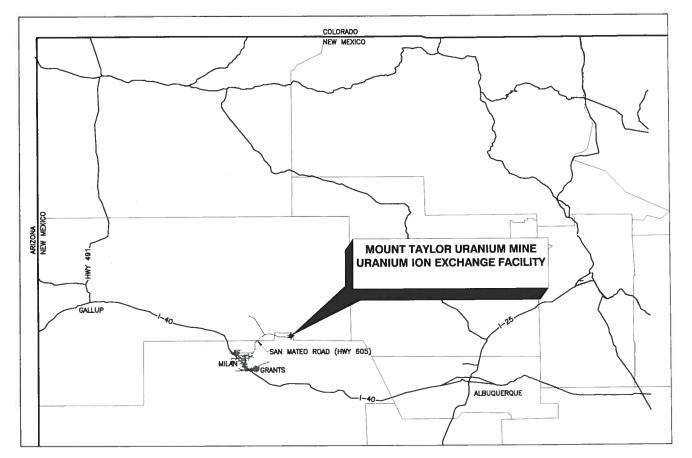
APPENDIX D

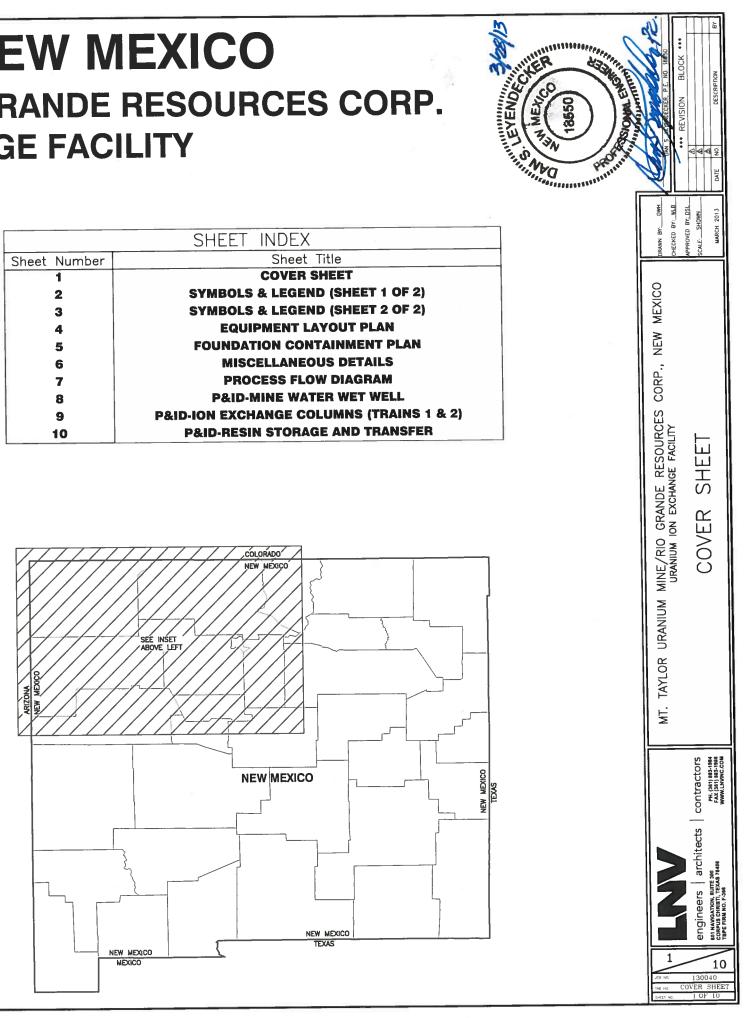
ION EXCHANGE PLANT DESIGN

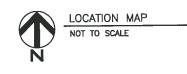
- Operation and Maintenance Manual
 - Plans

CIBOLA COUNTY, NEW MEXICO MOUNT TAYLOR URANIUM MINE/RIO GRANDE RESOURCES CORP. **URANIUM ION EXCHANGE FACILITY**



		SHEET INDEX
Sł	neet Number	Sheet Title
	1	COVER SHEE
	2	SYMBOLS & LEGEND (S
	3	SYMBOLS & LEGEND (S
	4	EQUIPMENT LAYOU
	5	FOUNDATION CONTAIN
	6	MISCELLANEOUS D
	7	PROCESS FLOW DI
	8	P&ID-MINE WATER V
	9	P&ID-ION EXCHANGE COLUM
	10	P&ID-RESIN STORAGE A







FUNCTION SYMBOLS:								
	CONTROL ROOM	FIELD MOUNTE	ED AUXILLIARY CONTROL PANEL NORMALLY ACCESSIBLE TO OPERATOR					
DISCRETE		\bigcirc	\bigcirc					
DCS	\square	\bigcirc						
COMPUTER FUNCTION		\bigcirc	\ominus					
PLC	\bigcirc		\bigcirc					
LINE	SYMBOLS:	_						
			FLOW LINE					
			CONTROL LINE (ELECTRICAL)					
			HARDWIRE					
	0		DATA COMMUNICATIONS RS485, RS422 BETWEEN PLC AND DCS					
		0-0-0-	PID CONTROL LOOP					
			AIR SUPPLY					
	\diamond		INTERLOCK					
	SVH		SET VALUE HIGH (DCS) FOR VFD.					
	SVL		SET VALUE LOW (DCS) FOR VFD.					
	MV		MANIPULATED VARIABLE FOR VFD.					
	PV		PROCESS VARIABLE FOR VFD.					
LINE	CONTINUA	TION ARI	ROWS:					

CONTINUATION	AKKUWS:	
		_

DWG. NUMBER - TO/FROM NON-ADJACENT DRAWING

- TO/FROM ADJACENT DRAWING

ABBREVIATIONS

 \rightarrow

- FIBERGLASS REINFORCED STEEL RUBBER LINED STEEL STAINLESS STEEL CARBON STEEL (PVC) POLYVINYL CHLORIDE RESIN IN RESIN OUT MINE WATER RESIN TRANSFER WATER

- FRP RLS SS STEEL LPB RO RI MW RTW

MECHANICAL	SYMBOLS:	VAL	VE SYMBOLS:
	PUMP		🗘 VALVE –
D	REDUCER		VALVE -
11	FLANGE JOINT		
I —	CAMLOCK FITTING	jbe va	KOI BALL VAL
T	FILTER	רו ני	BUTTERFL
M	FLEXIBLE JOINT		
\cap \square	VENTS	۵ ۱۷	
AG	AGITATOR	1 V	PRESSUR SPRING (
_ 	MANHOLE		PRESSUR OPERATE
Ŷ	PULSE DAMPENER		PRESSUR
R	RECEIVER		BACK PR OPERATE XXX PRESSUR
Ś	RADIOACTIVE SOURCE	L	CHECK V
)/	EDUCTOR		Ŧ
- E- ///- E=	FLEXIBLE HOSE	1	KNIFE G
	SONIC LEVEL SENSOR		
Ê	VERTICAL TURBINE PUMP		
<u>ج</u>			CONTROL 4-20mA
		v	MANUAL VXXX
			STRAINE

MISCELLANEOUS SYMBOLS:



MOTOR ACTUATED VALVE WITH MANUAL HANDWHEEL

MAG METER



VXXX L VALVE ID TRAIN (IF APPLICABLE) PROCESS VALVE

2 3 200 *<i>iter* 233 EVENDE 8550 VALVE - GENERAL MEA VALVE - NORMALLY CLOSED BALL VALVE HI HALLING BUTTERFLY VALVE MLB Ξ DIAPHRAGM VALVE MANUALLY OPERATED CKED MN PRESSURE RELIEF VALVE SPRING OPERATED CORP., NEW MEXICO PRESSURE REDUCING VALVE OPERATED BY DOWNSTREAM FLOW DIRECTION PRESSURE BACK PRESSURE VALVE OPERATED BY UPSTREAM - FLOW DIRECTION PRESSURE CHECK VALVE URANIUM MINE/RIO GRANDE RESOURCES C URANIUM ION EXCHANGE FACILITY SYMBOLS & LEGEND (SHEET 1 OF 2) KNIFE GATE VALVE HAND VALVE MANUALLY OPERATED CONTROL VALVE - FLOW MODULATING 4-20mA /PREUMATIC OPERATED MANUAL OVER-RIDE STRAINER VALVE NOMENCLATURE PROCESS - 0 MINE WATER ION EXCHANGE — 1 TAYLOR - 2 RESIN OUT — 3 RESIN IN 4 RESIN TRANSFER WATER MT. Inchitects Contractors Ľ 2 202 10 130040 SYMBOL

XX = EQUIPMENT ID.

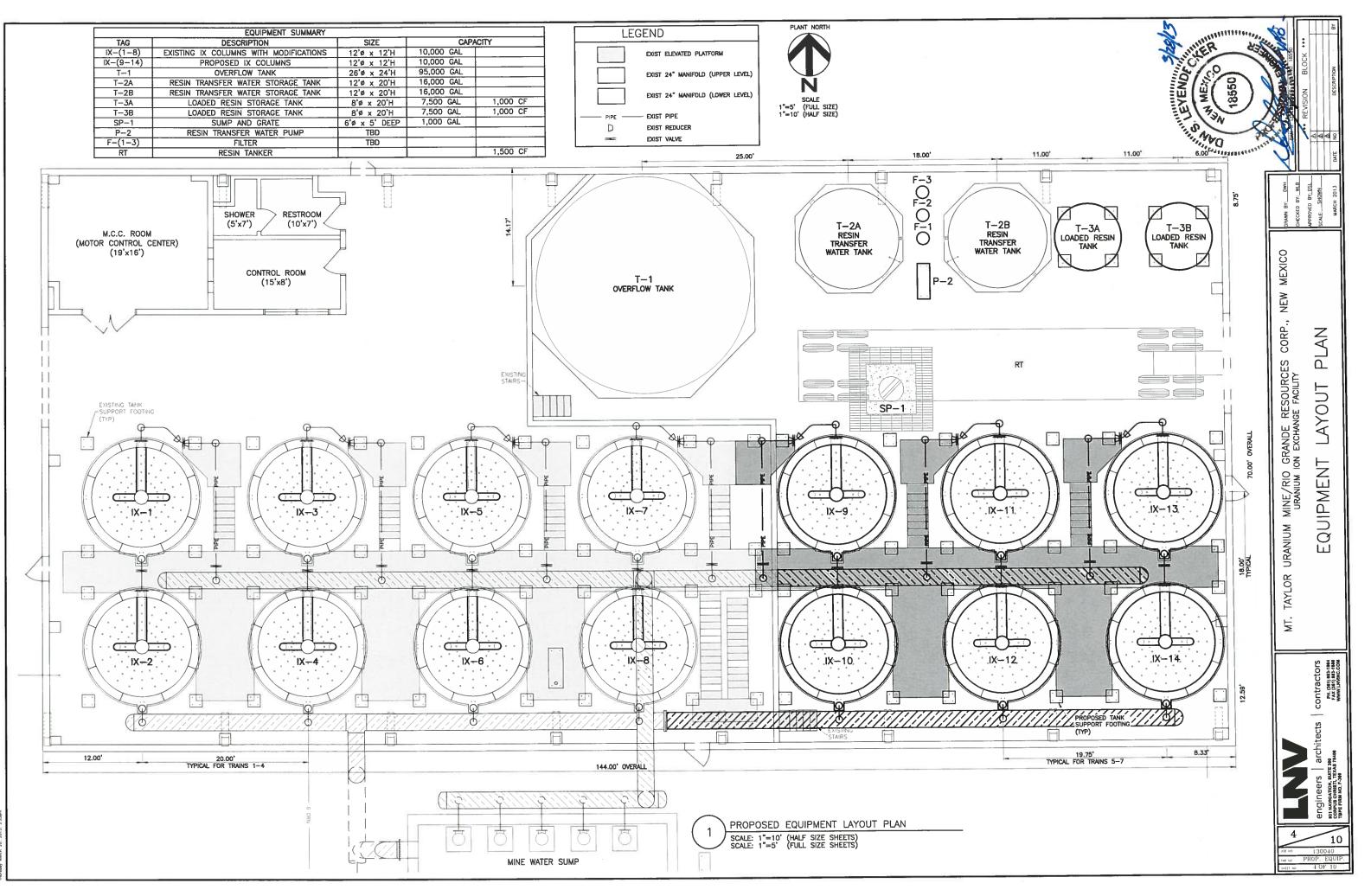
1	
— мw	MINE WATER
	ION EXCHANGE COLUMN (1-14)
- RI	RESIN IN
- RO	RESIN OUT
T1	OVERFLOW TANK
T 2A	RESIN TRANSFER WATER STORAGE TANK
— т-2В	RESIN TRANSFER WATER STORAGE TANK
— T-3A	LOADED RESIN STORAGE TANK
— T-3B	LOADED RESIN STORAGE TANK SUMP PUMP
SP-1	SUMP PUMP

	LEVEL INDICATOR
FI	FLOW INDICATOR
LT XX	LEVEL TRANSMITTER
(FT XX	FLOW TRANSMITTER
	LEVEL VALVE
(FCV XX	FLOW CONTROL VALVE
	LEVEL INDICATOR TRANSMITTER
(FIT XX	FLOW INDICATOR TRANSMITTER
LS	LEVEL SWITCH
LSH	LEVEL SWITCH HIGH
LSL XX	LEVEL SWITCH LOW
LSHL XX	LEVEL SWITCH HIGH LOW
	LEVEL CONTROL VALVE
(FE XX	FLOW SENSOR ELEMENT
LE	LEVEL SENSOR ELEMENT
(VFD XX	VARIABLE FREQUENCY DRIVE

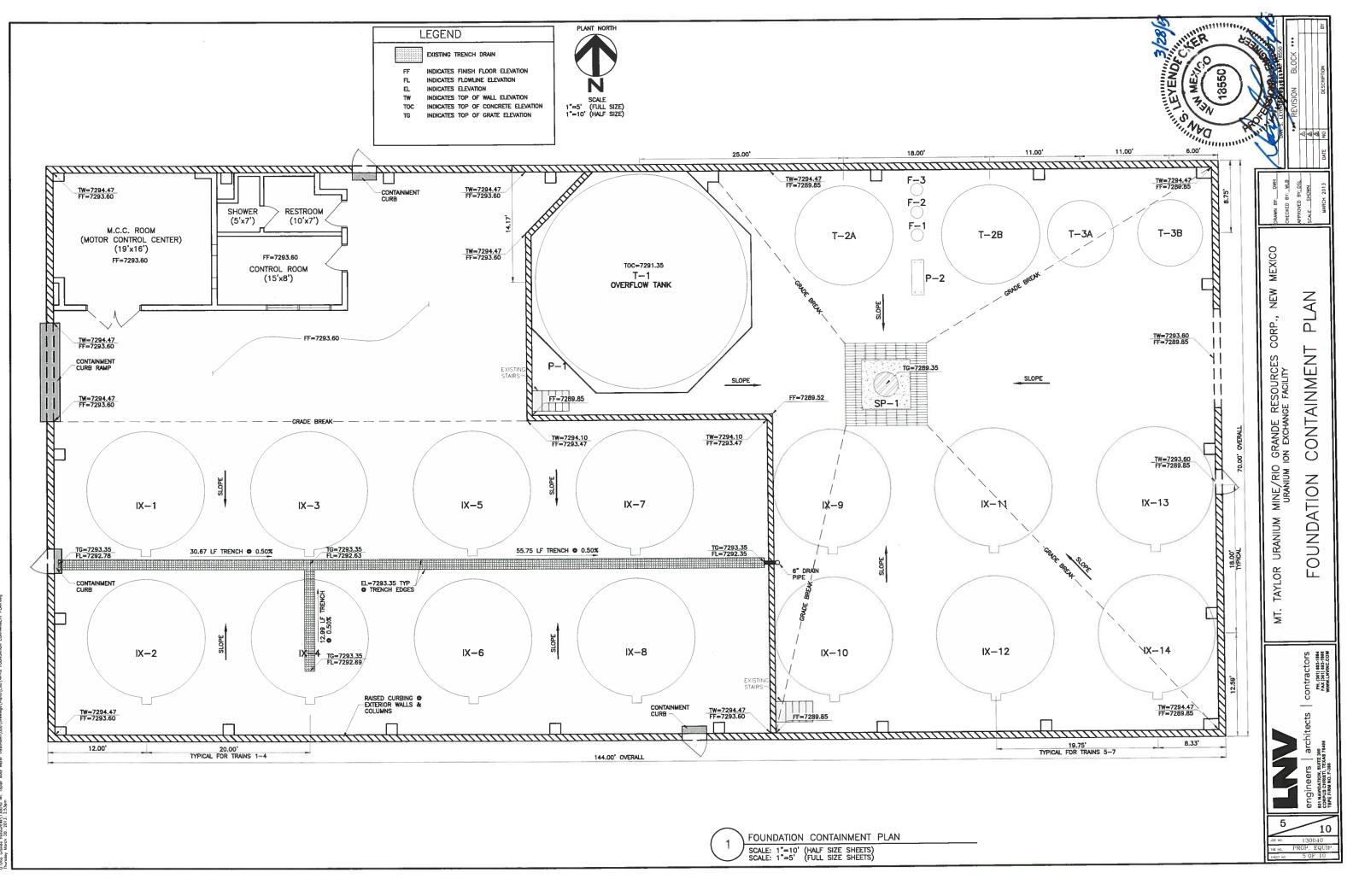
P&ID SYMBOLS; FIELD INSTRUMENTS

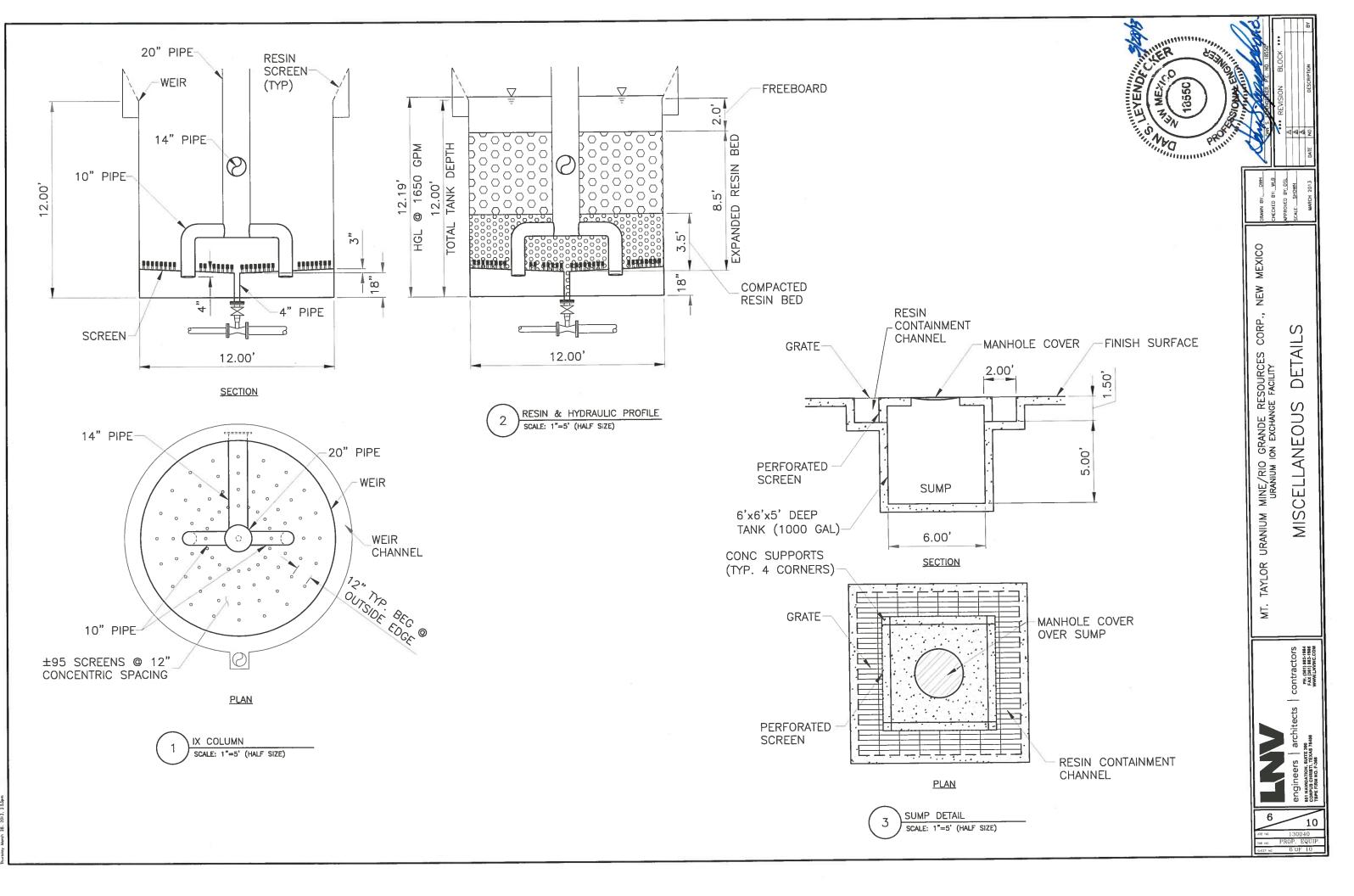
AHH	LEVEL ALARM HIGH HIGH by (
LAH	LEVEL ALARM HIGH by DCS
	LEVEL ALARM LOW by DCS
	LEVEL ALARM LOW LOW by D
FAL	FLOW ALARM LOW by DCS
FAH	FLOW ALARM HIGH by DCS
LIC XX	LEVEL INDICATOR CONTROL 6
FIC XX	FLOW INDICATOR CONTROL by
FR	FLOW RECORDER by DCS

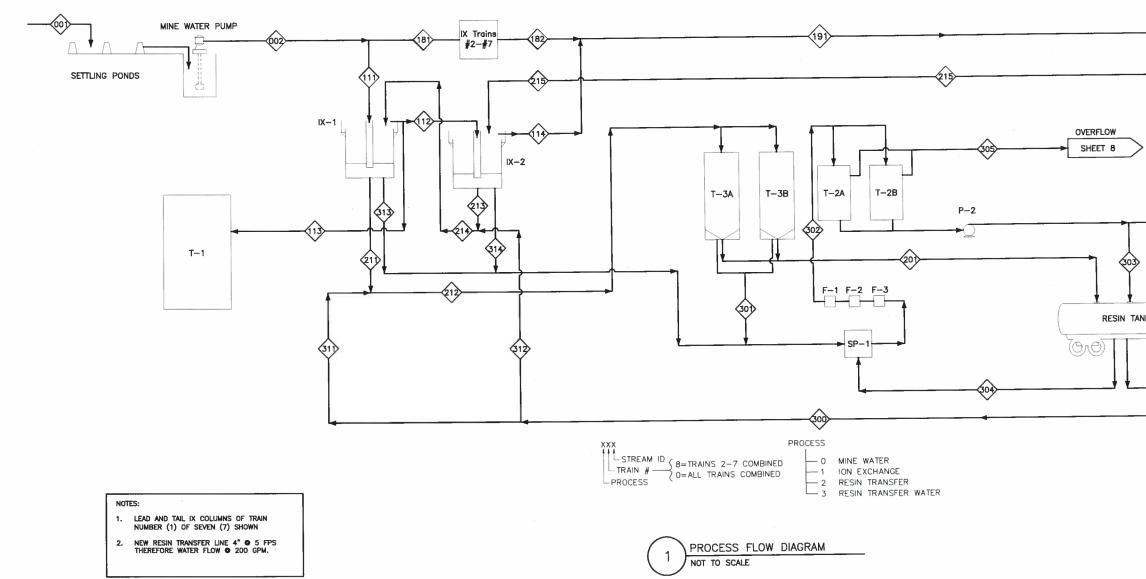
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				MT. TAYLOR URANIUM MINE/RIO GRANDE RESOURCES CORP., NEW MEXICO URANIUM ION EXCHANCE FACILITY		(SHEEL 2 OF 2)
				3 <u>17</u> 102 12 102	engineers architects c	
				SHEET NC:	3 OF	10



Wilso Gande Resources/1.00040 ML. Taylor Wite: Treatment/1000/Dramogs/Poors/Cimi/4-IX PR0P0SED EQUIPUENT LND Dr. Hornes, You 2011, 1.511-0.

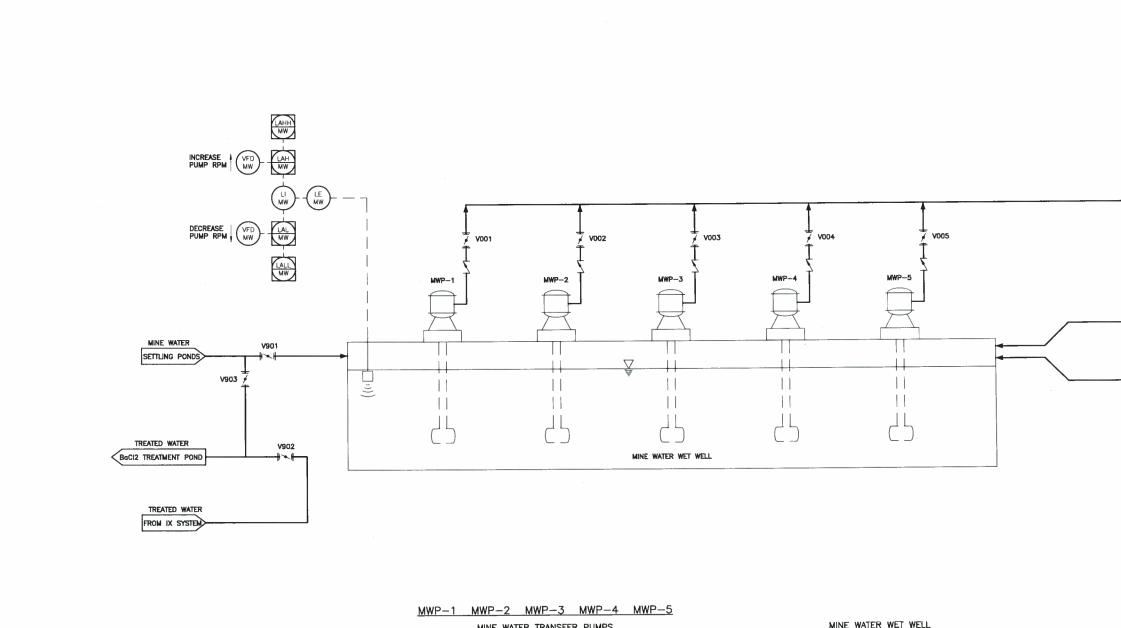






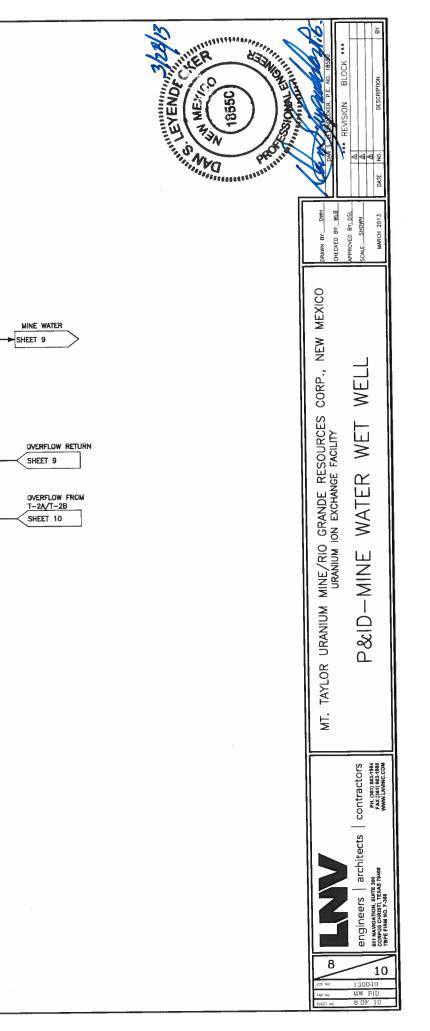
FLOW AND MASS BALANCE																							
PROCE	PROCESS ION EXCHANGE											RESIN TRANSFER							RESI				
STREAM	NO		001	002	111	112	113	114	181	182	191	201	211	212	213	214	215	300	301	302	303		
DESCRIP			RAW MINE WATER	SETTLED MINE WATER	TRAIN #1	TRAIN #1 LEAD COLUMN	OVERFLOW	TRAIN #1 TAIL COLUMN TREATED WATER		IX TRAINS #2		LOADED RESIN TO RESIN TANKER	TRAIN #1 LEAD COLUMN LOADED RESIN	LOADED RESIN AND RTW	TRAIN #1. TAIL COLUMN PARTIALLY LOADED RESIN	PARTIALLY LOADED RESIN AND RTW	STRIPPED RESIN	RTW TO EDUCTOR OF LEAD OR TAIL IX COLUMN	LOADED RESIN STORAGE TANK RTW RETURN	FILTERED WATER BACK TO RTW STORAGE TANK	RESIN TRANSFER WATER TO RESIN TANKER	R TA WA S	
	Q _{ux}	(gpm)	10,000	10,000	1,429	1,429	-	1,429	8,571	8,571	10,000	-	-	-	-	-	-	-	-	-		-	
	Q _{tx}	(ft ³ /min)	1,337	1,337	191	191		191		1,146	1,337	•	-	-	-	-	-	-	•			-	
ION EXCHANGE	SOLIDS	(mg/L)	1,000		100	100		100				•	-	-	-	-	-	•	-			ŀ	
	SOUDS	(Tons/h)	2.5		0.04	0.04		0.04	0.21	0.21	0.25	•	•	-	•	-	•		-				
	TRANSFER TIME	(min)	-	•	-	*	-	-	-	•	-	120	120	120	120	120	120	120	120	120	12		
	SP.GR.	LIQUOR	1	1	1	1	-	1	1	1	1	1	1	1	1	1	1		1	·	-	1	
	U ₃ O ₈	(mg/l)	0.1	0.1	0.1	0.020		0.017	0.1	0.017	0.017	0.3	961	0.3	35	C	-		-			1	
TOTALS	U ₃ O ₈	(Ibs/day)	12	12	1.7	0.34		0.29	10.3	1.8	2.04	•			-		-	-					
	U ₃ O ₈	(lbs/ft ³)	0	0	0	0	-	C	0	0	0	0	0.06		0.002	+	-	-	-	20	20	1	
	QTOTAL	(gpm)	10,000	10,000	1,429	1,429	-	1,429	8,571	8,571	10,000		<u> </u>										
	Water	(Tons/h)	2,502	2,502	357		<u> </u>	357	+ · · · · ·					56 56		5 50				-		0	
	TOTAL	(Tons/h)	2,505	2,503	358	358	-	358	3 2,145	2,145	2,503	56	+	<u> </u>	+					-		-	
	QRESIN	(gpm)	•		•			-		•					<u> </u>			+		-	-	-	
RESIN TRANSFER	QRESIN	(ft³/min)	•		-	-	-	-				3.3					+	+		-	-	-	
	VRESIN	(ft ³)	·	•	~	•	-		<u> </u>	-		400		200		20			200.0	0 200.	0 20	0	
RESIN TRANSFER WATER	QRTW	(gpm)	•	•		-			-	•	·	200	+			20						7	
	Qatw	(ft ³ /min)	ŀ	-	-	-	-	•	-			2	/	2	<u></u>	<u> </u>		<u>′</u>	<u> </u>	·	· · · · ·	<u> </u>	

	- - 120 1 - -	-	RESIN TRANS 304 RESIN TRANS SUMP	>	
) - - - - - D -		OVERFLOW	305 RESIN TRANSFER WATER STORAGE TANK		
- 200 50 - - - 200.0	- - 120 1 -	-	311 RTW TO EDUCTOR OF LEAD COLUMN		
50 	- - 120 1 -	•	312 RTW TO EDUCTOR OF TAIL COLUMN		VENNIN, S / S / R
50 50 - - - 200.0	- - 120 1 - -	RETURN	313 TRAIN #1 LEAD COLUMN RTW RETURN	ALM MEXT	S SUMERIO BUILDE
50 50 - - - 200.0	- - 120 1 - -	RETURN	314 TRAIN #1 TAIL COLUMN RTW RETURN	And a state of the	18550
1 1					C
201 HO: 140 HO: 140 HO:			MT. TAYLOR URANIUM MINE/RIO GRANDE RESOURCES CORP., NEW MEXICO	DRAWN BY	REVISION BLOCK ***
engineers arc 0140 01000 01100 01000000	hitects c	Contractors PH. (381) 883-1984 FAX (381) 883-1986 WWW.LWWINC.COM	PROCESS FLOW DIAGRAM	APPRIOVED BYLDSL SCALE - SHOWN WARCH 2013 DATE NO	DESCRAPTION
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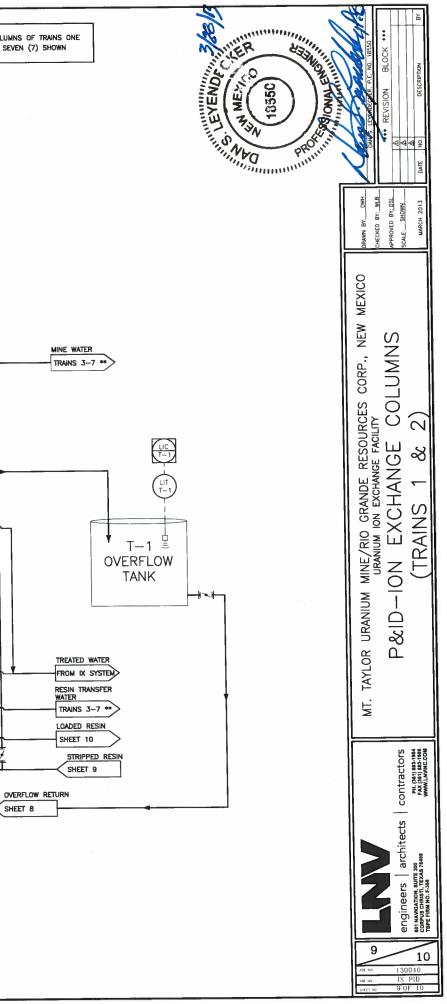
MINE WATER TRANSFER PUMPS GPM 2500 © 40 HEAD MOTOR HP: 40 MATERIAL: CAST STEEL, BRONZE TRIM MINE WATER WET WELL, SIZE: 30'x6'x8' CAPACITY: 10,800 GALLONS

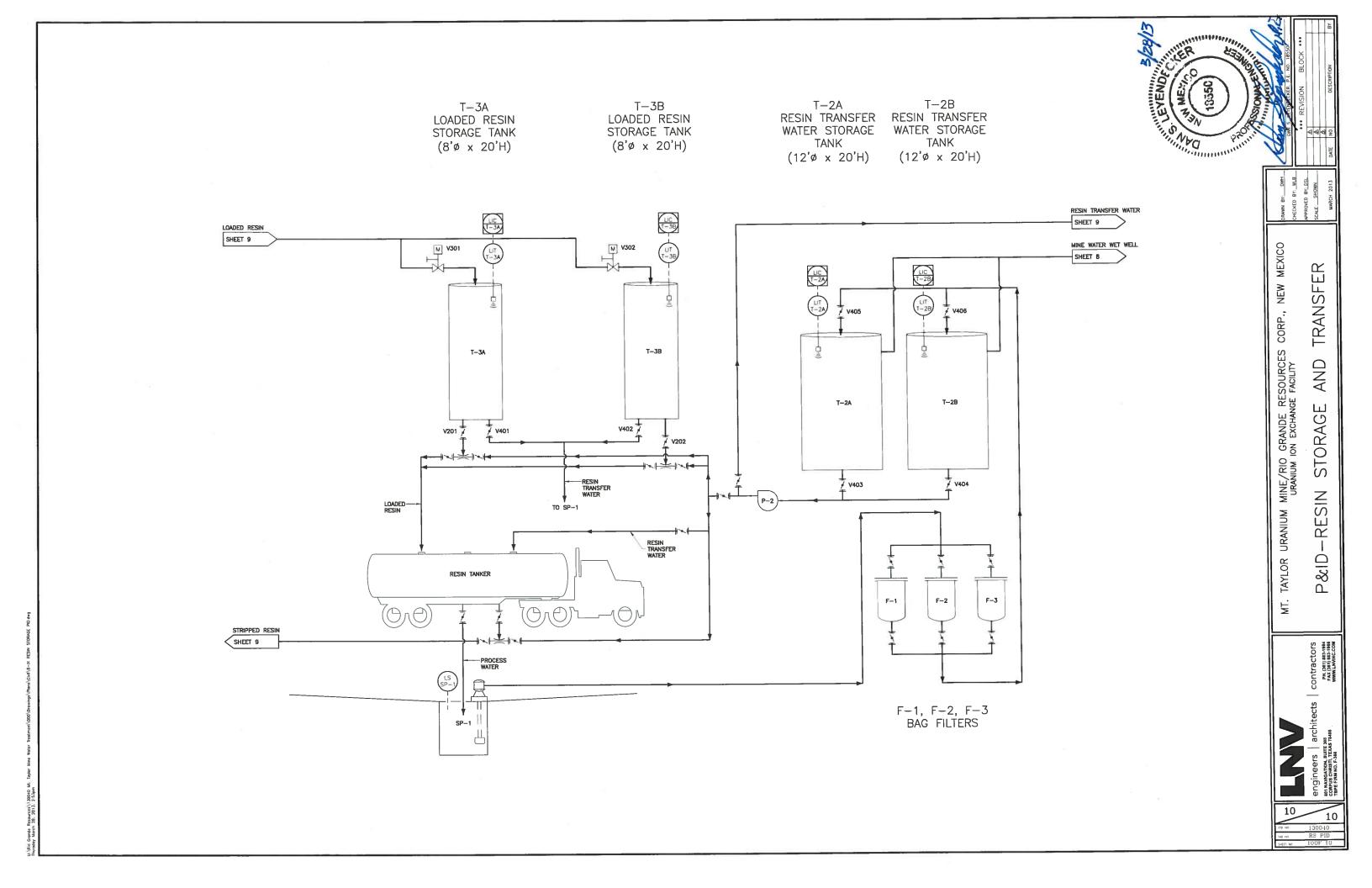
urces/120040 Mr. Toylor Wine Water Treatment\000\Drawings\Piane\Civili'(6-1X MakE WATER MET METL PO dag 2013, 233,pm



** LEAD AND TAIL IX COLUMNS OF TRAINS ONE (1) AND TWO (2) OF SEVEN (7) SHOWN IX-4 TAIL COLUMN IX-3 LEAD COLUMN IX-2 TAIL COLUMN IX-1 LEAD COLUMN train #2 TRAIN #2 TRAIN #1 TRAIN #1 FAL FR MW LAH 3 FIT LAHH 2 MINE WATER SHEET 8 FAH 3 V120 FAH 1 v110 $\begin{bmatrix} 1 \\ U \\ 1 \\ 1 \end{bmatrix} - \begin{bmatrix} F \\ 1 \\ 1 \end{bmatrix}$ FIC 3 FR 3 FR 1 $\begin{pmatrix} UT \\ 3 \end{pmatrix}$ V123 V113 FISH TAIL BFV SET TO OPEN 10% V122 V112 ļ TO OVERFLOW TANK (T-1) FCV 3 LCV 4 LCV 2 ļ 4<u>∼</u>+ v121 ¥4~↓ 111 V222 7 V221 7 V211 7 V212 7 **୷**୵୲<u></u>≹୲╲⊬ ୶୲୷୲ RESIN TRANSFER SHEET 10 V312 V311 ¥ V321 7 V322 🖡

SHEET 8





Operations & Maintenance Manual

Mt. Taylor Mine Mine Water Treatment Unit (MWTU) - IX Facility

LNV Project No. 130040



P.O. Box 1000 Hobson, TX 78117

Prepared by:



Phone: (361) 883-1984 Fax: (361) 883-1986 801 Navigation, Suite 300 Corpus Christi, Texas 78408



March 28, 2013

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2	. Test Method

Appendix A – Resin Spec Sheet

MT. TAYLOR URANIUM IX PLANT OPERATING MANUAL

I. <u>Background Information</u>

Rio Grande Resources (RGR) plans to re-open the Mt. Taylor uranium mine located outside of Grants, New Mexico. The existing mine has to be dewatered to enable access to the ore. To dewater the existing mine works and operate the mine in the future, an extensive water management system must be run in combination with a Mine Water Treatment Unit (MWTU) to remove uranium (U) from the mine water to enable discharge to an NPDES-permitted outfall north of the mine.

The water treatment will be operated in two main phases:

Phase 1 - Mine de-watering phase:

- Flow 8,000 -10,000 gallons per minute (gpm)
- U 0.07 parts per million (ppm) trend increasing
- TDS ~ 400 (ppm)

Phase 2 - Mine operation:

- Flow 4,000 -5,000 gpm
- U about 1 ppm (previous mining conditions, late phase)
- TDS 800 ppm

Discharge requirements:

- 30 parts per billion (ppb) U (human health standard in 20.6.2.3103.A(12)NMAC)

RGR considers U removal by ion exchange (IX) using the existing IX plant at the site as the primary option. IX loaded resin will be transferred to an off-site facility, duly licensed by the Nuclear Regulatory Commission (NRC) or an Agreement State, to be regenerated. The stripped resin will then be returned for reuse at the IX Plant.

RGR has put together a uranium removal system utilizing a proven IX process to meet the drinking water standard discharge requirements. The system will incorporate IX trains each consisting of two IX columns in series. Each IX column will have a load capacity of 400 cubic feet (ft³) of IX resin with a maximum loading capacity of 0.09 pounds of U per cubic foot of resin. Each train has been designed to handle a maximum flow rate of 1,650 gpm and will be operated at a nominal flow rate of 1,429 gpm. The individual trains will be sampled and assayed to insure that the discharge water will not exceed the discharge limits for uranium of 30 ppb. The IX columns are designed to transfer the resin in the lead IX column when it reaches a loading of about 0.06 pounds of U per cubic foot, to prevent discharge exceeding 30 ppb U. The loaded resin from the lead IX column will be transferred to one of two loaded resin storage tanks and then will be off loaded to a resin tanker. The resin tanker will transport the loaded resin to an off-site facility for regeneration.

Each of the IX columns will be operated in an up flow mode with safeguards to prevent resin leakage between IX columns or resin spills. Each of the IX columns will have safety devices to prevent resin spills as follows: 1) resin screens in the overflow of each column, 2) a level control system that will reduce the input flow rate to the lead IX column; and 3) a bypass on the tail column to reroute bypass fluid to an overflow storage tank. The fluid sent to the overflow storage tank will be recycled back to the main supply wet well where it will be fed to the lead IX column.

II. <u>Plant Function</u>

The Mt. Taylor IX Plant is designed to treat 10,000 gpm of mine water for removal of uranium. The ion exchange process for recovering uranium from mine water utilizes a quaternary amine incorporated onto a porous styrene divinylbenzene bead. The amine has the ability to give up anions in exchange for anions in solution, in this case,' uranium. When loaded with uranium to 0.06 pounds U per cubic foot the resin will be transported to an offsite facility to be regenerated with a concentrated brine solution in a split elution cycle. The regenerated resin will be returned to Mt. Taylor to be reused.

The following drawings should be referred to in conjunction with this Operation and Maintenance Manual (O&MM):

Drawing No.	Description
2	Symbols & Legend (Sheet 1 of 2)
3	Symbols & Legend (Sheet 2 of 2)
4	Equipment Layout Plan
5	Foundation Containment Plan
6	Miscellaneous Details
7	Process Flow Diagram
8	P&ID - Mine Water Wet Well
9	P&ID - IX Columns (Trains 1 & 2)
10	P&ID - Resin Storage and Transfer

III. <u>Facility Description</u>

Refer to Drawing Number 4 - Equipment Layout Plan for the location of the various items described below. The Mt. Taylor IX Plant consists of five mine water pumps, four operating and a spare, seven IX trains with two IX columns each (14 columns total), two loaded resin storage columns, one overflow storage tank and two resin transfer water storage tanks. All of the above equipment except the mine water pumps are enclosed within the building. Also housed inside of the building are the motor control center (MCC), office, control room and restroom.

A. <u>Mine Water Pumping</u>

Mine Water gravity flows from the treatment lagoons to a wet well located adjacent to the IX building on the south side. The wet well has dimensions of 30

ft. x 6 ft. x 8 ft. 4 in. deep. The mine water wet well is covered by a platform which supports the five mine water transfer pumps (MWP-1, 2, 3, 4, and 5). Each mine water pump has a capacity of 2,500 gpm. For the plants' capacity of 10,000 gpm, four pumps are operating with one full spare.

B. Ion Exchange

The IX portion of the facility is located within the building and consists of seven trains of two IX columns each (14 columns total). Each train has a capacity of 1,650 gpm or one-sixth the total plants flow. The IX trains are arranged so that water will gravity flow from the first (lead) column (IX-1, 3, 5, 7, 9, 11, and 13) in each train to the second (tail) column (IX-2, 4, 6, 8, 10, 12, and 14). Water from the tail column in each train will then gravity flow to the plant discharge. Each column is provided with overflow screens to prevent resin loss. Each column has a diameter of 12 ft with a 12 ft straight sidewall, and is loaded with approximately 400 ft³ of resin.

C. <u>Resin Transfer</u>

The resin transfer system consists of two resin transfer water storage tanks (T-2A/2B), a single process water pump (P-2), and two loaded resin storage tanks (T-3A/3B). The resin is transferred as a slurry with water and will incorporate the use of eductors at each vessel. Eductors are a type of device that uses liquid pressure as a motive force to effectively convey granular solids or slurries over relatively short distances. The eductors are supplied with process water from a 200 gpm centrifugal pump which is sufficiently sized for transferring resin from one vessel at a time.

Once the resin has been loaded with uranium in the IX columns, the resin from a given column will first be transferred to one of two loaded resin storage tanks, each capable of holding 1,000 ft^3 of resin. The purpose of the loaded resin storage tank is to temporarily hold loaded resin while it awaits transport to the offsite facility for regeneration. The loaded resin will then be transferred to a resin tanker that can hold up to 1,500 ft^3 of resin. This resin tanker will transport the loaded resin to the regeneration facility and then return regenerated resin back to Mt. Taylor to be put back into service.

Facilities are provided for hydraulic transport of the resin between the IX columns, loaded resin storage tanks, and resin tanker. To reduce water consumption, water used to transport resin throughout the facility will be recycled and stored in the resin transfer water storage tanks.

D. Instrumentation

The control system that RGR proposes to install in the IX Plant will be a computer-based system. It will incorporate an active screen for each process and will display real time activities of tank levels and process flow rates. This system will have input from flow transmitters and level transmitters. The IX system will

be monitored by operators and a Programmable Logic Controller (PLC) located in the control room.

E. <u>Plant Utility</u>

The following utility services are provided at the IX Facility: electricity, potable water, process water and instrument air. A 13.8 KV line delivers primary power from the Mt. Taylor Mine to a transformer for conversion to 440/220 volts. Distribution to plant users is through the MCC. Potable water is delivered to the IX Facility through an underground line originating at the Barium Chloride Building. Process water is provided at appropriate locations at a pressure of 60 pounds per square inch (psi). Filtered and dried instrument air is supplied by a 23.5 actual cubic feet per minute (ACFM) compressor at 100 psi for operation of pneumatic controls.

F. <u>Support Facilities</u>

Forced air heating is provided for the entire IX building. The office, MCC and restroom are air conditioned.

IV. <u>Plant Operation</u>

A. <u>Mine Water Pumping</u>

Refer to Drawing 8 - P&ID - Mine Water Wetl

- 1) The mine water wet well is equipped with an inlet line from the mine water ponds and a bypass line that can in emergency situations feed excess water to the radium removal system.
- 2) Under normal operations Valves V901 and V902 are fully open and the Isolation Valve V903 is closed.
- 3) The mine water pumping system is designed so that four of the five mine water transfer pumps will provide the necessary capacity. The fifth pump provides backup capacity.
- 4) Before starting the mine water pumps, the operator should select the desired wet well level for the level indicator controller (LIC located in the control room).
- 5) Two IX trains will be valved open to accept mine water flow and one mine water pump will be turned on. The operator will adjust fluid flow through both IX trains prior to placing a second pump and any additional trains in

service. This procedure will be followed until the desired water flow is obtained.

- 6) The mine water wet well is provided with level control which will automatically maintain a constant level within the wet well. This is accomplished through the use of Variable Frequency Drive (VFD) on each mine water pump (MWP-1, MWP-2, MWP-3, MWP-4 and MWP-5). The level controller is set at a predetermined elevation that will adjust the VFD accordingly to maintain this level set point. The level device will be installed in the wet well to cover the operating level range. In the event that the level continues to increase, the operator must manually reduce the incoming fluid to the mine water wet well. If the level drops below the low-low setting, the pumps will sequentially turn off to protect the pumps from insufficient fluid level.
- 7) To shut off the flow of water to the IX Plant, the following sequence should be observed:
 - Open Valve V903
 - Close Valves V901 & V902

The IX Plant will now be bypassed and all mine water will flow from the settling ponds to the Barium Chloride Treatment Facility.

- 8) To initiate flow of mine water to the IX Plant, the following sequence should be observed:
 - If Closed, Open Valves V901 & V902
 - Close Valve V903

The operator should visually observe the water levels in the mine water wet well at the IX Plant to insure that no obstructions are impeding the flow of water.

B. <u>Ion Exchange</u>

Refer to Drawing 9 - P&ID - IX Columns (Trains 1 & 2)

The IX Plant will utilize seven identical trains. Each train will have a capacity of 1,650 gpm and will consist of two (2) 12-foot diameter columns in each train. The operation of one train is described below as an example. The components and functions will be identical for the remaining trains.

Feed water is delivered by the mine water transfer pumps to the main plant header. This 24-inch diameter header is located above the IX columns. A mag

meter (M-MW) is located in the header with a flow recorder (FR-MW) and low flow alarm (FAL-MW) is located in the control room.

Prior to initiating flow to the IX columns, the operator should check the resin drain Valves V211 and V212, located below the IX column tank, to insure that they are both closed. Valves V112 and LCV-2 should be closed. Valve V110 should now be opened. The flow control valve (FCV-1) will regulate the flow to the IX train.

To begin flow to the Lead IX column, open Valve V110, check to make sure V112 and LCV-2 are closed and set FCV-1 to 25 percent of desired flow rate. Check the resin depth in the column and make sure flow has been established throughout train number one. Repeat this on train number 2 and then start increasing the flow rate through both trains by adjusting the VFD on the mine water pump and FCV to the desired flow rate.

The IX trains are designed with the capability of bypassing both the lead and tail IX columns. The FCV or LCV (LCV for tail column and FCV for lead column) will maintain a constant level in the IX column by opening and closing depending on observed levels and flow rates. If the LCV or FCV fails and the level increases past the first set point the operator will be notified by the level alarm high (LAH). In the event that the LCV still cannot control the flow, the level will continue to increase to the second set point. At this point, the operators will place the spare IX train in service which will receive flow diverted from the upset IX column. If the spare train is not ready to receive flow, the level alarm high high will sound and the bypass valve will open automatically. This will divert flow from the upset Tail IX column to the overflow storage tank.

C. <u>Resin Transfer</u>

Refer to Drawing 7 - Process Flow Diagram

Refer to Drawing 9 - P&ID - IX Columns (Trains 1 & 2)

Refer to Drawing 10 - P&ID - Resin Storage and Transfer

When the resin in the lead column of an IX train is loaded to about 0.06 pounds/ft³ with uranium, a resin transfer cycle will begin and proceed in the following order.

- 1. The resin will first be transferred from the lead IX column to the loaded-resin storage tanks.
- 2. The partially loaded resin from the tail IX column will then be transferred to the lead IX column.
- 3. Stripped (regenerated) resin will be transferred from the resin tanker to refill the tail IX column.
- 4. Loaded resin will be transferred from a loaded resin storage tank to the resin tanker.

The loaded resin will be removed from the lead IX column(s) (IX-1, 3, 5, 7, 9, 11, 13) by an eductor, where it is fluidized by the resin transfer water and conveyed through a 4" steel pipe at 200 gpm to the loaded resin storage columns. The transfer lines between each IX column have a clear inline sight glass so that the operator can determine when all of the resin has been removed. The inline sight glass will also allow the operator to ensure that the resin is in fact moving out of the IX column. The loaded resin storage columns (T-3A and T-3B) are located in the northeast quadrant of the building and are 8 ft in diameter by 20 ft high. The resin transfer water pump (P-2) will provide water from the resin transfer water storage tanks (T-2A and T-2B) at the necessary flow rate and pressure to fluidize the resin and transport it through the resin transfer cycle.

The partially loaded resin will then be removed from the tail IX column by an eductor and hydraulically transported to the lead IX column. This process will begin immediately after the loaded resin has been removed from the lead IX column.

The regenerated ion exchange resin will be transferred hydraulically from the resin tanker to the tail IX column(s) (IX-2, 4, 6, 8, 10, 12, or 14). This process will begin immediately after the partially loaded resin has been removed from the tail IX column, and transferred to the lead IX column.

The loaded resin will then be transferred from either T-3A or T-3B to the resin tanker. The resin transfer volume from the loaded resin storage tanks to the resin tanker is determined by the level indicator controller. The operator will open the resin tanker compartment hatch and drop the resin transfer hose into the designated receiving compartment. Once this is complete, the resin transfer water pump (P-2) and the resin outlet valve for either of the resin storage tanks will open. The "resin out" valve will close when the level indicator controller reaches a predetermined level change equal to 400 ft³. Excess water drained from the resin tanker during the resin transfer process will be picked up by a sump (SP-1), and pumped through a filter (F-1, F-2, or F-3) prior to being sent back to resin transfer water storage tanks (T-2A or T-2B). The reason for filtering and recycling is to minimize water consumption. The hose connection from the tanker to the resin eductor will have a "no-spill" check valve and a clear sight glass. The purpose of the sight glass will be to provide the operator with a view of the media being transferred, enabling the operator to determine when all of the resin has been transferred. The no-spill check valve will prevent water and/or resin from spilling during connection and disconnection.

D. Instrumentation

1. <u>Mine Water Sump and Pumps</u>

Mine Water Transfer Pumps will have local start-stop switches with a stop only switch located in the control room. In the event of low level in the mine water sump, the level indicator controller (LIC-MW) will adjust the pump speed and activate the level alarm low (LAL-MW) in the control room. Further reduction in level by 12 inches will trip level alarm low low (LALL-MW) and all pumps. The mine water wet well will also be provided with an overflow line to prevent the sump from overtopping. This sump overflow will go directly to the radium removal system.

Mine Water transfer pumps should hold a discharge pressure of at least 10 psi for proper operation of flow control valves at the IX columns.

The 24" diameter mine water header flow will be monitored downstream of the process water take-off. A recorder and low flow alarm will be provided in the control room. The low flow alarm point will be set at 2500 gpm.

2. <u>Lead IX Columns</u>

The control system proposed for the IX facility will display real time activities of tank levels and process flow rates by receiving input from transmitters and indicators throughout the plant. The instrumentation, placement, and function of the controls system is described below.

Flow of mine water to each IX column will be controlled either at the valve or in the control room as described below. Local flow readout will be provided for manual control.

Primary Control

The first magnetic flow meter (mag meter) monitoring each train will be placed on the common header. The mag meter (M-MW) will measure the total flow being delivered to the IX process by the pumps. The mag meter output signal will be transmitted through the flow indicator transmitter (FIT-MW) to the flow recorder (FR-MW) and the flow alarm low (FAL-MW). The FR-MW will record the real time flow and store it digitally for record keeping. The flow alarm low (FAL-MW) will activate or deactivate if the flow is below the pre-determined set point. FAL-MW will be an audible and visible alarm to alert the operator and other personnel of an inadequate flow rate. Downstream of M-MW the flow will enter a common header and be divided into the seven trains.

Each of the seven lead IX columns will be equipped with a mag meter (M-1, 3, 5, 7, 9, 11, 13) located on the supply line to each of the seven trains. The mag meter will be upstream of the flow control valve (FCV-1, 3, 5, 7, 9, 11, 13) and the lead column. The mag meter will measure the flow being delivered to each IX column. The mag meter output signal will be transmitted through the flow indicator transmitter (FIT-1,3, 5, 7, 9, 11, 13) to the flow indicator controller (FIC-1, 3, 5, 7, 9, 11, 13) and flow recorder (FR-1, 3, 5, 7, 9, 11, 13), both of which will be located in the control room. The flow recorder will digitally record data for recordkeeping. The

flow indicator controller will be programmable so that the operator can set it to maintain a desired flow rate. The flow indicator controller will send a signal to a flow control valve which will open and close to maintain the desired flow rate set on the flow indicator controller. The flow indicator controller will also activate or deactivate the flow alarm high (FAH-1, 3, 5, 7, 9, 11, 13). The flow alarm high will be an audible and visible alarm whose set point can be determined and programmed by the operator.

Secondary Control

Each of the seven lead IX columns will be equipped with a sonic level sensor, located in the column tank, which will send its output signal to a level indicator transmitter (LIT-1, 3, 5, 7, 9, 11, 13). The level indicator transmitter will transmit a signal to the level indicator controller (LIC-1, 3, 5, 7, 9, 11, 13). The level indicator controller will be located in the control room and display the water level in each lead column in real time. The level indicator controller will also be programmable to maintain a certain set point level. The purpose of the level indicator controller is to monitor tank levels and to insure that the levels are not high enough to overtop the tanks and cause a spill. The level indicator controller will communicate to the lead column flow control valve (FCV-1, 3, 5, 7, 9, 11, 13), the level alarm high (LAH-1, 3, 5, 7, 9, 11, 13), and the level alarm high high (LAHH-1, 3, 5, 7, 9, 11, 13). In the event that the first level set point has been reached the level indicator controller will activate the level alarm high to notify the operator. The level indicator controller will also adjust the flow control valve appropriately to maintain the programmed set point and prevent a spill. In the event that the level indicator controller is not able to resolve the abnormally high water level by manipulating the flow control valve and the second set point is reached, the level indicator controller will activate the level alarm high high and the operator will be able to manually divert the entire flow around the high level column to the tail IX column. The tail IX columns will have the ability to divert excess flow from the lead IX columns to the overflow storage tank (T-1).

3. <u>Tail IX Columns</u>

Each of the seven tail IX columns will be equipped with a sonic level sensor, located in the column tank, which will send its output signal to a level indicator transmitter (LIT-2, 4, 6, 8, 10, 12, 14). The level indicator transmitter will transmit a signal to the level indicator controller (LIC-2, 4, 6, 8, 10, 12, 14). The level indicator controller will be located in the control room and display the water level in each tail column in real time. The level indicator controller will also be programmable to maintain a certain set point level. The purpose of the level indicator controller is to monitor tank levels and to insure that the levels are not high enough to overtop the tanks and cause a spill. The level indicator controller will communicate to the tail column level control valve (LCV-2, 4, 6, 8, 10,

12, 14), the level alarm high (LAH-2, 4, 6, 8, 10, 12, 14), and the level alarm high high (LAHH-2, 4, 6, 8, 10, 12, 14). In the event that the first level set point has been reached the level indicator controller will activate the level alarm high to notify the operator, the level indicator controller will also adjust the level control valve appropriately to maintain the programmed set point and prevent a spill. In the event that the level indicator controller is not able to resolve the abnormally high water level by manipulating the level control valve and the second set point is reached, the level indicator controller will activate the level alarm high high is activated the level control valve will be closed 100% and all flow to the tail IX column will be diverted to the overflow storage tank (T-1).

E. <u>Quality Control of Discharge Fluids</u>

- 1. <u>Sampling of Discharge Fluids</u>
 - a. Composite sampling will be performed for all IX Tail columns, total discharge stream of the IX system and the total discharge stream leaving the facility.
 - b. This composite sampling will be on an eight (8) hour schedule and will incorporate a duplicate sample bottle for third party assay.
 - c. The operator will grab samples every eight (8) hours from each lead and tail IX column to determine when resin transfer must occur to keep the system discharge stream below the 30 ppb standard for uranium.
- 2. <u>Test Method</u>
 - a. The test method for uranium will follow the ASTM D5174 Standard. This test method for trace uranium in water uses Pulsed-Laser Phosphorimetery analyzed by a KPA (Kinetic Phosphorescence Analyzer). This analyzer achieves highly specific analysis for uranium down to 0.01 μ g/L with an analytical range of over 500,000 μ g/L.
 - b. The third party assay laboratory will be a NELAC-certified laboratory that will use a KPA system or other method(s) with detection capabilities sufficient to reliably detect down to $0.01 \mu g/L$.

APPENDIX A



DOWEX 21K 16/20

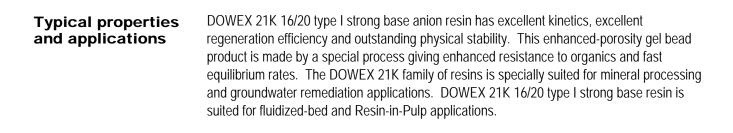
A High Efficiency, Large Bead, Strong Base Anion Exchange Resin for Mineral Processing Applications

Product	Туре	Matrix	Functional group
DOWEX* 21K 16/20	Type I strong base anion	Styrene-DVB, gel	Quaternary amine

Guaranteed Sales Specifications		CI-form	
Total exchange capacity, min.	eq/L	1.2	
Bead size distribution			
Thru 20 mesh, max.	%	10	
Thru 25 mesh, max.	%	2	

Typical Physical and Chemical Properties		Cl [.] form	
Water content	%	50 - 58	
Whole uncracked beads	%	90 - 100	
Total swelling (CI ⁻ \Rightarrow OH ⁻)	%	20	
Particle density	g/mL	1.08	
Shipping weight	g/L	690	
	lbs/ft ³	43	

Recommended Operating Conditions	 Maximum operating temperature: OH⁻ form Cl⁻ form 	60°C (140°F) 100°C (212°F)
	• pH range	0 - 14
	Bed depth, min.	800 mm (2.6 ft)
	 Flow rates: Service/fast rinse Backwash Co-current regeneration/displacement rinse 	5 - 50 m/h (2 - 20 gpm/ft²) See figure 1 1 - 10 m/h (0.4 - 4 gpm/ft²)
	Total rinse requirement	3 - 6 Bed volumes
	 Regenerant: Type Temperature 	NaCl/Carbonate Ambient or up to 50°C (122°F) for silica removal
	Organic loading, max.	3g KMnO₄/I resin



Packaging

5 cubic foot fiber drums

Figure 1. Pressure Drop vs. Flow Rate

For DOWEX 21K Resins, CI, 77 deg. F

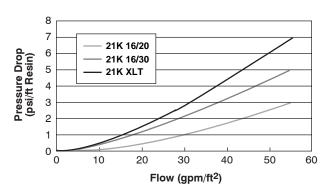
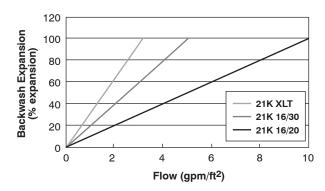


Figure 2. Backwash Expansion vs. Flow Rate

For DOWEX 21K Resins, CI, 77 deg. F



DOWEX Ion Exchange Resins For more information about DOWEX resins, call the Dow Liquid Separations business:

business.		
North America:	1-800-447-4369	
Latin America:	(+55) 11-5188-9222	
Europe:	(+32) 3-450-2240	
Pacific:	+60 3 7958 3392	
Japan:	+813 5460 2100	
China:	+86 21 2301 9000	
http://www.dowex.com		

Warning: Oxidizing agents such as nitric acid attack organic ion exchange resins under certain conditions. This could lead to anything from slight resin degradation to a violent exothermic reaction (explosion). Before using strong oxidizing agents, consult sources knowledgeable in handling such materials.

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