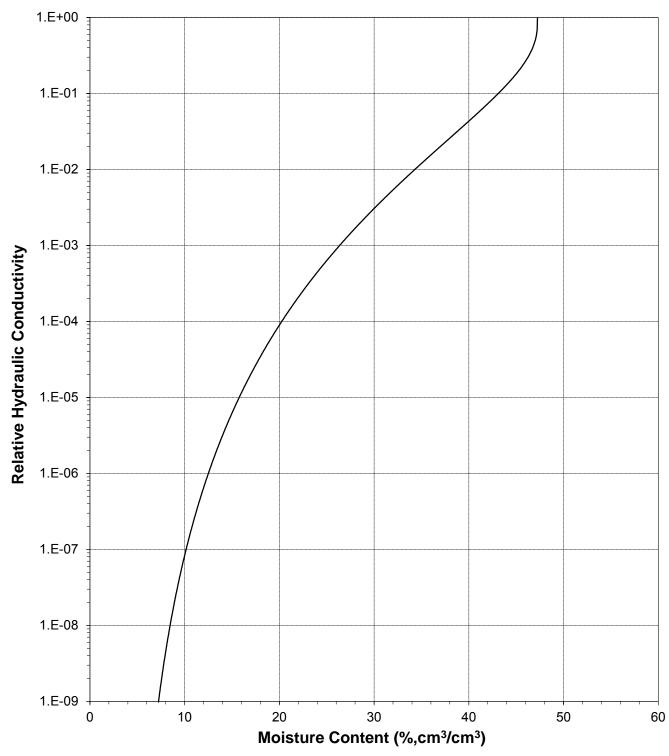




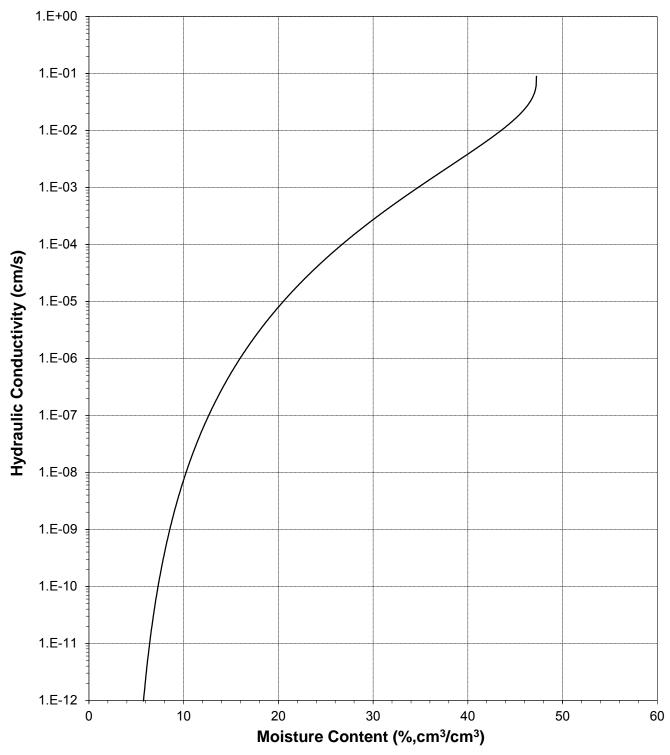
Water Retention Data Points



Predicted Water Retention Curve and Data Points

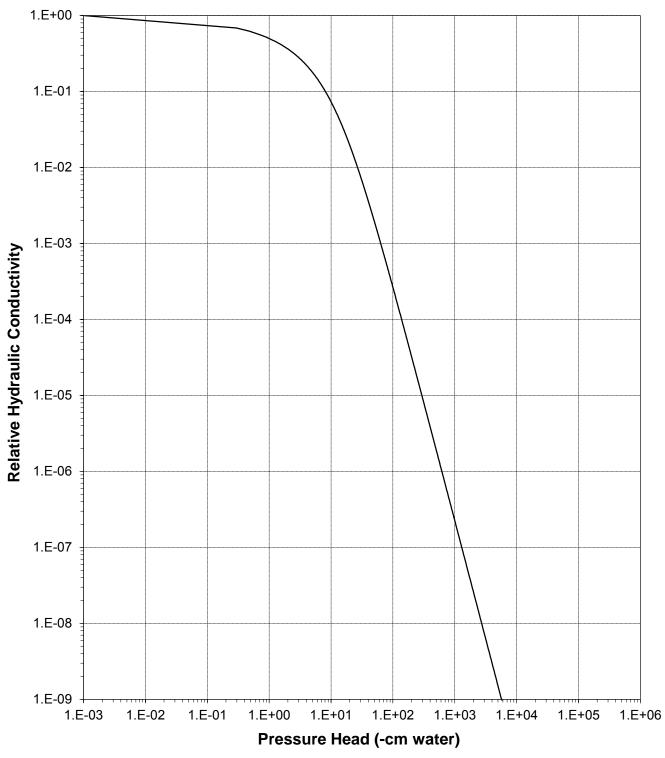


Plot of Relative Hydraulic Conductivity vs Moisture Content

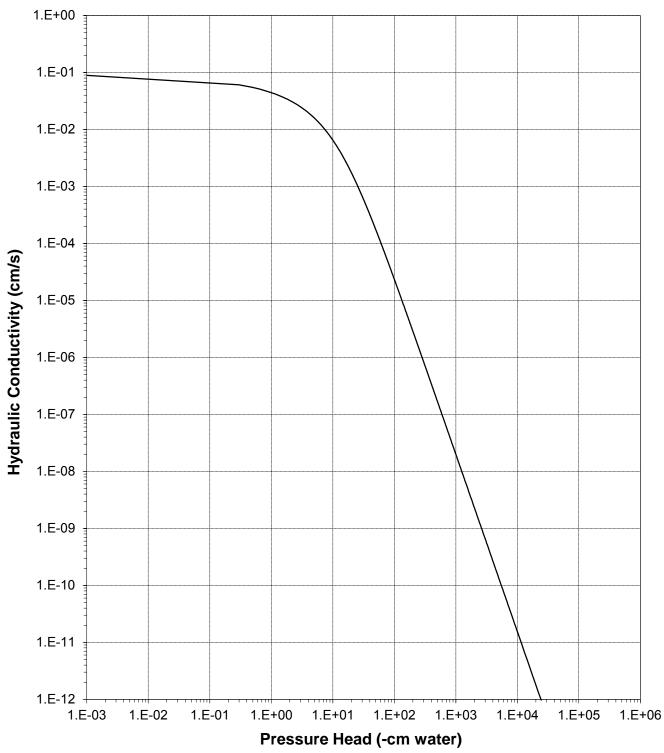


Plot of Hydraulic Conductivity vs Moisture Content





Plot of Relative Hydraulic Conductivity vs Pressure Head



Plot of Hydraulic Conductivity vs Pressure Head



Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	UTPQA-2 (<2mm, 1.4g/cc)
Date Sampled:	5/28/2015
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10

	Coarse Fraction*	Fines Fraction**	<u>Composite</u>
Subsample Mass (g):	4912.19	1087.57	5999.76
Mass Fraction (%):	81.87	18.13	100.00
Initial Sample θ_i			
Bulk Density (g/cm ³):	2.65	1.40	2.28
Calculated Porosity (% vol):	0.00	47.06	13.88
Volume of Solids (cm ³):	1853.66	410.40	2264.06
<i>Volume of Voids</i> (cm ³):	0.00	364.75	364.75
<i>Total Volume</i> (cm ³):	1853.66	775.15	2628.81
Volumetric Fraction (%):	70.51	29.49	100.00
Initial Moisture Content (% vol):	0.00	12.64	3.73
Saturated Sample θ_s			
Bulk Density (g/cm ³):	2.65	1.40	2.28
Calculated Porosity (% vol):	0.00	47.06	13.88
Volume of Solids (cm ³):	1853.66	410.40	2264.06
<i>Volume of Voids</i> (cm ³):	0.00	364.75	364.75
<i>Total Volume</i> (cm ³):	1853.66	775.15	2628.81
Volumetric Fraction (%):	70.51	29.49	100.00
Saturated Moisture Content (% vol):	0.00	47.26	13.93
Residual Sample θ_r			
Bulk Density (g/cm ³):	2.65	1.46	2.31
Calculated Porosity (% vol):	0.00	45.05	12.94
Volume of Solids (cm ³):	1853.66	410.40	2264.06
<i>Volume of Voids</i> (cm ³):	0.00	336.41	336.41
<i>Total Volume</i> (cm ³):	1853.66	746.81	2600.47
Volumetric Fraction (%):	71.28	28.72	100.00
Residual Moisture Content (% vol):	0.00	4.12	1.18
Ksat (cm/sec):	NM	8.9E-02	1.6E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

** = Volume adjusted, if applicable. See notes on Moisture Retention Data pages.

NM = Not measured



Moisture Retention Data

Hanging Column / Pressure Plate

(Soil-Water Characteristic Curve)

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: UTPQA-3 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098

Dry wt. of sample (g):	315.62
Tare wt., ring (g):	126.74
Tare wt., screen & clamp (g):	
<i>Initial sample volume</i> (cm ³):	224.72
Initial dry bulk density (g/cm³):	1.40
Assumed particle density (g/cm ³):	2.65
<i>Initial calculated total porosity (%):</i>	47.00

	Date	Time	Weight* (g)	Matric Potential (-cm water)	Moisture Content [†] (% vol)	
Hanging column:	11-Mar-16	12:17	579.90	0	48.66	_
	18-Mar-16	10:12	575.00	4.0	47.14	‡ ‡
	25-Mar-16	12:20	570.40	10.5	45.86	‡ ‡
	1-Apr-16	16:10	546.70	22.5	34.97	‡ ‡
	8-Apr-16	9:35	510.70	161.0	18.44	‡ ‡

Volume Adjusted Data ¹

	Matric Potential (-cm water)	Adjusted Volume (cm ³)	% Volume Change ² (%)	Adjusted Density (g/cm ³)	Adjusted Calculated Porosity (%)
Hanging column:	0.0				
	4.0	221.60	-1.39%	1.42	46.25
	10.5	217.73	-3.11%	1.45	45.30
	22.5	217.73	-3.11%	1.45	45.30
_	161.0	217.73	-3.11%	1.45	45.30

Comments:

- ¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent each of the volume change measurements obtained after saturated hydraulic conductivity testing and throughout hanging column/pressure plate testing. "---" indicates no volume changes occurred.
- ² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

[†] Assumed density of water is 1.0 g/cm³

^{‡‡} Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

Technician Notes:



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: UTPQA-3 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of dew point potentiometer sample (g): 170.92 Tare weight, jar (g): 115.29

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	
Dew point potentiometer:	29-Mar-16	11:50	175.75	612	12.59	±‡
	24-Mar-16	9:35	174.57	3977	9.51	‡ ‡
	21-Mar-16	10:37	173.11	57211	5.71	‡ ‡
	17-Mar-16	8:30	172.64	219155	4.48	

			Volume Adjusted	d Data ¹	
	Water Potential	Adjusted Volume	% Volume Change ²	Adjusted Density	Adjusted Calc. Porosity
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)
Dew point potentiometer:	612	217.73	-3.11%	1.45	45.30
	3977	217.73	-3.11%	1.45	45.30
	57211	217.73	-3.11%	1.45	45.30
	219155	217.73	-3.11%	1.45	45.30

Comments:

¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

^{##} Volume adjustments are applicable at this matric potential (see comment #1).



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: UTPQA-3 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40

Dry weight* of relative humidity box sample (g): 71.93 Tare weight (g): 39.38

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content (% vol)	
Relative humidity box:	15-Mar-16	10:40	72.69	845560	3.41	
			Volume Adjust	ted Data ¹		
	Water	Adjusted	% Volume	Adjusted	Adjusted	
	Potential	Volume	Change ²	Density	Calc. Porosity	
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)	
Relative humidity box:	845560	217.73	-3.11%	1.45	45.30	_

Comments:

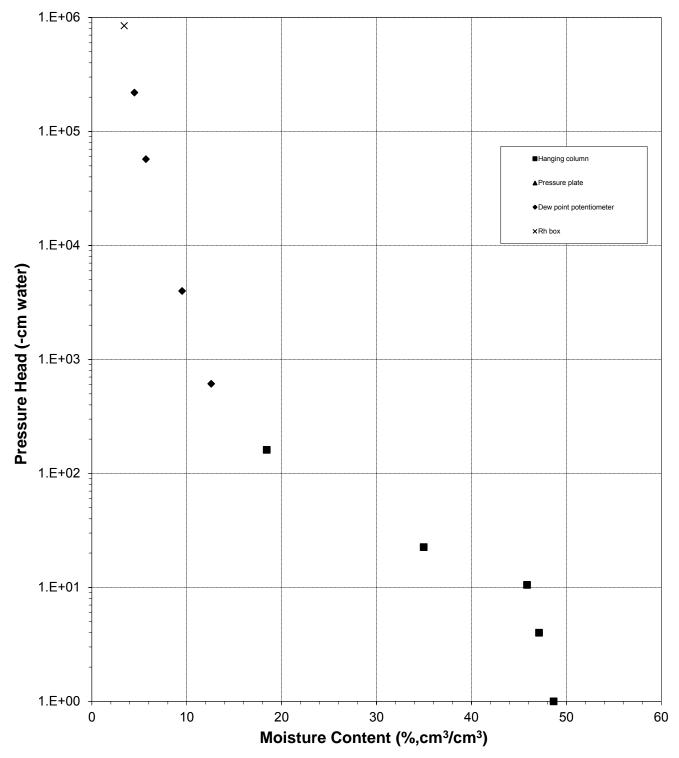
¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

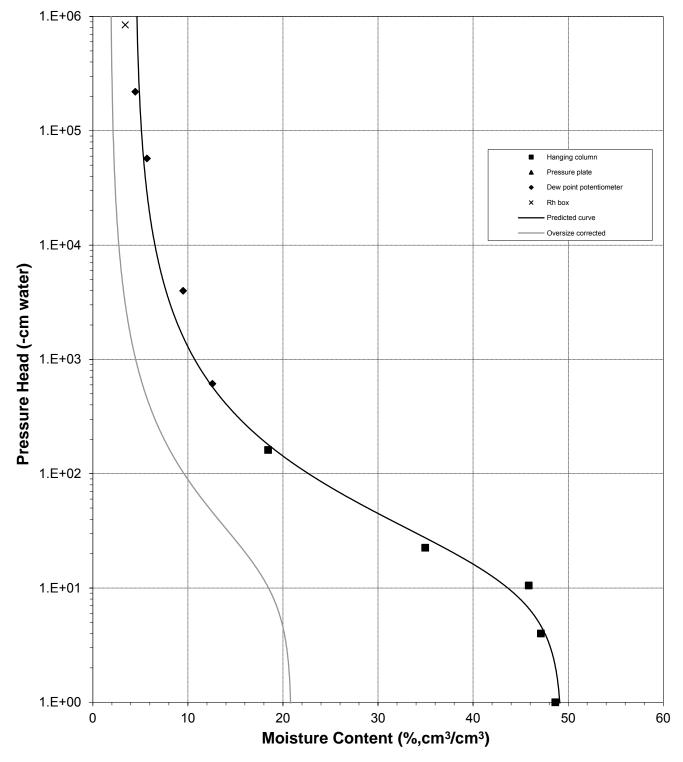
* Weight including tares

^{‡‡} Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

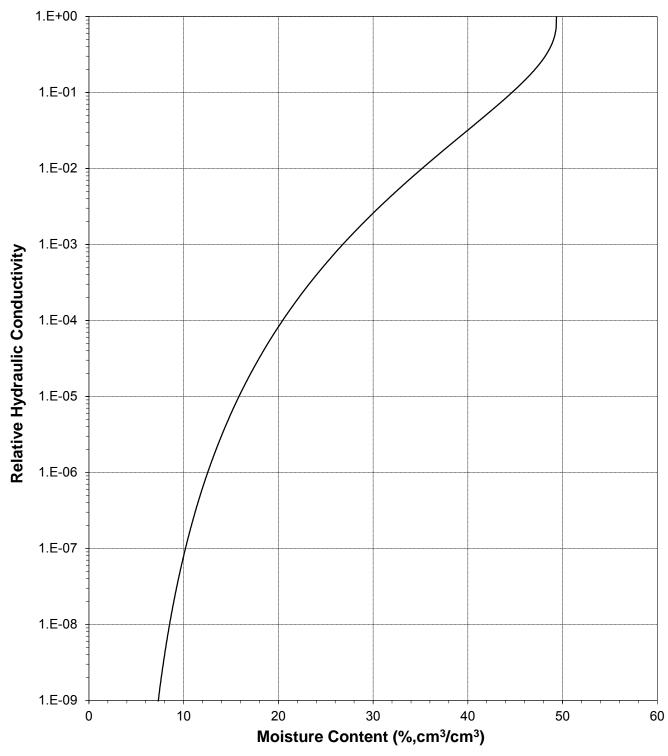




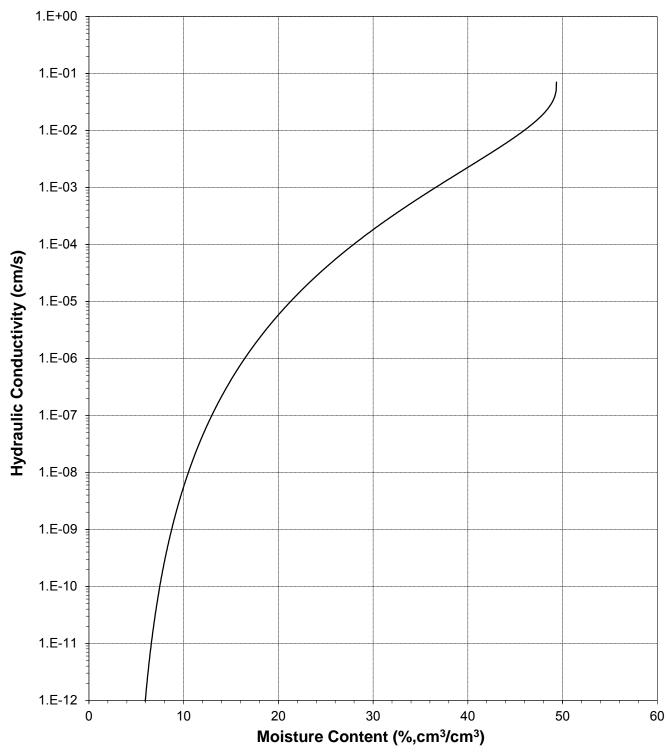
Water Retention Data Points



Predicted Water Retention Curve and Data Points

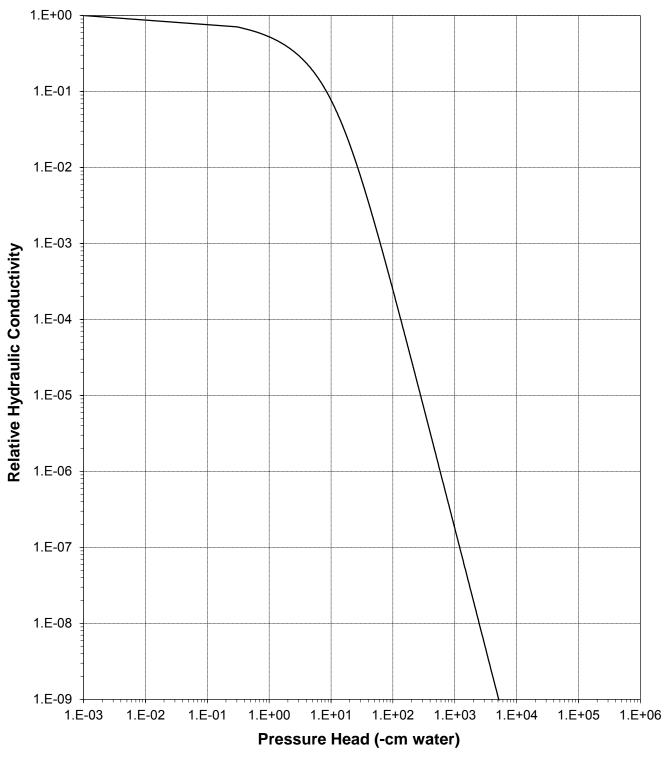


Plot of Relative Hydraulic Conductivity vs Moisture Content

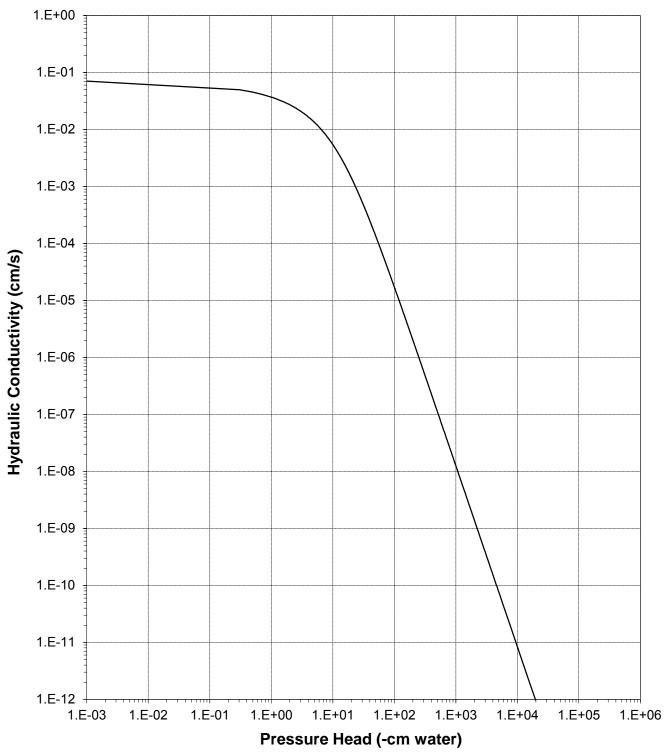


Plot of Hydraulic Conductivity vs Moisture Content





Plot of Relative Hydraulic Conductivity vs Pressure Head



Plot of Hydraulic Conductivity vs Pressure Head



Oversize Correction Data Sheet

Job Name:	Golder Associates, Inc.
Job Number:	NM16.0055.00
Sample Number:	UTPQA-3 (<2mm, 1.4g/cc)
Date Sampled:	5/28/2015
Project:	USNR, 1303098

Split (3/4", 3/8", #4): #10

	Coarse Fraction*	Fines Fraction**	<u>Composite</u>
Subsample Mass (g):	4561.39	1776.38	6337.77
Mass Fraction (%):	71.97	28.03	100.00
Initial Sample θ_i			
Bulk Density (g/cm ³):	2.65	1.40	2.12
Calculated Porosity (% vol):	0.00	47.00	19.91
Volume of Solids (cm ³):	1721.28	670.33	2391.61
<i>Volume of Voids</i> (cm ³):	0.00	594.47	594.47
<i>Total Volume</i> (cm ³):	1721.28	1264.80	2986.08
Volumetric Fraction (%):	57.64	42.36	100.00
Initial Moisture Content (% vol):	0.00	11.57	4.90
Saturated Sample θ_s			
Bulk Density (g/cm ³):	2.65	1.40	2.12
Calculated Porosity (% vol):	0.00	47.00	19.91
Volume of Solids (cm ³):	1721.28	670.33	2391.61
<i>Volume of Voids</i> (cm ³):	0.00	594.47	594.47
<i>Total Volume</i> (cm ³):	1721.28	1264.80	2986.08
Volumetric Fraction (%):	57.64	42.36	100.00
Saturated Moisture Content (% vol):	0.00	49.37	20.91
Residual Sample θ_r			
Bulk Density (g/cm ³):	2.65	1.45	2.15
Calculated Porosity (% vol):	0.00	45.30	18.84
Volume of Solids (cm ³):	1721.28	670.33	2391.61
<i>Volume of Voids</i> (cm ³):	0.00	555.09	555.09
<i>Total Volume</i> (cm ³):	1721.28	1225.42	2946.70
Volumetric Fraction (%):	58.41	41.59	100.00
Residual Moisture Content (% vol):	0.00	4.39	1.83
Ksat (cm/sec):	NM	7.0E-02	2.0E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

** = Volume adjusted, if applicable. See notes on Moisture Retention Data pages.

NM = Not measured



Moisture Retention Data

Hanging Column / Pressure Plate

(Soil-Water Characteristic Curve)

Job Name: Golder Associates, Inc. Job Number: NM16.0055.00 Sample Number: LTPQA-4 (<2mm, 1.4g/cc) Date Sampled: 5/28/2015 Project: USNR, 1303098

Dry wt. of sample (g):	316.08
Tare wt., ring (g):	127.87
Tare wt., screen & clamp (g):	
<i>Initial sample volume</i> (cm ³):	225.21
Initial dry bulk density (g/cm³):	1.40
Assumed particle density (g/cm ³):	2.65
Initial calculated total porosity (%):	47.04

			\\/aiabt*	Matric Potential	Moisture Content [†]	
	Dete	Time	Weight*			
_	Date	Time	(g)	(-cm water)	(% vol)	_
Hanging column:	11-Mar-16	12:25	579.31	0	47.79	
	18-Mar-16	10:17	575.70	4.0	47.62	‡ ‡
	25-Mar-16	12:25	572.80	11.5	46.63	‡ ‡
	1-Apr-16	16:11	543.60	26.0	33.48	‡ ‡
	8-Apr-16	9:38	513.90	157.0	19.76	‡ ‡

Volume Adjusted Data¹

	Matric Potential (-cm water)	Adjusted Volume (cm ³)	% Volume Change ² (%)	Adjusted Density (g/cm ³)	Adjusted Calculated Porosity (%)
Hanging column:	0.0				
	4.0	218.44	-3.01%	1.45	45.40
	11.5	216.87	-3.70%	1.46	45.00
	26.0	214.80	-4.62%	1.47	44.47
	157.0	213.65	-5.13%	1.48	44.17

Comments:

- ¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent each of the volume change measurements obtained after saturated hydraulic conductivity testing and throughout hanging column/pressure plate testing. "---" indicates no volume changes occurred.
- ² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

[†] Assumed density of water is 1.0 g/cm³

⁺⁺ Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

Technician Notes:



Moisture Retention Data Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: LTPQA-4 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40 Fraction of test sample used (<2.00mm fraction) (%): 100.00

Dry weight* of dew point potentiometer sample (g): 164.55

Tare weight, jar (g): 115.28

	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content [†] (% vol)	
Dew point potentiometer:	25-Mar-16	12:33	168.63	918	12.25	
	22-Mar-16	13:10	167.31	10504	8.29	‡ ‡
	18-Mar-16	9:30	166.47	69142	5.77	‡ ‡
	15-Mar-16	10:10	165.75	722120	3.60	

	Volume Adjusted Data ¹				
	Water Potential	Adjusted Volume	% Volume Change ²	Adjusted Density	Adjusted Calc. Porosity
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)
Dew point potentiometer:	918	213.65	-5.13%	1.48	44.17
	10504	213.65	-5.13%	1.48	44.17
	69142	213.65	-5.13%	1.48	44.17
	722120	213.65	-5.13%	1.48	44.17

Comments:

¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

⁺ Adjusted for >2.00mm (#10 sieve) material not used in DPP/RH testing. Assumed moisture content of material >2.00mm is zero, and assumed density of water is 1.0 g/cm³.

^{##} Volume adjustments are applicable at this matric potential (see comment #1).



Moisture Retention Data

Dew Point Potentiometer / Relative Humidity Box

(Soil-Water Characteristic Curve)

Sample Number: LTPQA-4 (<2mm, 1.4g/cc)

Initial sample bulk density (g/cm³): 1.40 Fraction of test sample used (<2.00mm fraction) (%): 100.00

Dry weight* of relative humidity box sample (g): 81.61

Tare weight (g): 44.09

_	Date	Time	Weight* (g)	Water Potential (-cm water)	Moisture Content [†] (% vol)	_
Relative humidity box:	15-Mar-16	10:40	82.53	845560	3.65	
	Volume Adjusted Data ¹					
	Water	Adjusted	% Volume	Adjusted	Adjusted	
	Potential	Volume	Change ²	Density	Calc. Porosity	
	(-cm water)	(cm ³)	(%)	(g/cm ³)	(%)	
Relative humidity box:	845560	213.65	-5.13%	1.48	44.17	_

Comments:

¹ Applicable if the sample experienced volume changes during testing. 'Volume Adjusted' values represent the volume change measurements obtained after the last hanging column or pressure plate point. "---" indicates no volume changes occurred.

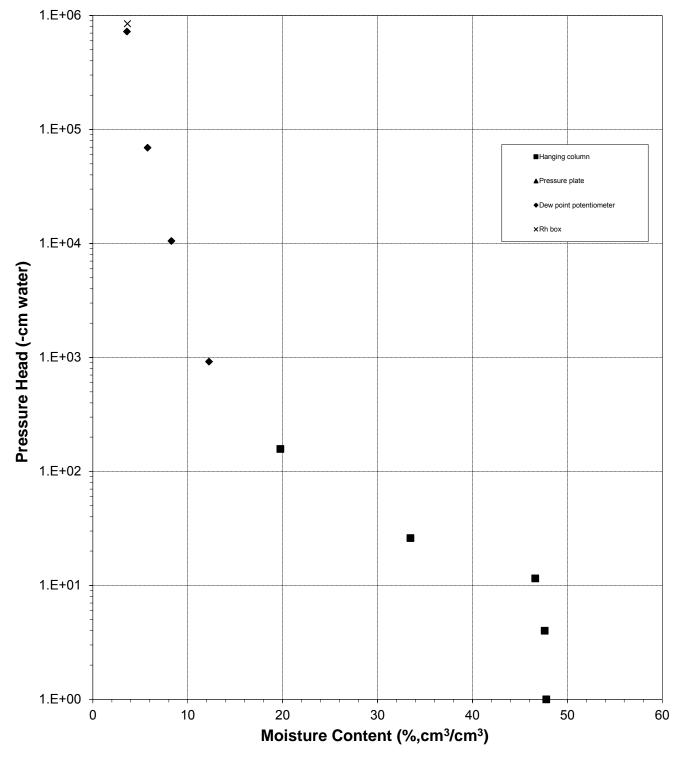
² Represents percent volume change from original sample volume. A '+' denotes measured sample swelling, a '-' denotes measured sample settling, and '---' denotes no volume change occurred.

* Weight including tares

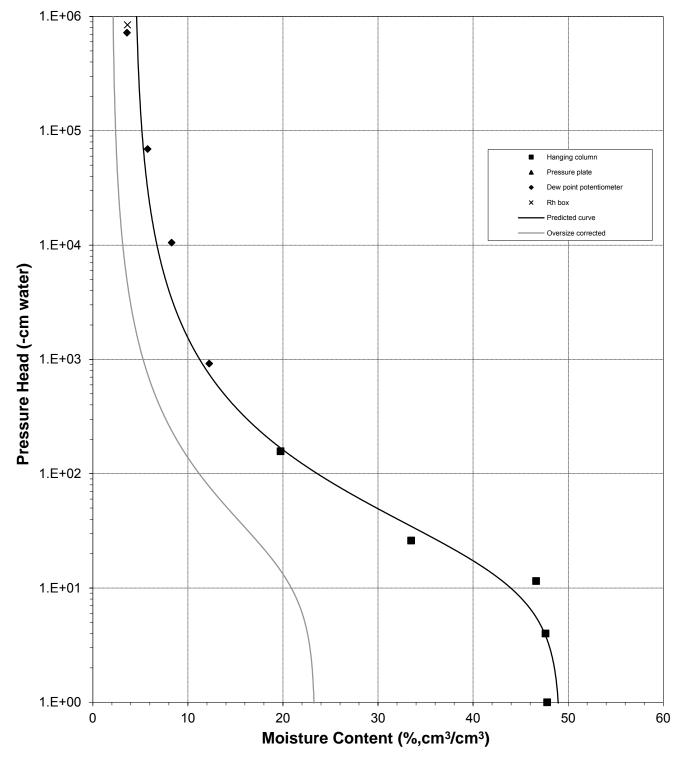
⁺ Adjusted for >2.00mm (#10 sieve) material not used in DPP/RH testing. Assumed moisture content of material >2.00mm is zero, and assumed density of water is 1.0 g/cm³.

^{##} Volume adjustments are applicable at this matric potential (see comment #1). Changes in volume, if applicable, are estimated based on obtainable measurements of changes in sample length and diameter.

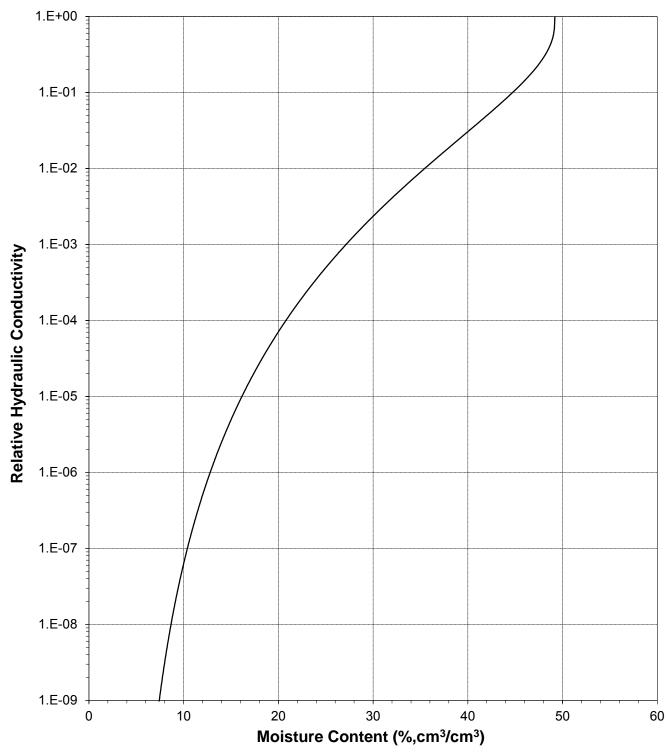




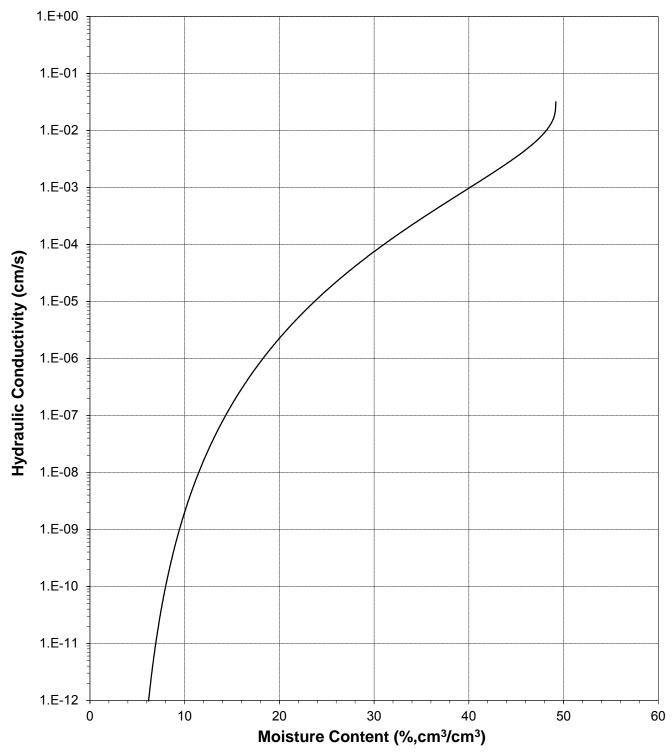
Water Retention Data Points



Predicted Water Retention Curve and Data Points



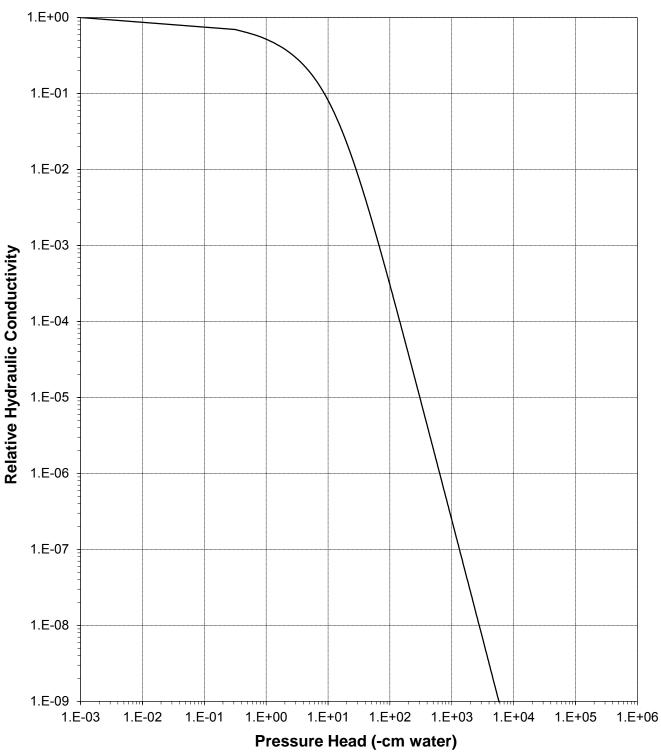
Plot of Relative Hydraulic Conductivity vs Moisture Content



Plot of Hydraulic Conductivity vs Moisture Content

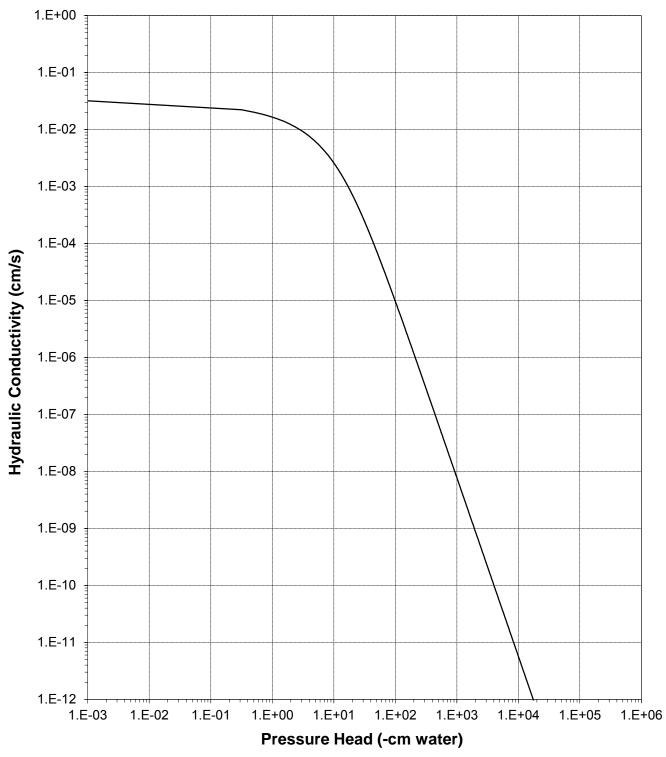
Sample Number: LTPQA-4 (<2mm, 1.4g/cc)





Plot of Relative Hydraulic Conductivity vs Pressure Head

Sample Number: LTPQA-4 (<2mm, 1.4g/cc)



Plot of Hydraulic Conductivity vs Pressure Head

Sample Number: LTPQA-4 (<2mm, 1.4g/cc)



Oversize Correction Data Sheet

)
)

Split (3/4", 3/8", #4): #10

	Coarse Fraction*	Fines Fraction**	<u>Composite</u>
Subsample Mass (g):	5018.47	2406.12	7424.59
Mass Fraction (%):	67.59	32.41	100.00
Initial Sample θ_i			
Bulk Density (g/cm ³):	2.65	1.40	2.06
Calculated Porosity (% vol):	0.00	47.04	22.35
Volume of Solids (cm ³):	1893.76	907.97	2801.73
<i>Volume of Voids</i> (cm ³):	0.00	806.41	806.41
<i>Total Volume</i> (cm ³):	1893.76	1714.38	3608.15
Volumetric Fraction (%):	52.49	47.51	100.00
Initial Moisture Content (% vol):	0.00	10.33	4.91
Saturated Sample θ_s			
Bulk Density (g/cm ³):	2.65	1.40	2.06
Calculated Porosity (% vol):	0.00	47.04	22.35
Volume of Solids (cm ³):	1893.76	907.97	2801.73
<i>Volume of Voids</i> (cm ³):	0.00	806.41	806.41
<i>Total Volume</i> (cm ³):	1893.76	1714.38	3608.15
Volumetric Fraction (%):	52.49	47.51	100.00
Saturated Moisture Content (% vol):	0.00	49.19	23.37
Residual Sample θ_r			
Bulk Density (g/cm ³):	2.65	1.48	2.11
Calculated Porosity (% vol):	0.00	44.17	20.41
Volume of Solids (cm ³):	1893.76	907.97	2801.73
<i>Volume of Voids</i> (cm ³):	0.00	718.40	718.40
<i>Total Volume</i> (cm ³):	1893.76	1626.37	3520.13
Volumetric Fraction (%):	53.80	46.20	100.00
Residual Moisture Content (% vol):	0.00	4.31	1.99
Ksat (cm/sec):	NM	3.2E-02	1.0E-02

* = Porosity and moisture content of coarse fraction assumed to be zero.

** = Volume adjusted, if applicable. See notes on Moisture Retention Data pages.

NM = Not measured

Laboratory analysis by: D. O'Dowd Data entered by: D. O'Dowd Checked by: J. Hines

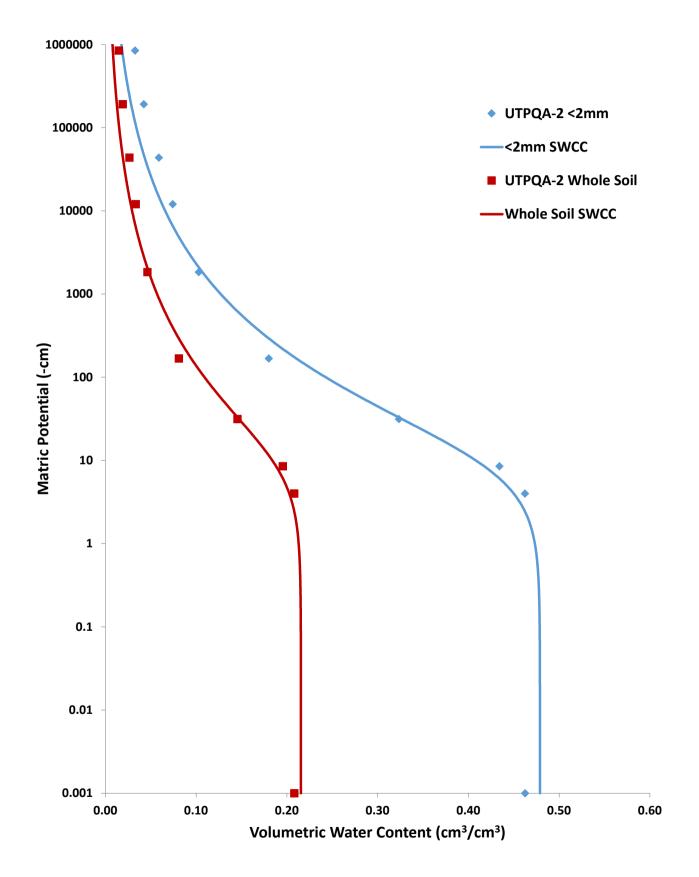
Laboratory Tests and Methods



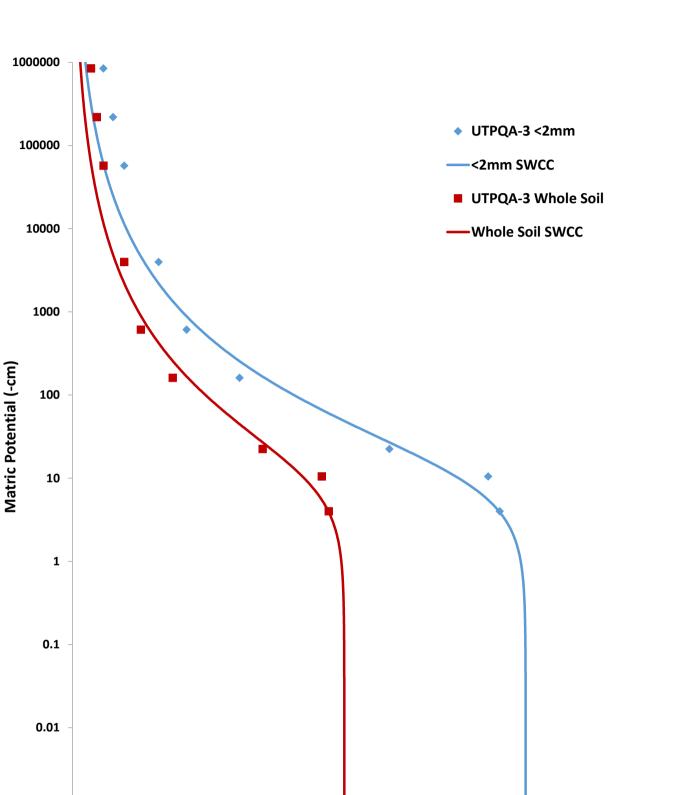
Tests and Methods

Dry Bulk Density:	ASTM D7263
Moisture Content:	ASTM D7263, ASTM D2216
Calculated Porosity:	ASTM D7263
Saturated Hydraulic Conductivit Constant Head: (Rigid Wall)	y: ASTM D 2434 (modified apparatus)
Hanging Column Method:	ASTM D6836 (modified apparatus)
Pressure Plate Method:	ASTM D6836 (modified apparatus)
Water Potential (Dewpoint Potentiometer) Method:	ASTM D6836
Relative Humidity (Box) Method:	Campbell, G. and G. Gee. 1986. Water Potential: Miscellaneous Methods. Chp. 25, pp. 631-632, in A. Klute (ed.), Methods of Soil Analysis. Part 1. American Society of Agronomy, Madison, WI; Karathanasis & Hajek. 1982. Quantitative Evaluation of Water Adsorption on Soil Clays. SSA Journal 46:1321-1325
Moisture Retention Characteristics & Calculated Unsaturated Hydraulic Conductivity:	ASTM D6836; van Genuchten, M.T. 1980. A closed-form equation for predicting the hydraulic conductivity of unsaturated soils. SSSAJ 44:892-898; van Genuchten, M.T., F.J. Leij, and S.R. Yates. 1991. The RETC code for quantifying the hydraulic functions of unsaturated soils. Robert S. Kerr Environmental Research Laboratory, Office of Research and Development, U.S. Environmental Protection Agency, Ada, Oklahoma. EPA/600/2091/065. December 1991
Coarse Fraction (Gravel) Correction (calc):	ASTM D4718; Bouwer, H. and Rice, R.C. 1984. Hydraulic Properties of Stony Vadose Zones. Groundwater Vol. 22, No. 6

APPENDIX B SOIL WATER CHARACTERISTICS CURVES







0.20

0.10

0.30

Volumetric Water Content (cm³/cm³)

0.40

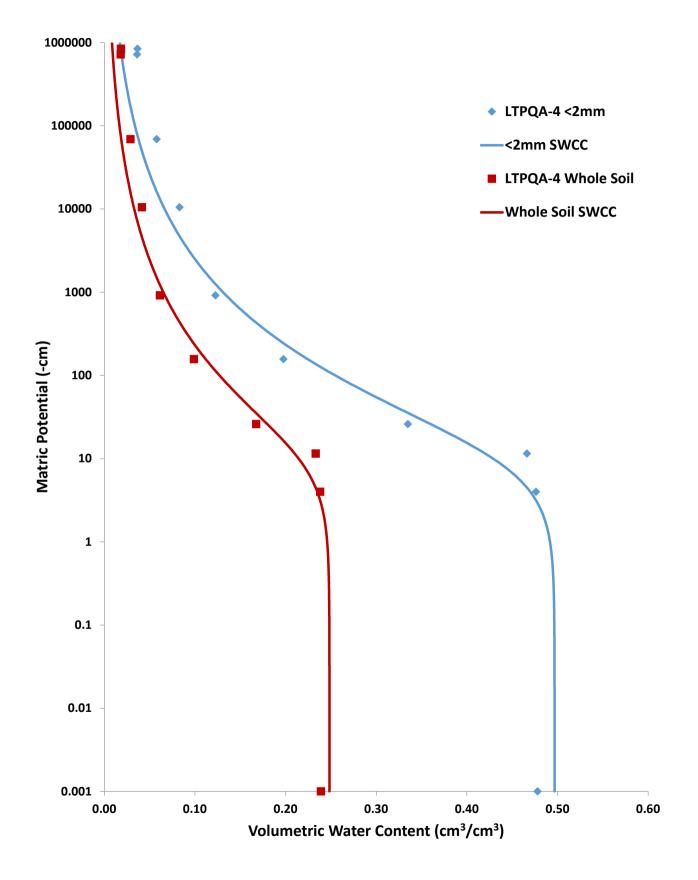
0.50



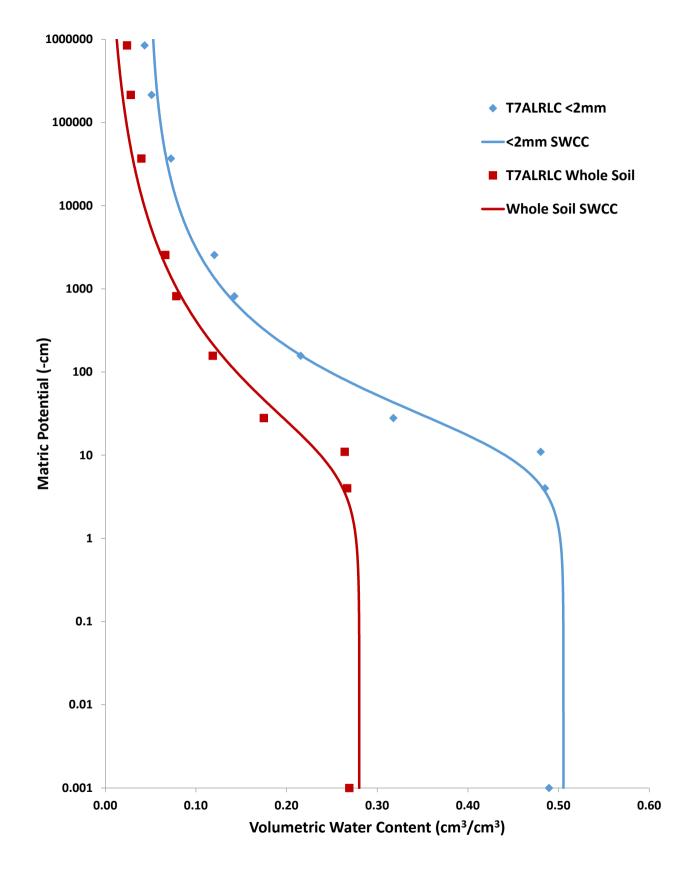
0.60

0.001

0.00

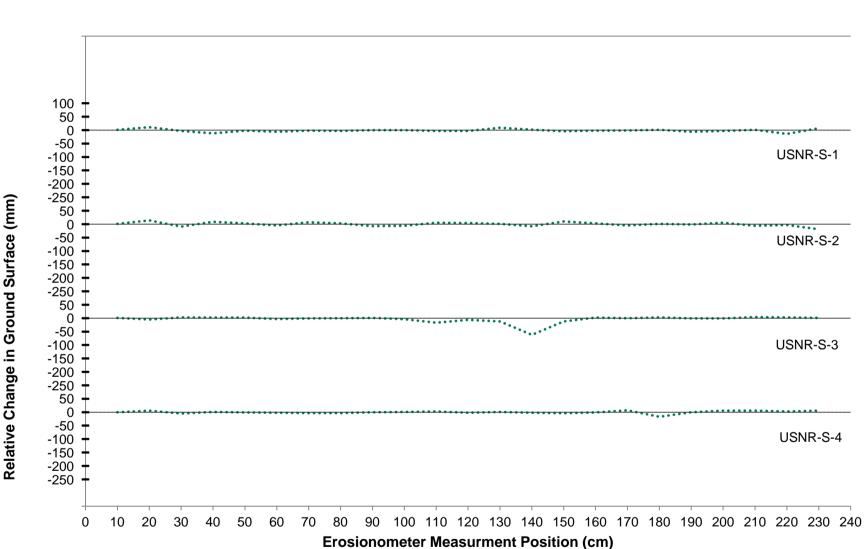








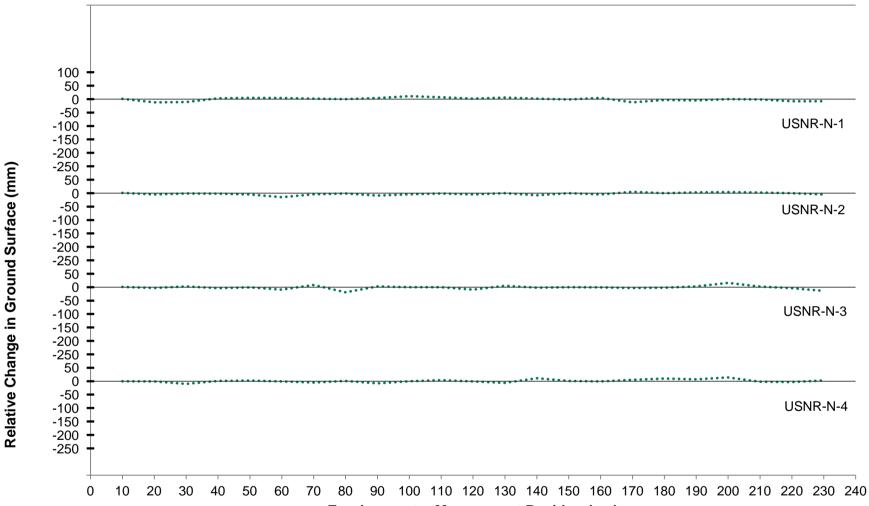
APPENDIX C EROSION STATION CROSS-SECTIONS



Golder

Figure C-1: USNR South Transect



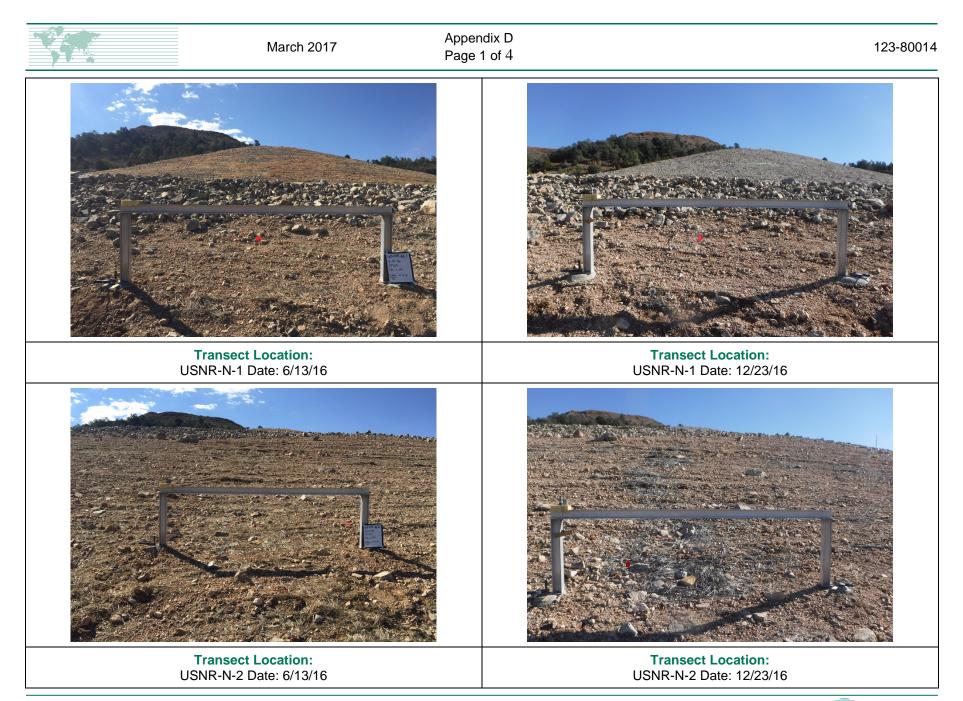


Erosionometer Measurment Position (cm)

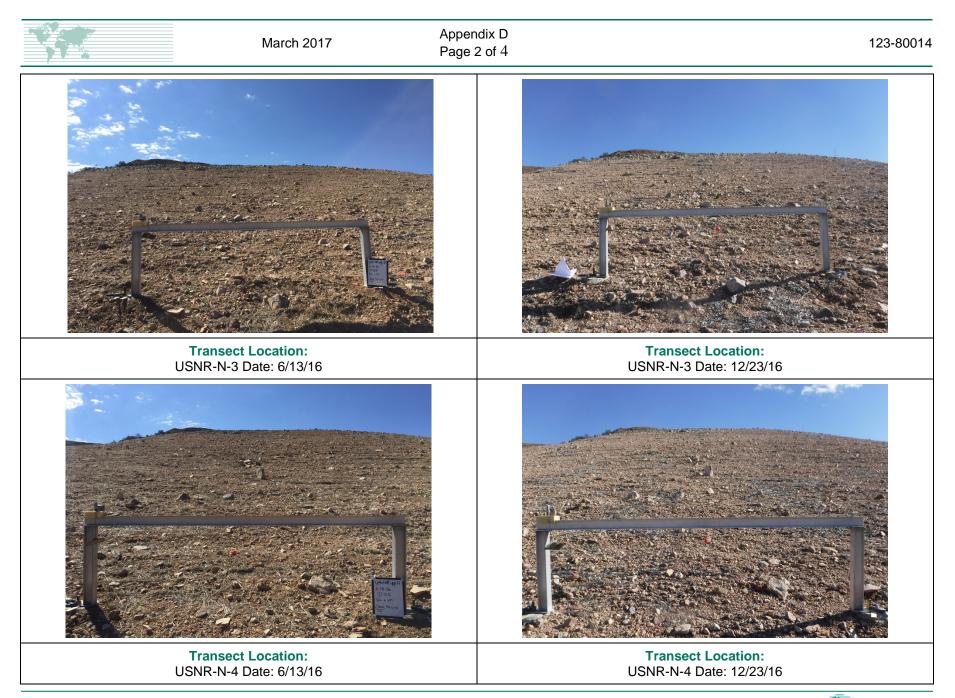


123-80014

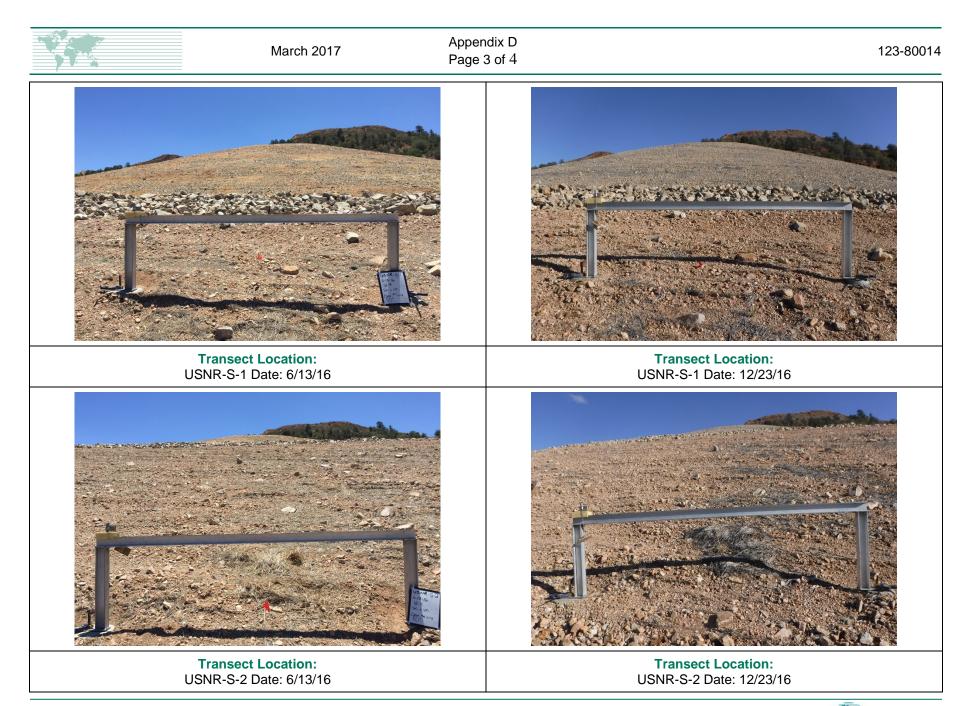
APPENDIX D EROSION TRANSECT PHOTOGRAPHS



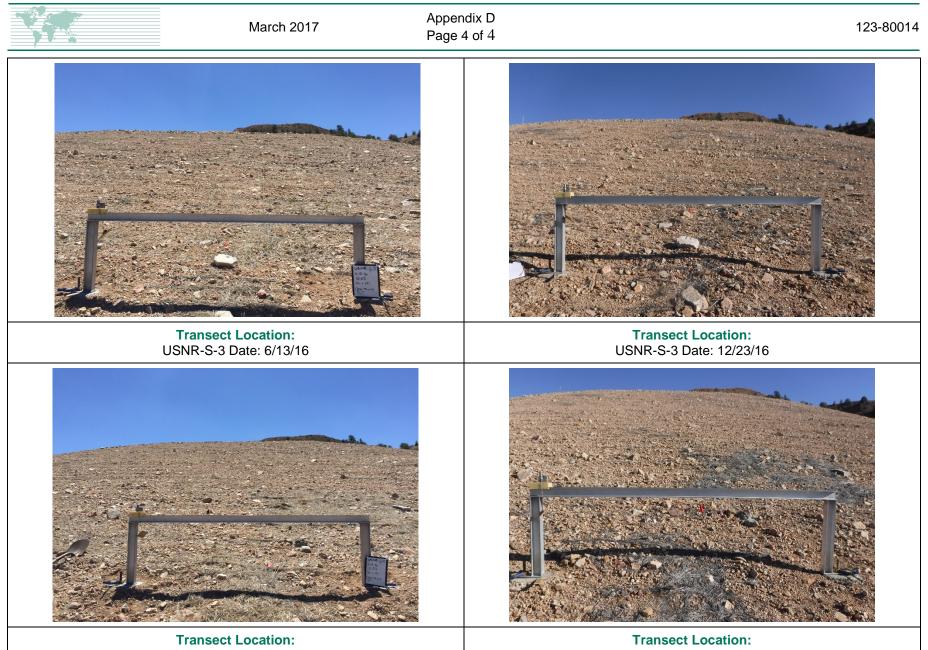












USNR-S-4 Date: 6/13/16

USNR-S-4 Date: 12/23/16



Established in 1960, Golder Associates is a global, employee-owned organization that helps clients find sustainable solutions to the challenges of finite resources, energy and water supply and management, waste management, urbanization, and climate change. We provide a wide range of independent consulting, design, and construction services in our specialist areas of earth, environment, and energy. By building strong relationships and meeting the needs of clients, our people have created one of the most trusted professional services organizations in the world.

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