

Copper Flat Project



Impoundment
Design Report

Prepared For:



Certified Professional Engineer Seal

This report documents work conducted under the oversight of the following Engineer:

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Exp. 12/31/2017

Date 14/2/2019

IMPOUNDMENT DESIGN REPORT COPPER FLAT PROJECT

TABLE OF CONTENTS

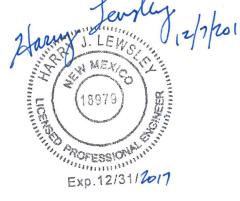
SECTIO	N	<u> </u>	PAGE
TABLE (OF CONT	TENTS	I
LIST OF	TABLES	S	[]
LIST OF	FIGURE	S	II
1		OUCTION	
2		/I DESCRIPTIONS	
3	BASIS C	DF DESIGN	
	3.1	GENERAL	
	3.2	IMPACTED STORMWATER IMPOUNDMENTS	
	3.3	PROCESS WATER RESERVOIR	3
4		AND CONSTRUCTION OF IMPACTED STORMWATER IMPOUNDMENTS AND PROCESS RESERVOIR	
	4.1	FACILITIES	
	4.2	SURFACE WATER CONTROL	5
	4.3	GEOLOGIC HAZARDS	5
	4.4	SOLUTION CHARACTERIZATION	5
	4.5	CAPACITY AND STORAGE DESIGN	
	4.6	SPILLWAY DESIGN	5
	4.7	SITE PREPARATION	6
	4.8	LINER SYSTEMS	
	4.9	LEAK COLLECTION SYSTEM	
	4.10	PERFORMANCE INSPECTIONS AND OPERATIONAL MONITORING	7





LIST OF TABLES

TABLE	DESCRIPTION	Tables follows text
Table 1	Impoundment Design Criteria	
	LIST OF FIGURES	
FIGURE	DESCRIPTION	Figures follow Tables
Figure 1	Site Location Plan	
Figure 2	Proposed Site Plan	
Figure 3	Developed Watershed Areas	
Figure 4	Stormwater and Process Water Ponds Overall Plan	
Figure 5	Process Area Site Plan	
Figure 6	Impacted Stormwater Impoundment A Plan View	
Figure 7	Impacted Stormwater Impoundment A Sections	
Figure 8	Impacted Stormwater Impoundment B Plan View	
Figure 9	Impacted Stormwater Impoundment B Sections	
Figure 10	Impacted Stormwater Impoundment C Plan View	
Figure 11	Impacted Stormwater Impoundment C Sections	
Figure 12	Process Water Reservoir Plan View	
Figure 13	Process Water Reservoir Plan Sections	
Figure 14	Standard Details Sheet 3	



1 INTRODUCTION

The Copper Flat Project is located in South Central New Mexico, near the town of Hillsboro, approximately 150 miles south of Albuquerque, and approximately 20 miles southwest of Truth or Consequences (straight-line distances) (Figure 1). The Project is owned and operated by New Mexico Copper Corporation (NMCC), a wholly owned subsidiary of THEMAC Resources Group Limited.

The State of New Mexico has promulgated regulations pertaining to groundwater protection at copper mining facilities (New Mexico Administrative Code Title 20, Chapter 6, Part 7 [20.6.7 NMAC], the "Copper Rule"), the stated purpose of which is "to control discharges of water contaminants specific to copper mine facilities and their operations to prevent water pollution."

This report provides the design criteria, location, purpose, operation, and performance of certain elements of the project identified in Section 2 of this report to comply with 20.6.7 NMAC. This report excludes the design considerations for the Tailings Storage Facility (TSF), i.e., the tailings impoundment, underdrain collection pond, surge pond and the secondary containment trench from the processing facility to the TSF, which have been completed by others and are reported separately.



1

2 SYSTEM DESCRIPTIONS

Impacted Stormwater Impoundments are designed to receive surface drainage that potentially has come in contact with water contaminants on a copper mine facility. These systems consist of a network of diversion channels designed to convey to the impoundment at minimum the peak from a 100-year-return-interval storm with at least 6 inches of freeboard per 20.6.7.17.D.(2).(f). The Impacted Stormwater Impoundments are designed to store impacted stormwater for less than 30 days and include an engineered liner system, as described in Section 3.2.

The Process Water Reservoir is designed to receive reclaimed process water from a variety of sources including the TSF, impacted stormwater impoundments and freshwater supply system conveyed via pipelines. The reservoir also receives direct precipitation to the pond surface and embankment crest area. The Process Water Reservoir is designed with an engineered liner system, leak collection system, and subgrade bedding, as described in Section 3.3.



3 BASIS OF DESIGN

3.1 GENERAL

All impoundments for the Copper Flat Project will be considered "new" impoundments as defined by NMAC 20.6.7.17 (D).

Outside Slopes	20.6.7.17.D.(1).(a) NMAC	Maximum 2:1 (H:V)
Static factor of safety	20.6.7.17.D.(1).(a) NMAC	Minimum 1.3
Liner Sidewall seams	20.6.7.17.D.(1).(e) NMAC	Vertical only
Capacity	20.6.7.17.D.(2) NMAC	Contain 100-year return interval storm event plus minimum 2 ft of freeboard

3.2 IMPACTED STORMWATER IMPOUNDMENTS

Impacted stormwater impoundments are designed to hold impacted stormwater for less than 30 days in accordance with NMAC 20.6.7.17 (D) (4) and (7).

Liner system	20.6.7.17.D.(4).(a) NMAC	Compacted minimum 6-inch subbase overlain by 60 mil HDPE liner system
Wind protection	20.6.7.17.D.(4).(d) NMAC	Weighting system to limit liner damage in high winds
Spillway design	20.6.7.17.D.(7) NMAC	Safely discharge peak flow from 24-hour storm event with 25-year return

3.3 PROCESS WATER RESERVOIR

Process Water Impoundments/Reservoirs are designed to hold process water at design capacity plus impacted stormwater for more than 30 days in accordance with NMAC 20.6.7.17 (D) (3).

Liner system	20.6.7.17.D.(3).(a)and 20.6.7.17.D.(3). (c) NMAC	Primary 60 mil HDPE liner over a secondary 60 mil HDPE liner with drainage layer over a compacted minimum 6-inch subbase
Leakage collection system	20.6.7.17.D.(3).(d) NMAC	Drainage layer between primary and secondary liners with fluid removal system
Drainage layer	20.6.7.17.D.(3).(d) NMAC	Granular soil material or geosynthetic drainage net
Drainage layer slope	20.6.7.17.D.(3).(d) NMAC	At least 2 percent
Drainage layer permeability	20.6.7.17.D.(3).(d) NMAC	At least 1 x 10 ⁻² centimeters per second (cm/s)
Collection sump	20.6.7.17.D.(3).(d) NMAC	At confluence drainage layer with dedicated automatic pump system with totalizing flow meter and automated failure alarm system
Spillway design	20.6.7.17.D.(7) NMAC	No discharge to ground surface, safely discharge peak process flows



4 DESIGN AND CONSTRUCTION OF IMPACTED STORMWATER IMPOUNDMENTS AND PROCESS WATER RESERVOIR

The Copper Flat Project permit boundary (Figure 2) incorporates the mine pit, processing plant area, waste rock stockpiles (WRSPs), and the TSF. The TSF and related facilities including the cyclone plant, surge pond, and underdrain collection pond are described by others. The mine and process plant area includes five developed watershed (WS) areas (Figure 3) that are managed as part of this plan. The facilities described below are designed to manage process and impacted stormwater to prevent releases from the site to surface water and groundwater (Figure 4).

4.1 FACILITIES

WS A includes the process plant, maintenance, and administrative areas of the Copper Flat Project. It also includes WS E, which is the Process Water Reservoir as a separate, internal area of stormwater and process water management (Sec. 4.1.5). During precipitation events, sheet flow of stormwater is directed (Figure 5) to open channel conveyances designed to convey the peak flow from a 100-year return interval storm event with at least 6 inches of freeboard to Impacted Stormwater Impoundment A (Figures 6 and 7). The impoundment is designed with a spillway that is capable of safely discharging the peak flow from a 25-year, 24-hour precipitation event with a 90 percent chance of not being exceeded during the design life of the impoundment. Design criteria for Impacted Stormwater Impoundment A are presented in Table 1.

WS B includes runoff from the western flank of Animas Peak and proposed new waste rock stockpiles (WRSP-1) (Figure 3). During precipitation events, sheet flow of stormwater is directed (Figure 3) to open channel conveyances designed to convey the peak flow from a 100-year return interval storm event with at least 6 inches of freeboard to Impacted Stormwater Impoundment B (Figures 8 and 9). The impoundment is designed with a spillway to the mine pit that is capable of safely discharging the peak flow from a 25-year, 24-hour precipitation event with a 90 percent chance of not being exceeded during the design life of the impoundment. Design criteria for Impacted Stormwater Impoundment B are presented in Table 1.

WS C includes runoff from the eastern flank of Animas Peak and proposed new waste rock stockpiles (WRSP-2 and 3) (Figure 3). During precipitation events, sheet flow of stormwater is directed (Figure 3) to open channel conveyances designed to convey the peak flow from a 100-year return interval storm event with at least 6 inches of freeboard to Impacted Stormwater Impoundment C (Figures 10 and 11). The impoundment is designed with a spillway that is capable of safely discharging the peak flow from a 25-year, 24-hour precipitation event with a 90 percent chance of not being exceeded during the design life of the impoundment. Design criteria for Impacted Stormwater Impoundment C are presented in Table 1.

WS D includes runoff from uphill slopes and existing waste rock stockpiles (EWRSP-1 and -2b) to the mine pit (Figure 3). During precipitation events, sheet flow of stormwater is directed by natural drainage channels and open channel conveyances designed to convey the peak flow from a 100-year return interval storm event with at least 6 inches of freeboard to the mine pit.

WS E consists of direct precipitation onto the lined surfaces of the Process Water Reservoir and unlined perimeter road that is directed to the reservoir (Figure 3). The amount of direct precipitation to the pond is small (9.5 cubic feet per second [cfs]) in comparison to the design throughput of process solutions through the pond (100,000 cfs). The design freeboard of 2 ft is more than adequate to handle the additional flux from a precipitation event. The design capacity of the pond is 726,400 cubic feet (ft³) with 2 ft of freeboard and the ultimate capacity is 938,000 ft³ (Figures 12 and 13). Overtopping of the reservoir is controlled by an alarm system and emergency shutoff system. Overtopping flows, in the event of system failure, are directed to the lined tailings conveyance trench to the lined tailings impoundment. Design criteria for the Process Water Reservoir are presented in Table 1.



4.2 SURFACE WATER CONTROL

Surface areas draining to the Impacted Stormwater Impoundments (A, B, and C), mine pit, and Process Water Reservoir will be shielded from run-on surface drainage by site diversions as described in a separate report.

4.3 GEOLOGIC HAZARDS

No geologic hazards are known to exist in the vicinities of the Impacted Stormwater Impoundments or Process Water Reservoir. Impacted Stormwater Impoundment B is located on the eastern wall of the ultimate mine pit (Figure 11J-3). In the event of a pit slope failure, any liquids contained in Impacted Stormwater Impoundment B would be contained in the mine pit.

4.4 SOLUTION CHARACTERIZATION

Liquids routinely expected to enter the Impacted Stormwater Impoundments (A, B, and C) are direct precipitation and stormwater runoff from areas impacted by mining activities including mining, hauling, waste rock stockpiling, mineral processing, and shipping and receiving of goods and products. The Impacted Stormwater Impoundments will be typically empty. Impacted stormwater collected in the impoundments will be pumped out and used as process makeup water.

Liquids routinely expected to enter the Process Water Reservoir include direct precipitation, water reclaimed from the Copper-Moly (Cu-Mo) Thickener, fresh make-up water from the water supply wellfield, and reclaimed water from the Tailings Impoundment and Underdrain Collection Pond. The Process Water Reservoir is typically maintained at a nearly full operational level at all times to ensure continuity of the process during short-term interruptions of return or makeup flows. The physical characteristics of these constituents are expected to be neutral to slightly alkaline and completely compatible with the liner materials. Flows from upset conditions in the concentrator do not flow directly to the Process Water Reservoir, but would eventually contribute to the water reclaimed from the Tailings Impoundment and Underdrain Collection Pond.

4.5 CAPACITY AND STORAGE DESIGN

The capacity and storage design of the subject impoundments and reservoir are provided in Table 1. The impacted water impoundments are designed to contain the runoff from a 100-year, 24-hour storm event with a minimum of 2 ft of freeboard.

The Process Water Reservoir is designed to contain the maximum design process flow plus stormwater runoff from the reservoir catchment area with a minimum of 2 ft of freeboard.

4.6 SPILLWAY DESIGN

Spillways for Impacted Stormwater Impoundments A, B, and C are designed to safely discharge the peak runoff of a 25-year, 24-hour precipitation event. The spillways for Impacted Stormwater Impoundments A and C are designed as open channel spillways with slopes that are suitable for vehicle access on the perimeter road. The spillway for Impacted Stormwater Impoundment B is designed as a culvert beneath the haul road. The culvert(s) will have sufficient capacity to safely pass peak runoff from the prescribed precipitation event.

Overflow protection for the process water reservoir is accomplished via a designed solution conveyance to the lined tailings conveyance trench, which conveys any upset flows that exceed the maximum capacity without compromising the integrity of the structure.



4.7 SITE PREPARATION

The pond areas will be cleared and grubbed of vegetation. Any unsuitable foundation materials within the pond footprint will be excavated and replaced. Bedding soil will be placed, moisture conditioned, and compacted pursuant to 20.6.7.17.D.(3) and (4). The bedding soil must be free of sharp rock, vegetation, and stubble to a depth of at least 6 inches. The bedding surface must be smooth to ensure good contact between the liner and the bedding. The liner must be placed on a layer of sand or fine soil. The floor of the bedding surface will be sloped to collection sump at grades of up to 1 percent to facilitate removal of the contents. Side slopes will be less than 2H:1V to permit proper installation of the liner system. The liner bedding shall have an acceptance certificate prior to installation of the liner.

4.8 LINER SYSTEMS

Pursuant to 20.6.7.17.D.(4), the liner system of the Impacted Stormwater Impoundments consists of a single 60 mil HDPE textured geomembrane liner that is certified as UV resistant in accordance with a Construction Quality Assurance and Construction Quality Control (CQA/CQC) Plan, which will be generated and approved prior to construction. Liner panels shall be oriented such that the seams on the sidewall of the impoundments are vertical. Sufficient slack in the liner will be maintained to accommodate expansion and contraction of the liner material due to changes in temperature. These impoundments are typically empty and the liner will be weighted to prevent wind damage. The liner shall be secured in an anchor trench (Figure 14, Detail 3).

Pursuant to 20.6.7.17.D. (3), the liner system for the Process Water Reservoir consists of a secondary liner, drainage layer, and primary liner. The drainage layer connects directly to the fluid collection sump and fluid removal system to alleviate the need for fluid collection pipes. This reservoir typically contains solution and will not require the liner to be weighted unless there is a prolonged period when the reservoir will be empty and susceptible to wind damage. The liner system shall be secured in an anchor trench (Figure 14, Detail 1).

The lower (secondary) liner consists of a single 60 mil HDPE geomembrane AGRU® drainage liner, or equivalent, that is installed in accordance with an approved CQA/CQC Plan. This type of secondary liner, paired with a primary liner, doubles as a drainage layer with a coefficient of permeability of 1 x 10-2 cm/s on a design slope of 2 percent. Liner panels shall be oriented such that the seams on the sidewall of the impoundments are vertical. Sufficient slack in the liner will be maintained to accommodate expansion and contraction of the liner material due to changes in temperature.

The primary liner for the Process Water Reservoir consists of a single 60 mil HDPE textured geomembrane liner that is certified as UV resistant and installed in accordance with an approved CQA/CQC Plan. Liner panels shall be oriented such that the seams on the sidewall of the impoundments are vertical. Sufficient slack in the liner will be maintained to accommodate expansion and contraction of the liner material due to changes in temperature.

A CQA/CQC plan will be developed by the design engineer and the liner installation contractor and for approval by the appropriate agency as part of the final design prior to construction. The plan includes the following elements.

- Identification of persons and entities responsible for overseeing the program.
- Inspection protocols for subgrade, materials, placement, anchoring, welding, testing, and repairing.
- Identification of field and laboratory testing equipment and testing entities.
- Procedures for observing and testing liner, subgrade, bedding, etc.
- Verification protocol for manufacturer's QC testing.
- Procedures for reviewing results of testing and inspection.
- Corrective actions for material repair, subgrade and bedding deficiencies, weld testing failures, or other construction defects.
- Seaming procedures, qualification, testing, and inspection.
- QA/QC reporting procedures, schedules, and certifications.



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Guidelines, schedules, contents, and certifications for submission of a CQA/CQC report.

4.9 LEAK COLLECTION SYSTEM

Pursuant to 20.6.7.17.D.(3).(d), the liner drainage layer of the process water reservoir discharges directly into a leakage collection sump (Figure 14, Detail 6) which is part of the fluid removal system. The sump contains granular fill materials to convey the drainage fluid to the fluid removal pipe and pump system. The fluid removal pipe consists of a 6" Sch. 80 polyvinyl chloride (PVC) pipe with 3 ft of slotted screen at the bottom for water collection. The fluid removal pipe can be cleaned using conventional pipe cleaning equipment. An automated fluid removal pump is installed at the bottom of the pipe to enable removal of leakage. The pump is activated in the presence of drainage fluid in the sump and is turned off when the fluid has been removed. A totalizing flow meter records the volume of fluid removed from the sump. The pump also has an alarm system to notify the operator of system failure.

4.10 Performance Inspections and Operational Monitoring

Routine inspections of the Process Water Reservoir and Impacted Stormwater Impoundments begin at the time of construction and proceed quarterly. Additional inspections are prescribed in the event of a process upset or a significant stormwater flow event. Inspections include visual assessment of integrity and physical assessment of pond capacity. Water levels in the ponds are noted with respect to the freeboard. Totalizing meter readings are recorded from fluid removal pumps from the leakage collection sump and from the impacted stormwater impoundment pumps.



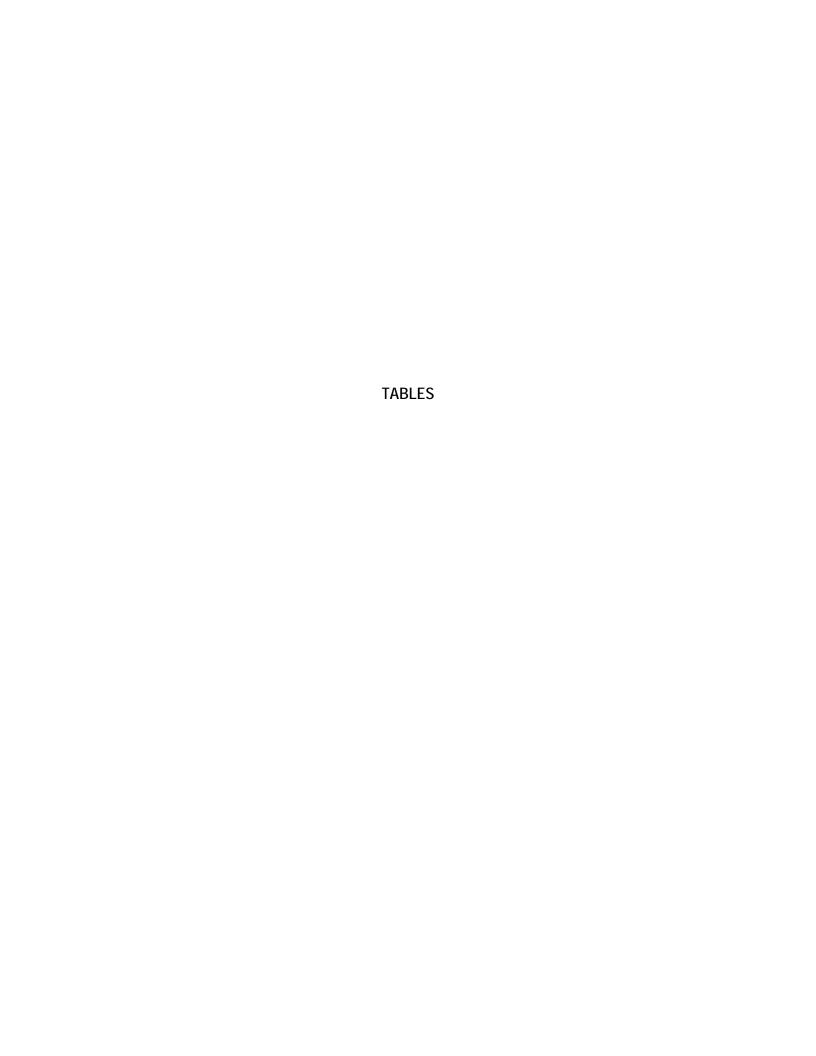


Table 1: Impoundment Design Criteria

Impoundment ID	Stormwater Impoundment A	Stormwater Impoundment B	Stormwater Impoundment C	Process Water Reservoir
Catchment Area (ac)	91.06	98.52	198.66	1.80
Peak Flow, Q100 (cfs) ¹	200.25	176.88	315.76	9.54
Pond Size - Approx, Surface area (ac)	1.98	2.12	6.37	1.80
Freeboard Requirement (ft)	2.0	2.0	2.0	2.0
Capacity at Freeboard (ft ³)	976,800	748,400	1,405,500	726,400
Design Capacity at spillway/crest (ft ³)	1,280,500	913,200	1,802,100	938,000
Primary Liner Specifications ²	60 mil HDPE or equivalent 6" fine soil subgrade Certified UV resistant	60 mil HDPE or equivalent 6" fine soil subgrade Certified UV resistant	60 mil HDPE or equivalent 6" fine soil subgrade Certified UV resistant	60 mil HDPE or equivalent Certified UV resistant
Secondary Liner Specifications ²	N/A	N/A	N/A	60 mil HDPE or equivalent 6" fine soil subgrade
Drainage Layer Specifications ³	N/A	N/A	N/A	Geonet drainage layer Slope min. 2% Perm. min. 1 x 10-2 cm/s
Perforated Fluid Collection System ⁴	N/A	N/A	N/A	Geonet drainage layer
Fluid Removal System ²	N/A	N/A	N/A	Automatic pump Totalizing flow meter Automated failure alarm
Design Flow for Conveyance Structures (cfs)	Q100 = 200.25	Q100 = 176.88	Q100 = 315.76	Q100 = 9.54
Design Storm for Pond & Source	100-yr, 24hr rainfall event, WS A	100-yr, 24hr rainfall event, WS B	100-yr, 24hr rainfall event, WS C	100-yr, 24hr rainfall event, WS E
Design Storm for Spillway & Source	200-yr, 24hr rainfall event, WS A	200-yr, 24hr rainfall event, WS B	200-yr, 24hr rainfall event, WS C	N/A
Peak Flow, Q200 for Spillway (cfs) ⁵	6.16	6.37	8.80	N/A
Bank Slopes	2:1 (H:V) Max	2:1 (H:V) Max	2:1 (H:V) Max	2:1 (H:V) Max

 $^{^{\}rm 1}$ Precipitation data is per NOAA Atlas 14, Volume 1, Version 5; Hillsboro, NM, Station ID: 29-4009

² Specifications are per 20.6.7.17.D.(3) and (4)(c)

³ Specifications are per 20.6.7.17.D.(3)(d)

⁴ Geonet layer drains directly into collection sump and fluid removal system

⁵ Design Flow for spillway is approximate flow from pond to spillway during the 200-yr event assuming the spillway elevation is at the 100-yr WSEL





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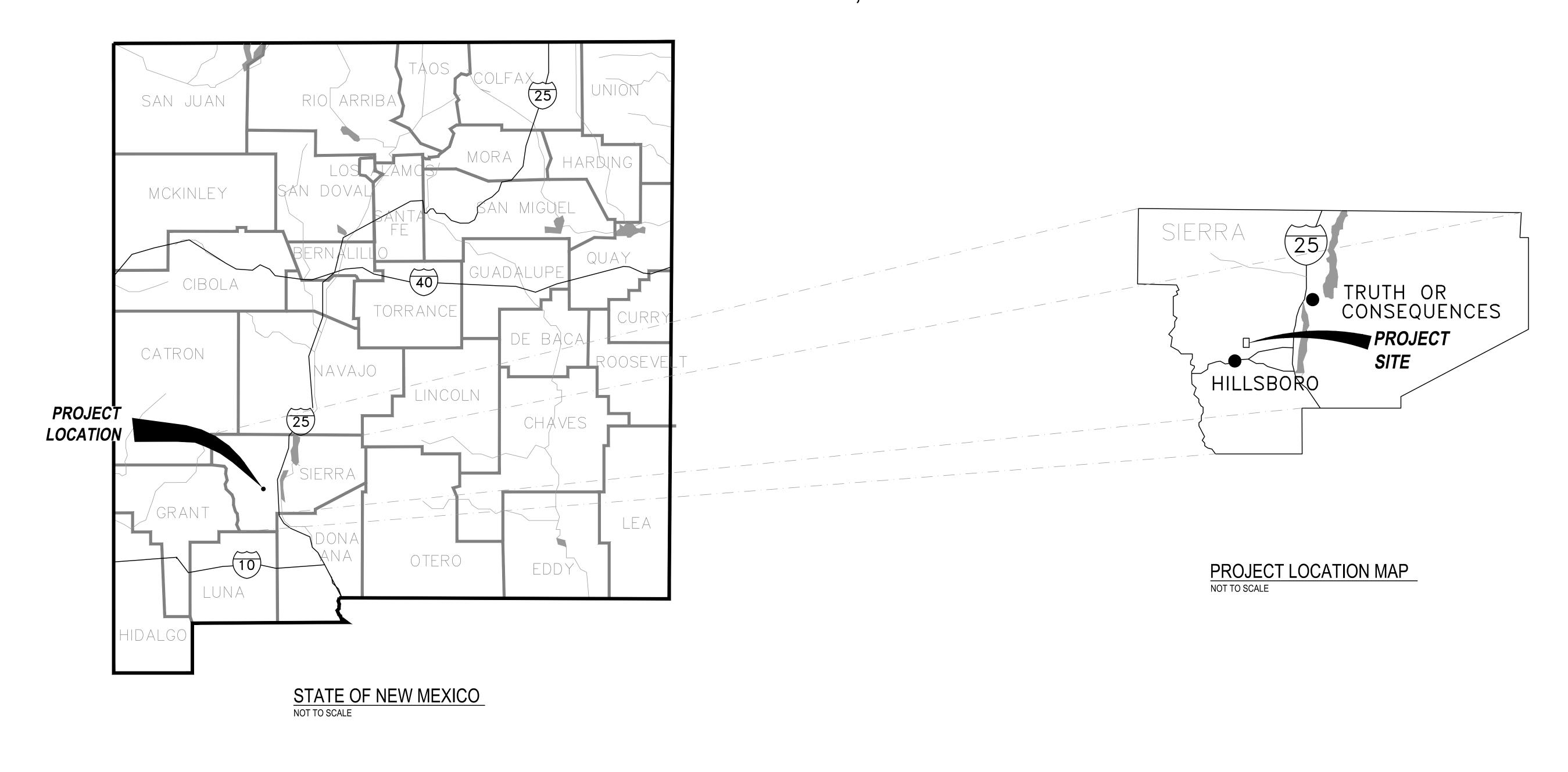


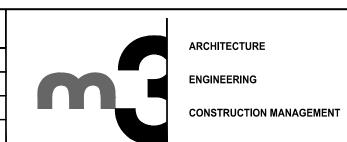
FIGURE 1

PRELIMINARY FOR AGENCY REVIEW

DO NOT SCALE 11x17 DRAWINGS

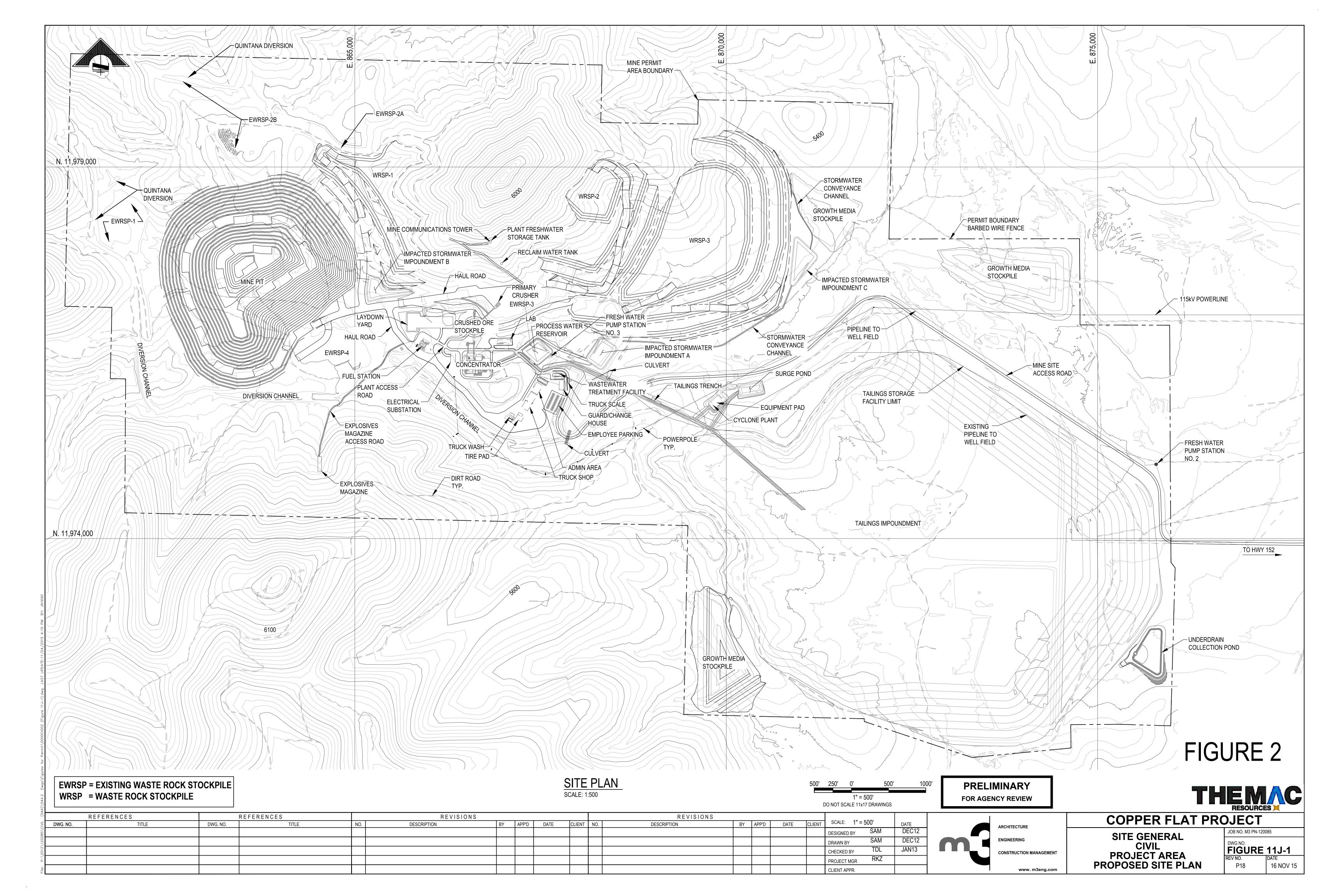


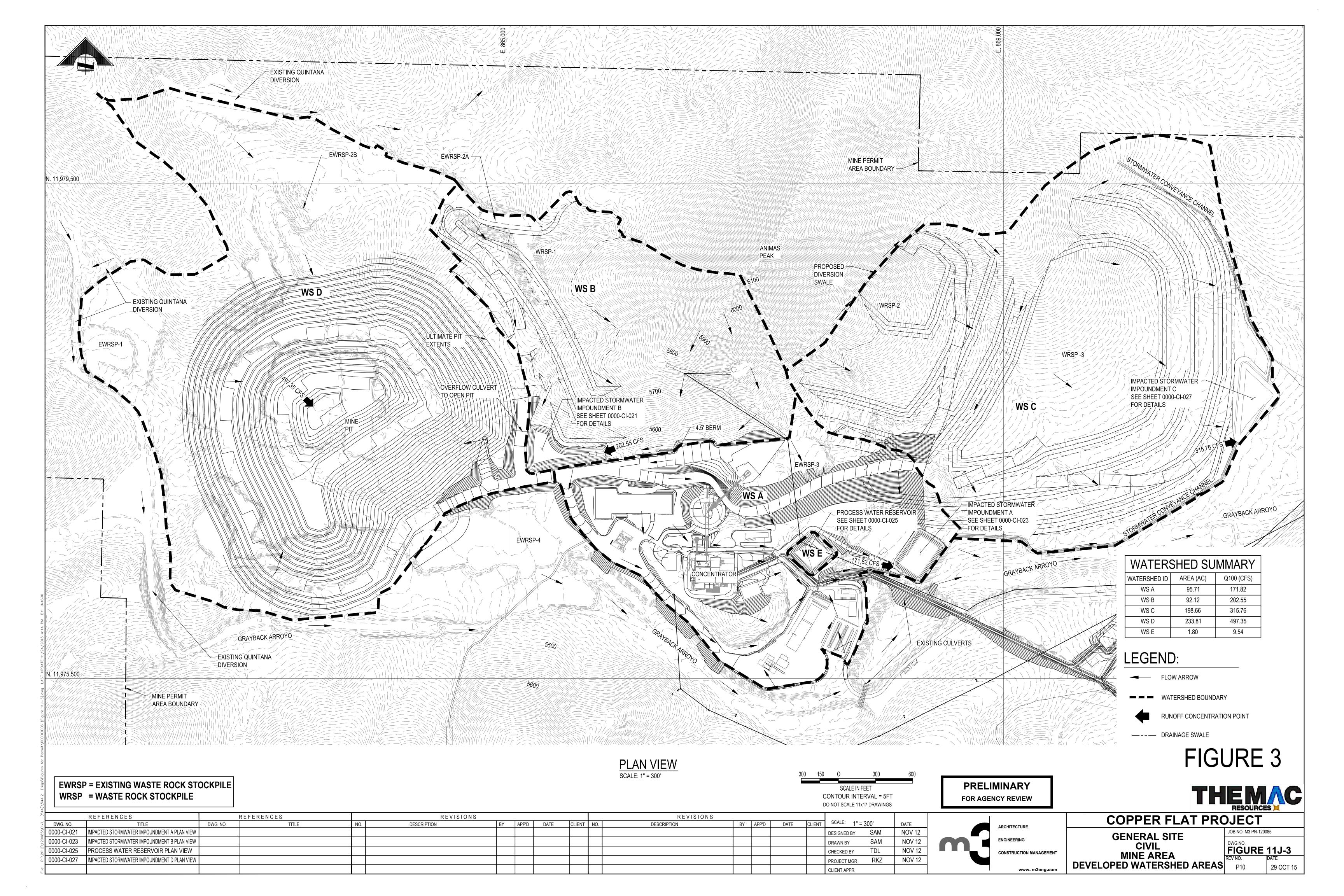
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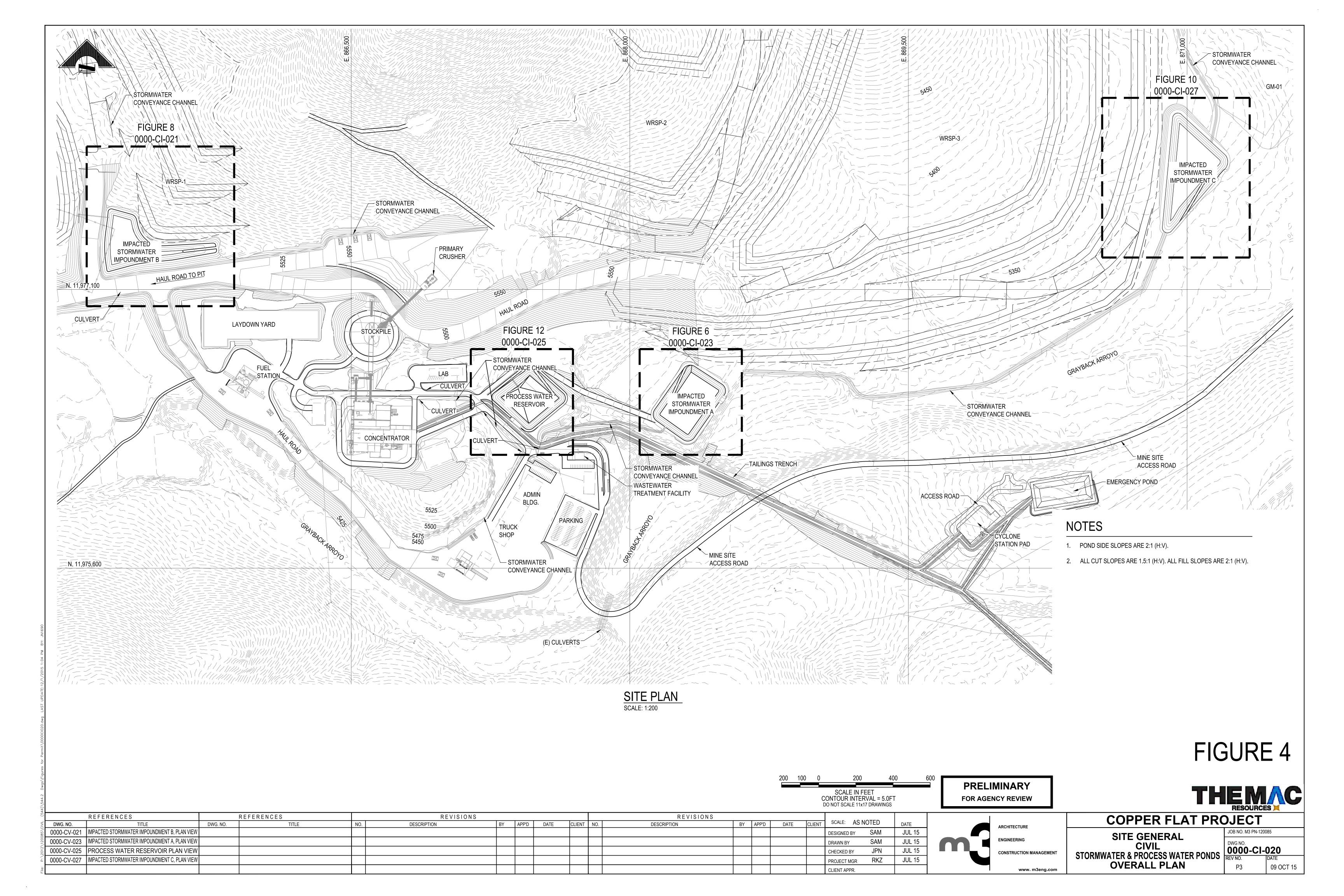


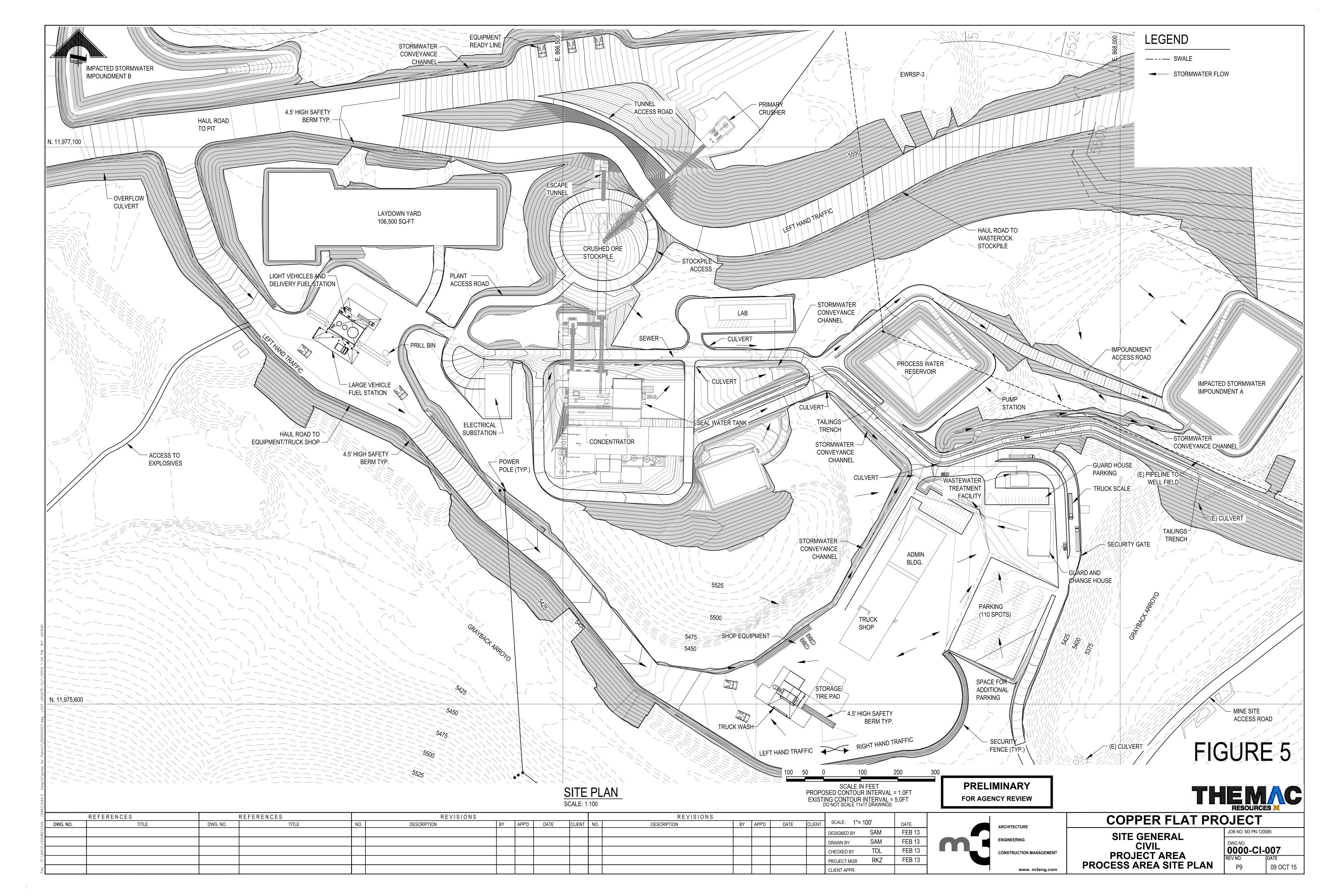
COPPER FLAT PROJECT SITE GENERAL CIVIL PROJECT AREA SITE LOCATION PLAN

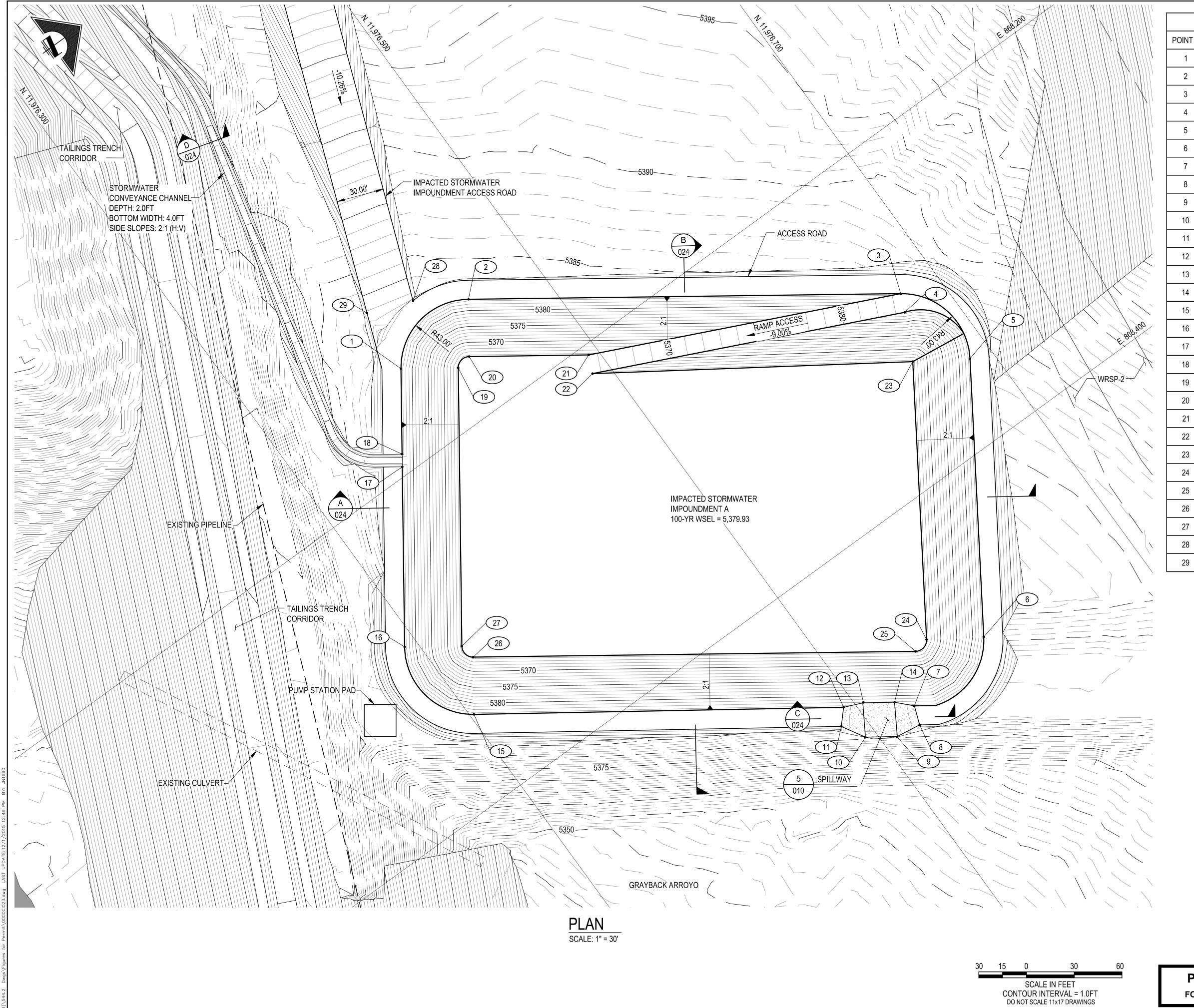
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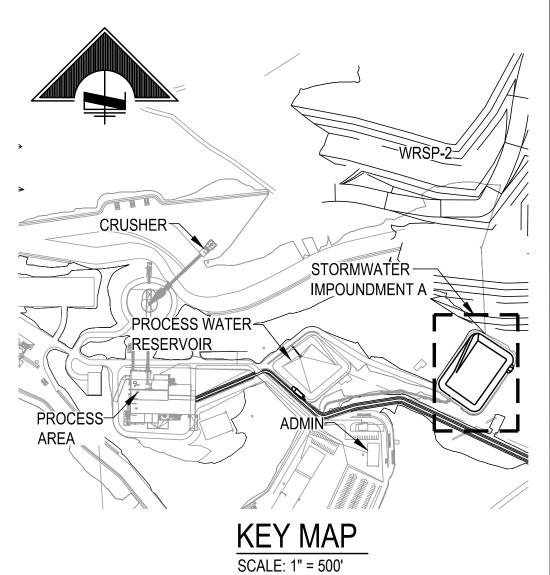








POINT TABLE												
POINT#	NORTHING	EASTING	ELEVATION									
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2	11976453.06	868133.72	5383.50									
3	11976675.02	868290.57	5383.50									
4	11976670.08	868301.51	5383.50									
5	11976686.19	868349.21	5383.50									
6	11976590.39	868495.80	5383.50									
7	11976529.56	868505.28	5383.50									
8	11976525.25	868516.90	5383.50									
9	11976509.58	868514.53	5381.96									
10	11976493.13	868503.16	5381.96									
11	11976484.86	868488.73	5383.50									
12	11976493.10	868479.86	5383.50									
13	11976504.45	868484.69	5382.18									
14	11976520.85	868496.13	5382.18									
15	11976302.43	868346.86	5383.50									
16	11976292.13	868286.93	5383.50									
17	11976357.47	868194.48	5383.50									
18	11976362.08	868187.95	5383.50									
19	11976422.53	868164.79	5365.50									
20	11976432.28	868163.12	5365.50									
21	11976493.65	868206.42	5365.50									
22	11976488.60	868217.31	5365.50									
23	11976656.01	868329.59	5365.50									
24	11976560.26	868476.10	5365.50									
25	11976550.36	868477.99	5365.50									
26	11976323.21	868317.47	5365.50									
27	11976321.53	868307.71	5365.50									
28	11976424.35	868113.97	5383.50									
29	11976396.34	868103.21	5383.50									



NOTES:

- 1. STORMWATER IMPOUNDMENT A IS INTENDED TO CAPTURE STORMWATER RUNOFF FROM THE MINE SITE PROCESS AREA.
- 2. STORMWATER IMPOUNDMENT IS SIZED TO CONTAIN THE 100-YR, 24-HR RAINFALL EVENT WITH A MINIMUM OF 2.0 FEET OF FREEBOARD.
- 3. STORMWATER IMPOUNDMENT SHALL BE SINGLE LINED WITH 60MIL HDPE LINER, PER DETAIL 4 ON SHEET 0000-CI-010, OR APPROVED EQUAL.
- 4. STORMWATER SPILLWAY IS DESIGNED FOR THE 25-YR, 24-HR RAINFALL EVENT AT MINIMUM.
- 5. SPILLWAY IS DESIGNED TO ALLOW FOR VEHICULAR TRAFFIC.

IMPOUNDMENT SUMMARY									
CAPACITY AT 100-YR WSEL	976,772	CU-FT							
ULTIMATE CAPACITY	1,280,516	CU-FT							

FIGURE 6

PRELIMINARY FOR AGENCY REVIEW



44																		
9		REFERENCES		REFERENCES		REVISIONS						REVISIONS						
] 	DWG. NO.	TITLE	DWG. NO.	TITLE	NO.	DESCRIPTION	BY	APP'D	DATE	CLIENT	NO.	DESCRIPTION B	3Y <i>f</i>	APP'D	DATE	CLIENT SCALE: AS NOT	ED	DATE
)85/0	0000-CI-024	IMPACTED STORMWATER IMPOUNDMENT A, SECTIONS														DESIGNED BY	SAM	JUN 15
\1200	0000-CI-010	STANDARD DETAILS SHEET 3														DRAWN BY	SAM	JUN 15
2012																CHECKED BY	JPN	AUG 15
ġ.																PROJECT MGR F	RKZ	AUG 15
ë															_	CLIENT APPR.		



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GENERAL SITE

RESOURCES

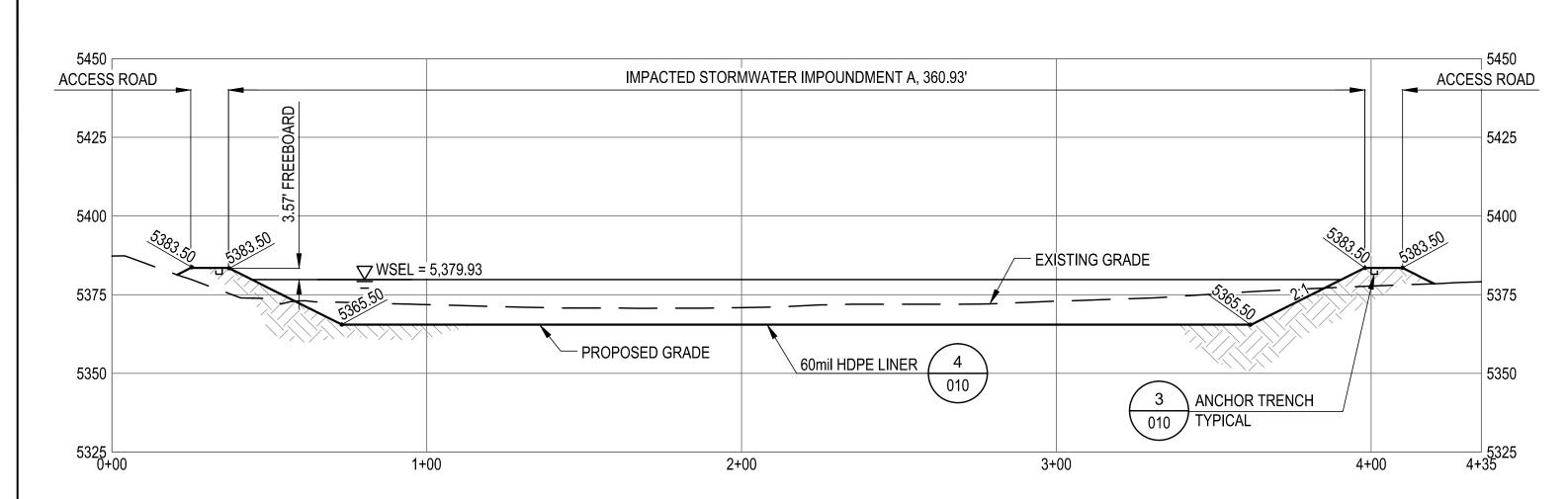
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GENERAL SITE
CIVIL
IMPACTED STORMWATER IMPOUNDMENT A
PLAN VIEW

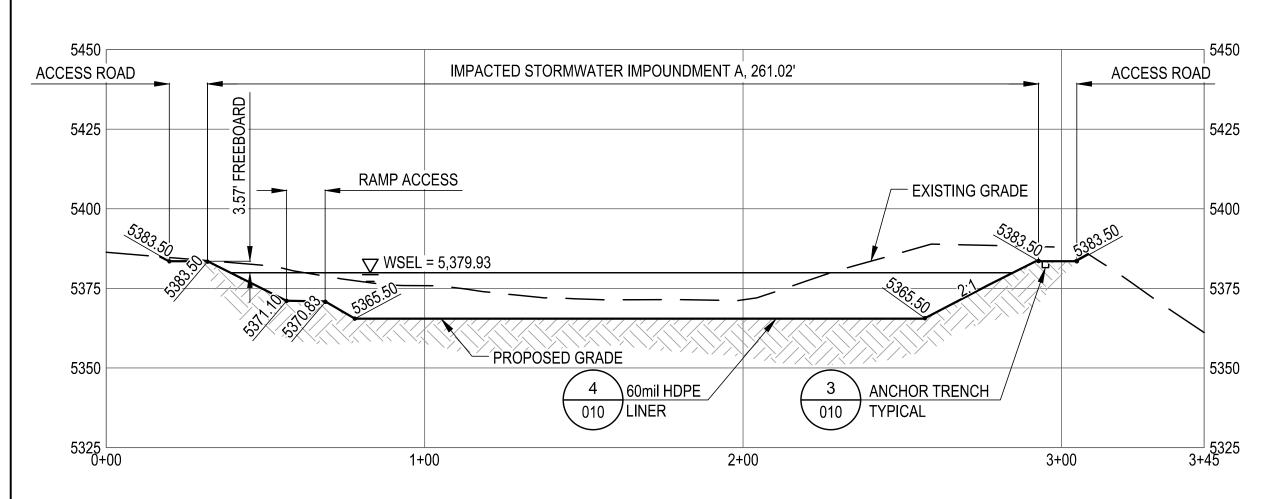
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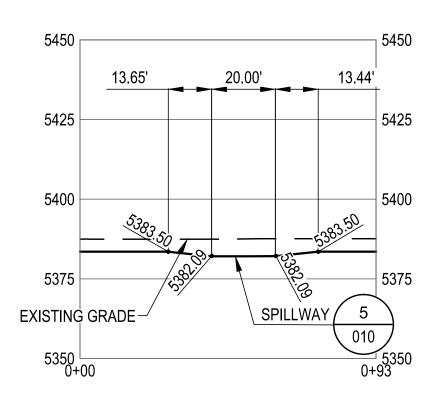
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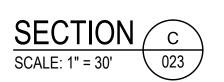


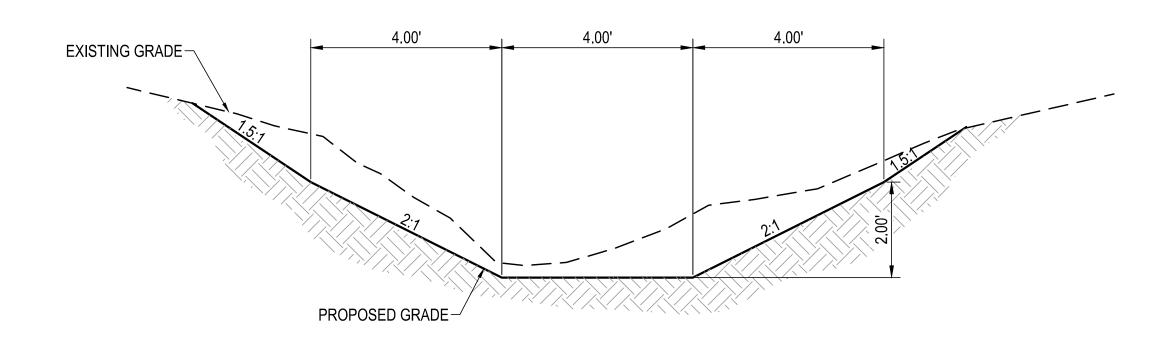






SECTION B SCALE: 1" = 30' 023



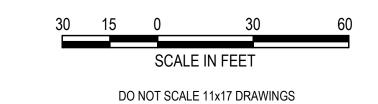


SECTION D SCALE: NTS 023

NOTES:

- 1. STORMWATER CONVEYANCE CHANNEL WILL BE DESIGNED TO CONVEY, AT A MINIMUM, THE PEAK FLOW FROM A 100 YEAR RETURN INTERVAL STORM EVENT WHILE PRESERVING NO LESS THAN 6 INCHES OF FREEBOARD.
- 2. CONVEYANCE STRUCTURE WILL BE DESIGNED TO MINIMIZE PONDING AND INFILTRATION OF STORMWATER.

FIGURE 7

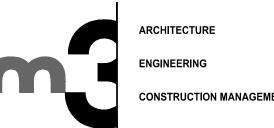


PRELIMINARY FOR AGENCY REVIEW



09 OCT 15

4																	
(5)	REFERENCES		REFERENCES	REVISIONS				REVISIONS									
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g 0000-CI-02	23 IMPACTED STORMWATER IMPOUNDMENT A, PLAN VIEW														DESIGNED BY	SAM	JUN 15
0000-CI-0	0 STANDARD DETAILS SHEET 3														DRAWN BY	SAM	JUN 15
2012															CHECKED BY	JPN	AUG 15
ä															PROJECT MGR	RKZ	AUG 15
ë															CLIENT APPR.		

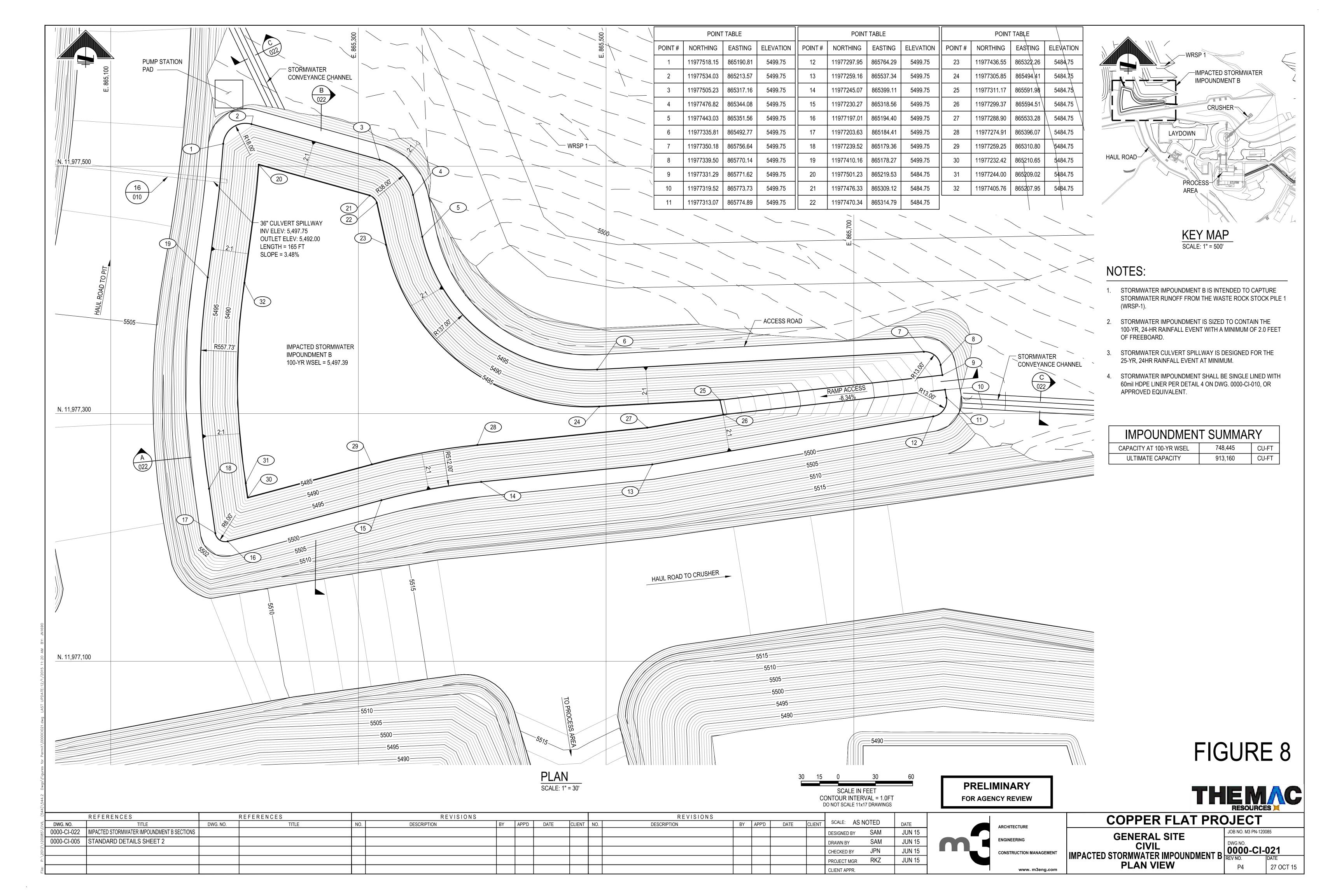


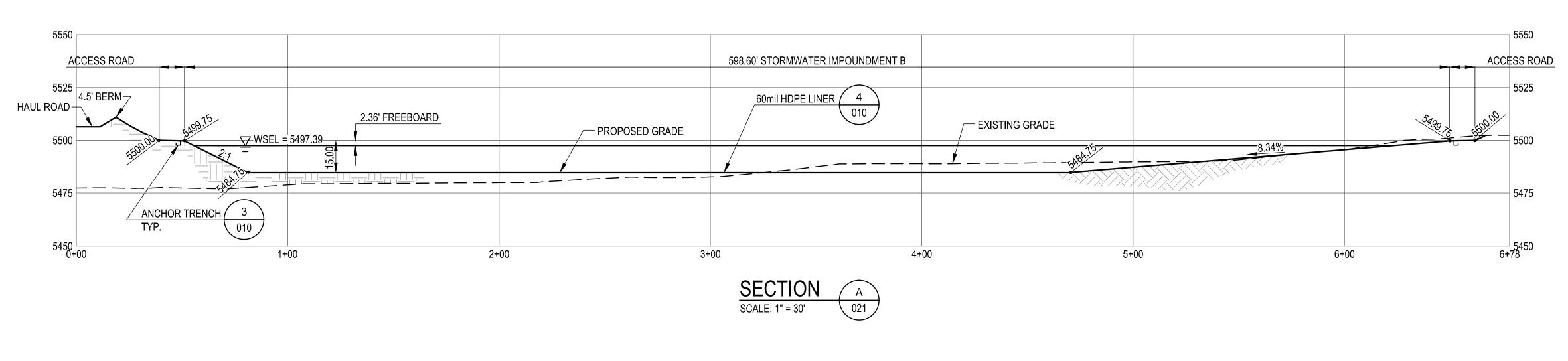
ARCHITECTURE	
ENGINEERING	
CONSTRUCTION MANAGEMENT	

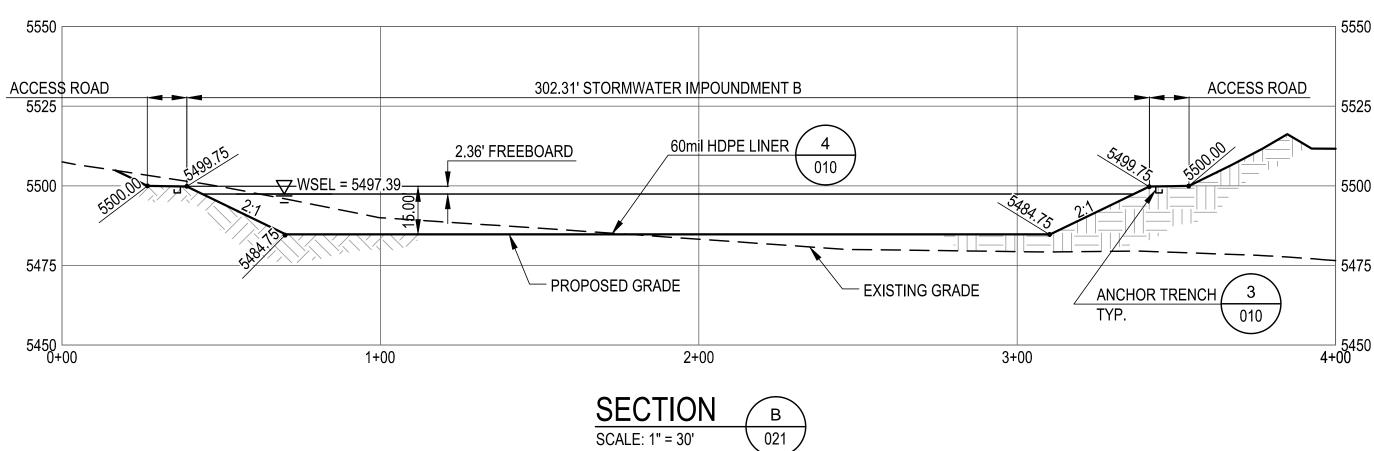
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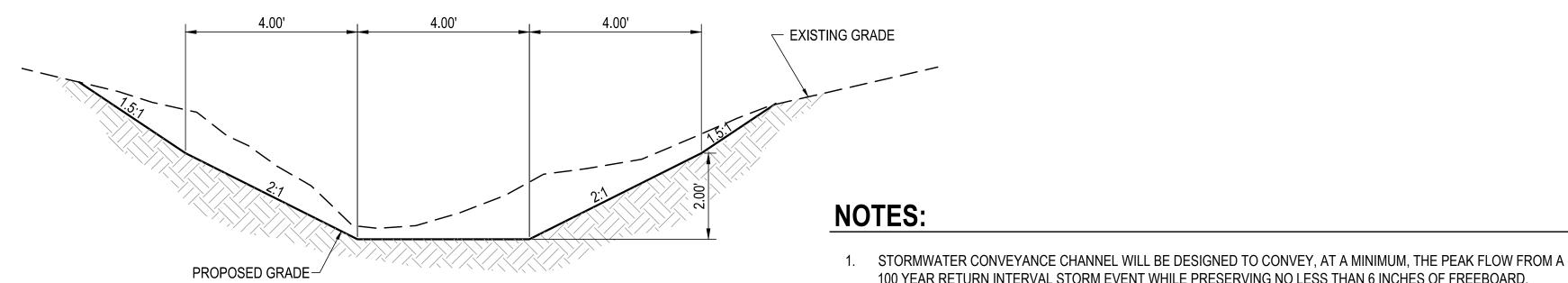
COPPER FLAT PROJECT JOB NO. M3 PN-120085

GENERAL SITE
CIVIL
IMPACTED STORMWATER IMPOUNDMENT A
SECTIONS DWG NO. **0000-CI-024**REV NO. DATE P3



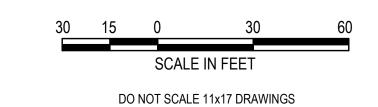






- 100 YEAR RETURN INTERVAL STORM EVENT WHILE PRESERVING NO LESS THAN 6 INCHES OF FREEBOARD.
- 2. CONVEYANCE STRUCTURE WILL BE DESIGNED TO MINIMIZE PONDING AND INFILTRATION OF STORMWATER.

FIGURE 9



PRELIMINARY NOT FOR CONSTRUCTION

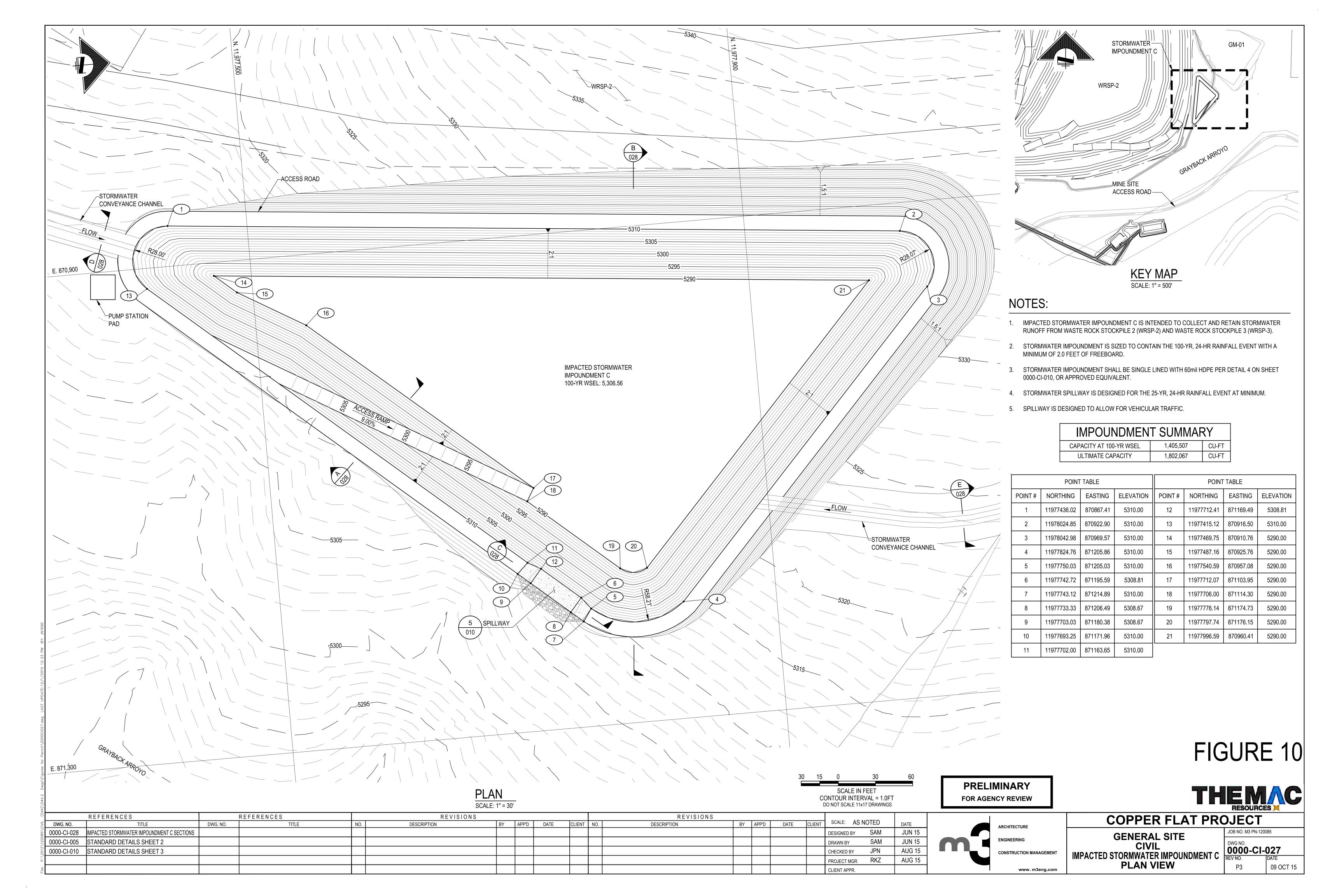


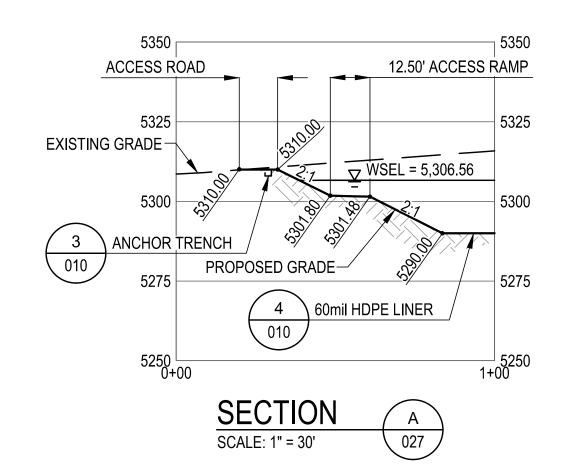
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0000-CI-021	IMPACTED STORMWATER IMPOUNDMENT B PLAN VIEW														DESIGNED BY	SAM	JUN 15
0000-CI-010	STANDARD DETAILS SHEET 3														DRAWN BY	SAM	JUN 15
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															PROJECT MGR	RKZ	AUG 15
															CLIENT APPR.		

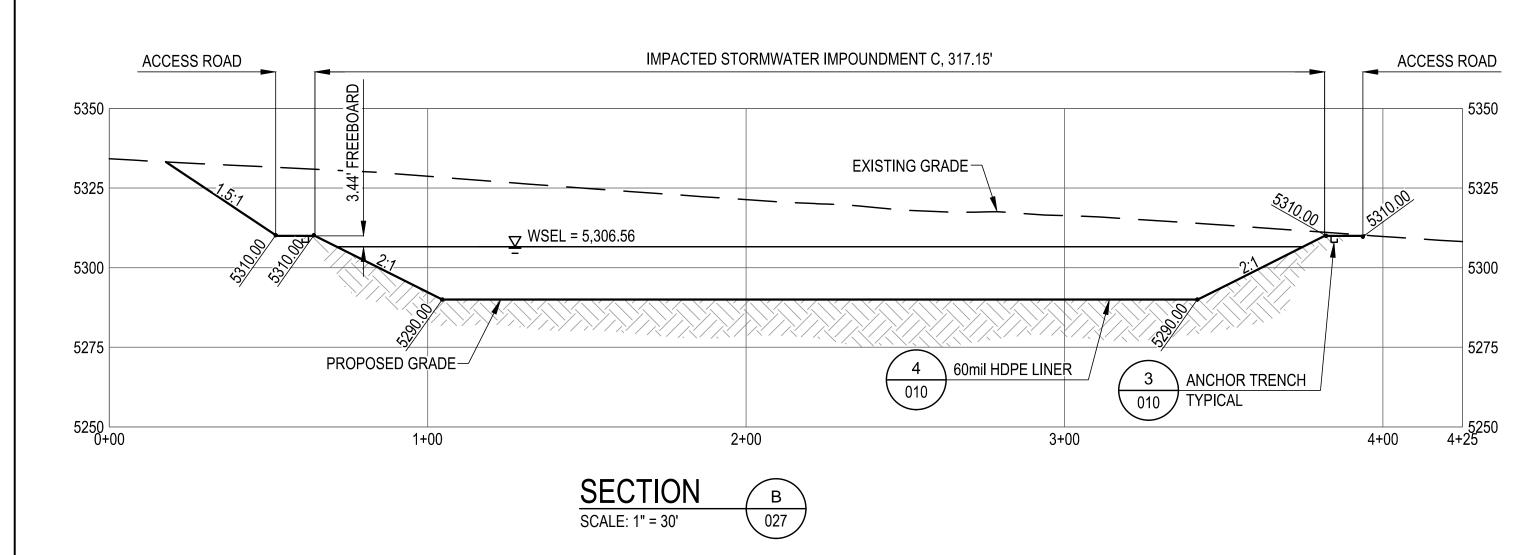
		ARCHITECTURE ENGINEERING CONSTRUCTION MANAGEMENT
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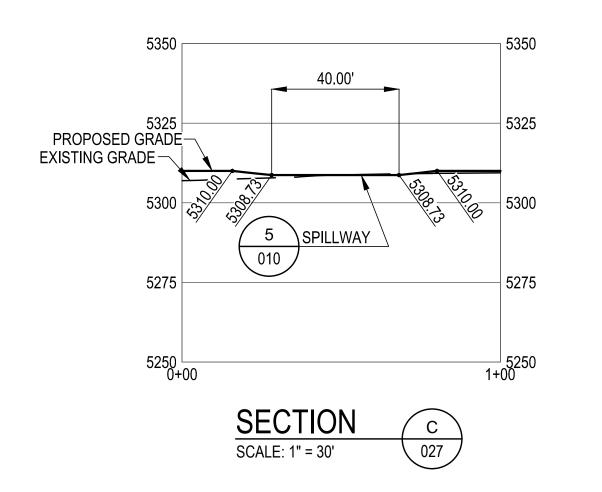
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GENERAL SITE	JOB N
CIVIL MPACTED STORMWATER IMPOUNDMENT B	DWG
SECTIONS	REV N

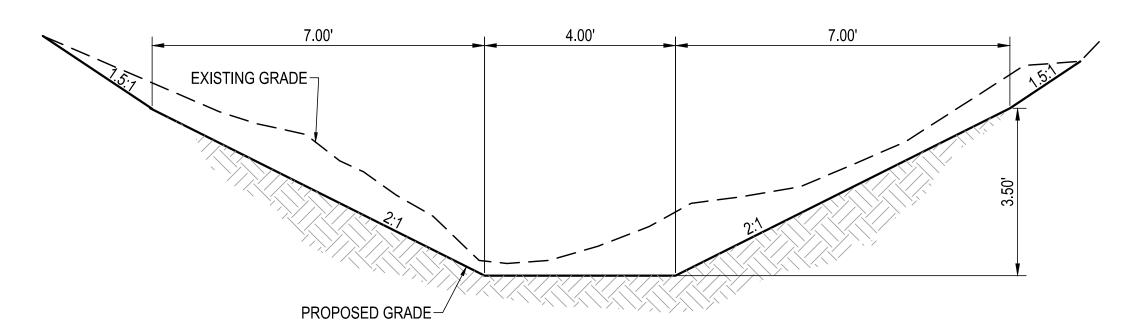
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ТВ	DWG NO. 0000-C1-	022						
ı D	REV NO.	DATE						
	P3	09 OCT 15						







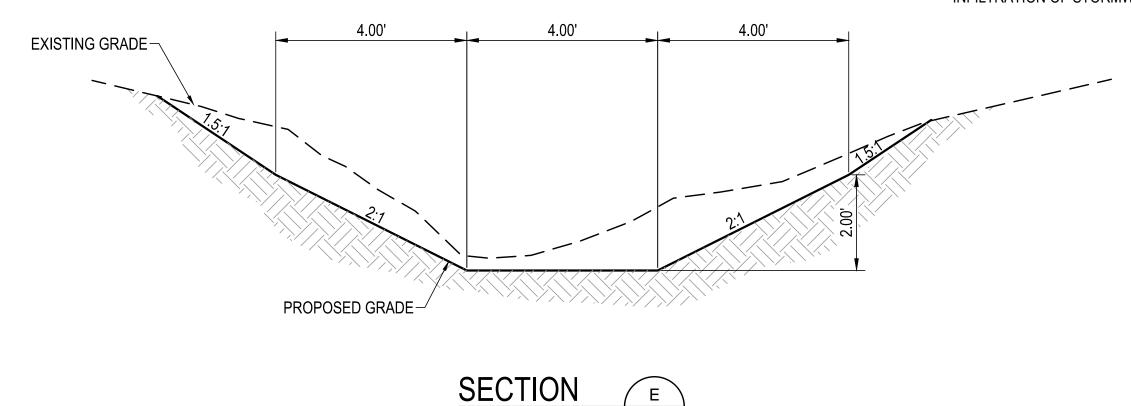




SECTION 027 SCALE: NTS

NOTES:

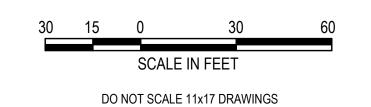
- 1. STORMWATER CONVEYANCE CHANNEL WILL BE DESIGNED TO CONVEY, AT A MINIMUM, THE PEAK FLOW FROM A 100 YEAR RETURN INTERVAL STORM EVENT WHILE PRESERVING NO LESS THAN 6 INCHES OF FREEBOARD.
- 2. CONVEYANCE STRUCTURE WILL BE DESIGNED TO MINIMIZE PONDING AND INFILTRATION OF STORMWATER.



SCALE: NTS

027

FIGURE 11



PRELIMINARY FOR AGENCY REVIEW



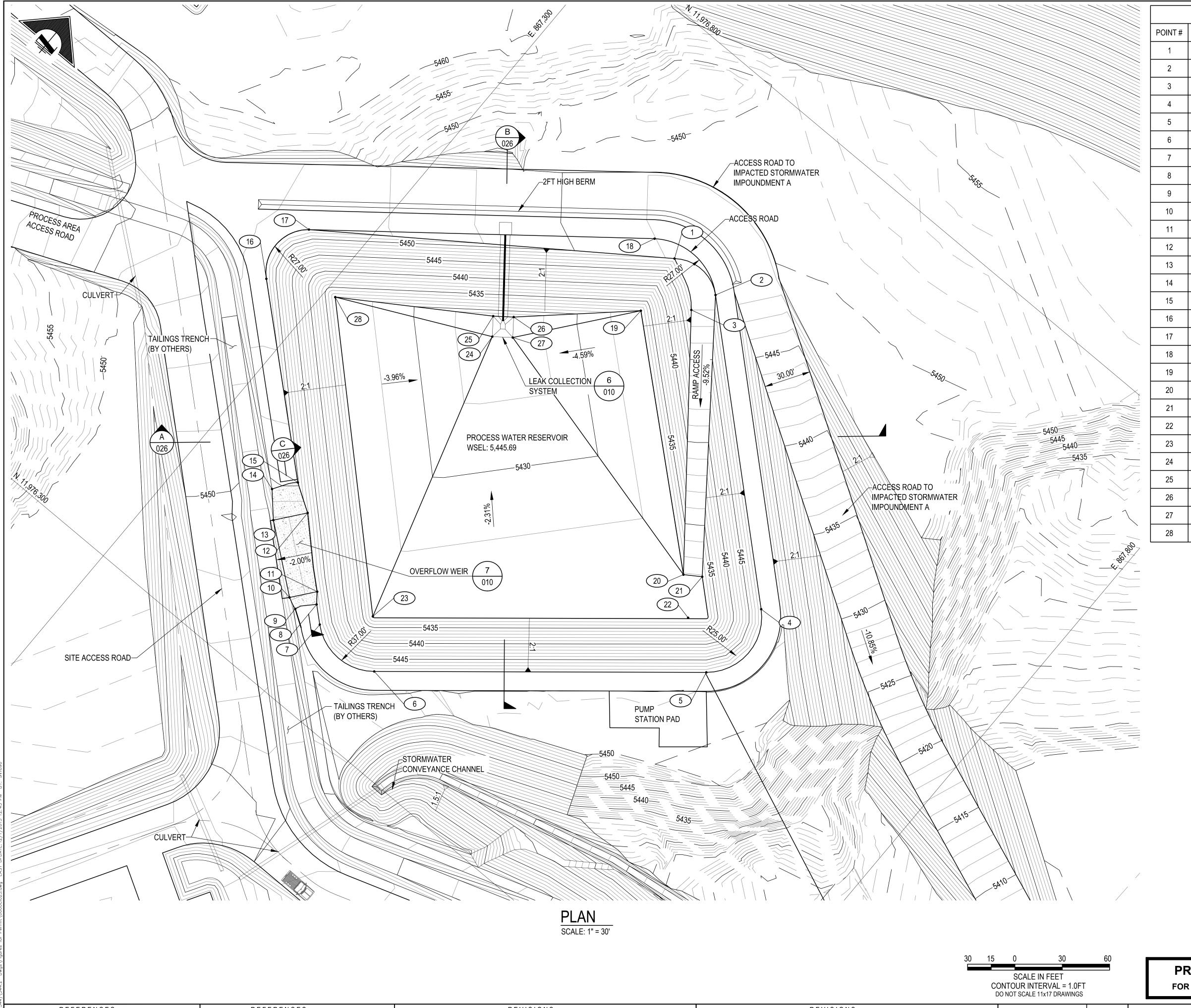
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0000-CI-027	IMPACTED STORMWATER IMPOUNDMENT C, PLAN VIEW														DESIGNED BY	SAM	JUN 15
0000-CI-010	STANDARD DETAILS SHEET 3														DRAWN BY	SAM	JUN 15
															CHECKED BY	JPN	
															PROJECT MGR	RKZ	
								_							CLIENT APPR.		

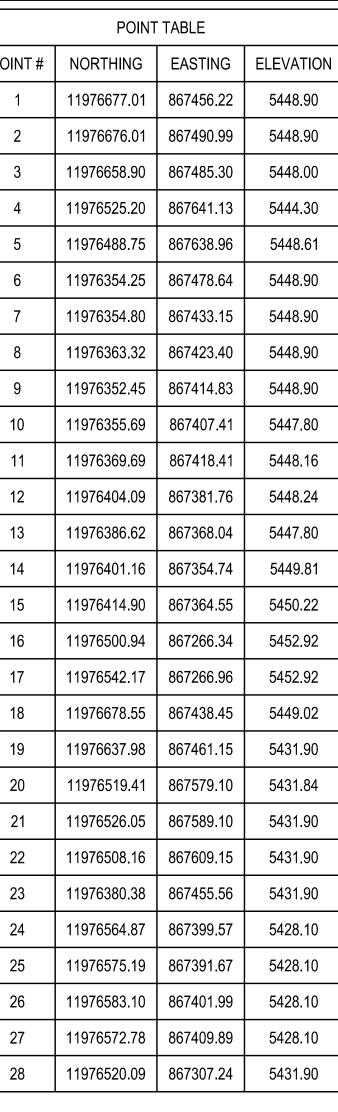


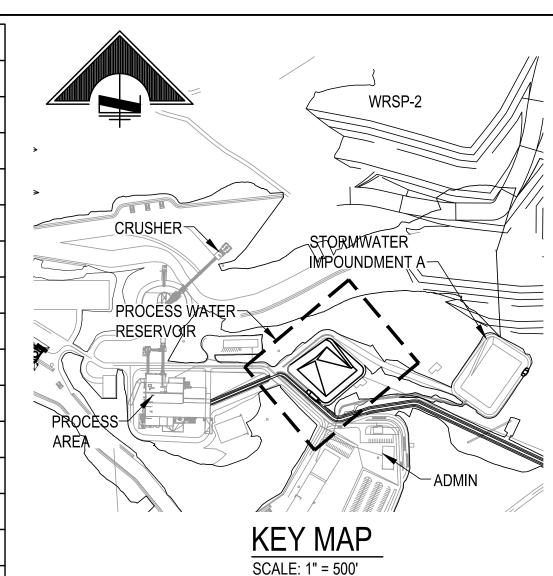
ARCHITECTURE

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COPPER FLAT PROJECT JOB NO. M3 PN-120085 GENERAL SITE
CIVIL
IMPACTED STORMWATER IMPOUNDMENT C
SECTIONS DWG NO. **0000-C1-028**REV NO. DATE 09 OCT 15 P3







- THE PROCESS WATER RESERVOIR IS INTENDED TO RETAIN PROCESS WATER, STORMWATER THAT FALLS DIRECTLY ON THE POND SURFACE, AND STORMWATER TRANSFERED FROM OTHER IMPACTED STORMWATER IMPOUNDMENTS.
- THE PROCESS WATER RESERVOIR IS SIZED TO RETAIN 12 HRS OF 7,200GPM INFLOW AND THE 100-YR, 24-HR RAINFALL EVENT PLUS 2 FEET OF FREEBOARD.
- THE PROCESS WATER WATER RESERVOIR SHALL BE DOUBLE LINED WITH 60mil HDPE PER DETAIL 2 SHEET 0000-CI-010.
- THE PROCESS WATER RESERVOIR OVERFLOW WEIR IS DESIGNED FOR THE 25-YR, 24-HR RAINFALL EVENT AT CAPACITY (SEE NOTE 2) AT MINIMUM. THE WEIR CONVEYS PROCESS WATER INTO THE TAILINGS TRENCH AND TO THE TAILINGS IMPOUNDMENT.
- OVERFLOW WEIR IS DESIGNED TO ALLOW FOR VEHICULAR TRAFFIC.

IMPOUNDMEN	T SUMMAF	RY
CAPACITY AT 100-YR WSEL	726,365	CU-FT
ULTIMATE CAPACITY	937,998	CU-FT

FIGURE 12

PRELIMINARY FOR AGENCY REVIEW



REFERENCES REVISIONS REFERENCES REVISIONS SCALE: AS NOTED BY APP'D DATE BY APP'D DATE CLIENT TITLE DESCRIPTION DWG. NO. DESCRIPTION PROCESS WATER RESERVOIR SECTIONS JUN 15 SAM 0000-CI-026 DESIGNED BY JUN 15 STANDARD DETAILS SHEET 3 SAM 0000-CI-010 RAWN BY AUG 15 JPN CHECKED BY AUG 15 PROJECT MGR RKZ CLIENT APPR.



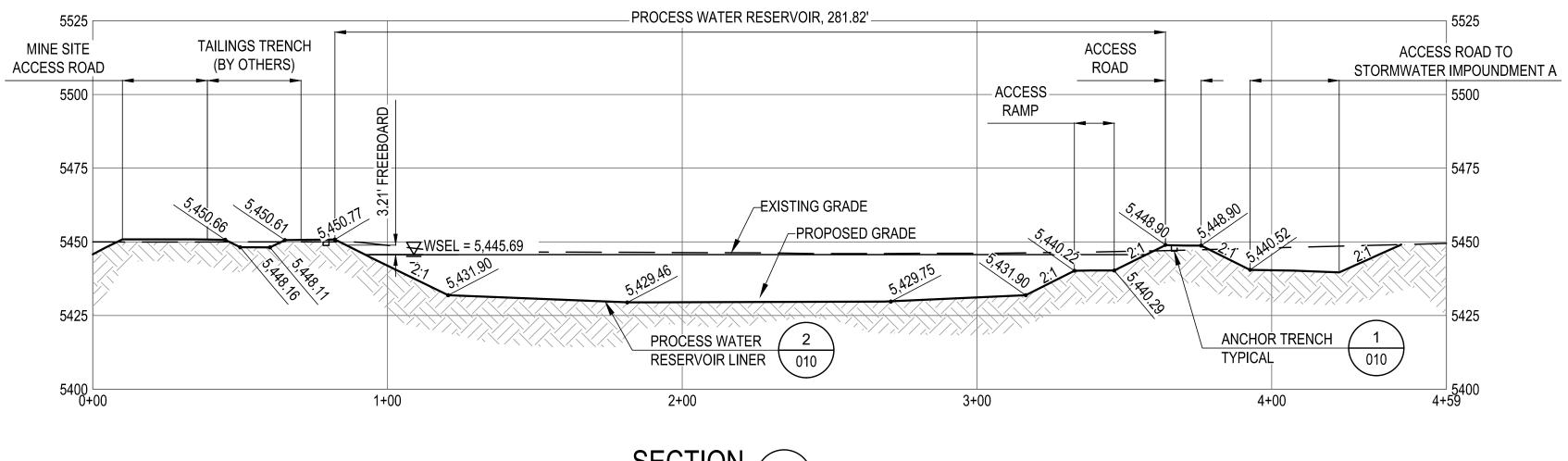
ARCHITECTURE **ENGINEERING**

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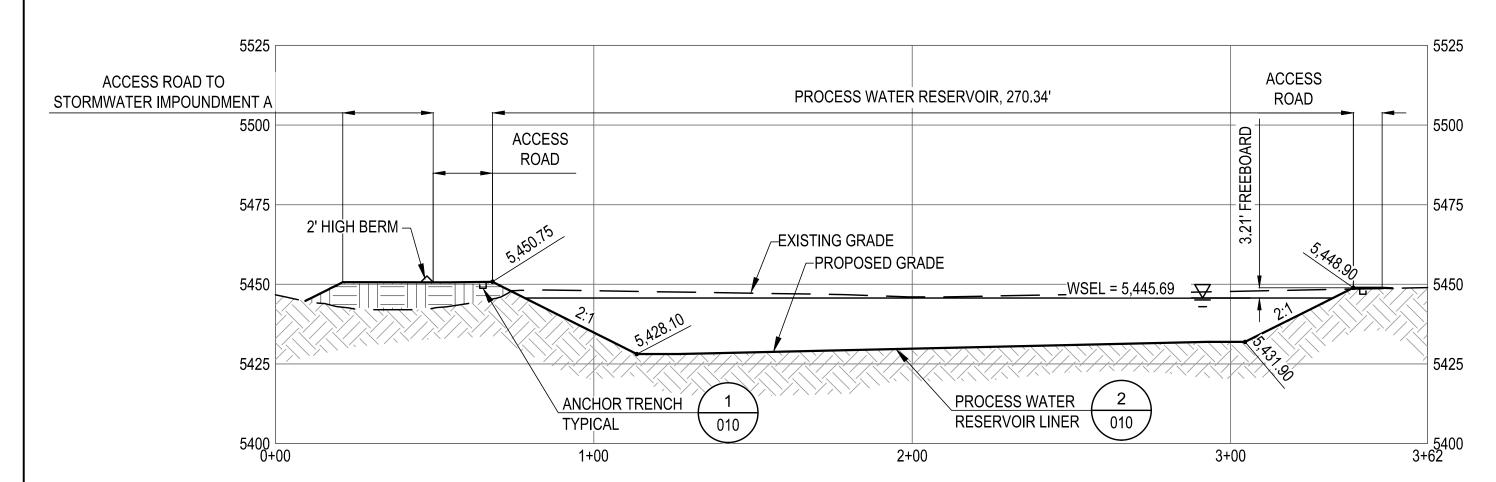
COPPER FLAT PROJECT

GENERAL SITE
CIVIL
PROCESS WATER RESERVOIR **PLAN VIEW**

JOB NO. M3 PN-120085 DWG NO. **0000-CI-025** 09 OCT 15 P3







SECTION B SCALE: 1" = 30' 025

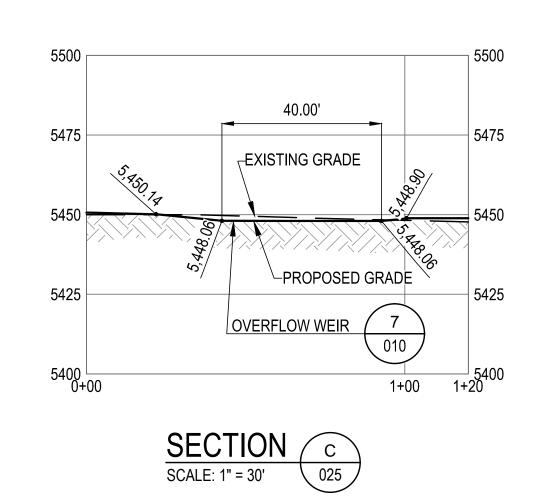
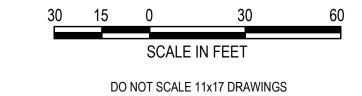


FIGURE 13



PRELIMINARY
FOR AGENCY REVIEW



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(5		REFERENCES		REFERENCES		REVISIONS					REVISIONS							
	DWG. NO.	TITLE	DWG. NO.	TITLE	NO.	DESCRIPTION BY	APP'D	DATE	CLIENT	NO.	DESCRIPTION	BY	APP'D D	DATE CL	LIENT	SCALE: AS NOTED	DATE	
085/0	0000-CI-025	PROCESS WATER RESERVOIR PLAN VIEW														DESIGNED BY SAM	JUN 15	
1200	0000-CI-010	STANDARD DETAILS SHEET 3														DRAWN BY SAM	JUN 15	
2012	1 - - -															CHECKED BY JPN		
á	-															PROJECT MGR RKZ		
<u>.</u>	<u> </u>															CLIENT APPR.		



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PROCESS WATER RESERVOIL
SECTIONS

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	JOB NO. M3 PN-1200)85						
IR	DWG NO. 0000-C1-0							
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	P3	09 OCT 15						

